

Annex A Damage consequence class and quick clay grade class

1 Lanner 1

Damage consequence class

Faktorer	Vekttall	Konsekvens, score				Score	Poeng	Kommentar
		3	2	1	0			
Boligenheter, antall	4	Tett > 5	Spredt > 5	Spredt < 5	Ingen	0	0	Ingen
Næringsbygg, personer	3	> 50	10 - 50	< 10	Ingen	0	0	Ingen
Annen bebyggelse, verdi	1	Stor	Betydelig	Begrenset	Ingen	0	0	Ingen
Vei, ÅDT	2	> 5000	1001 - 5000	100 - 1000	< 100	3	6	E18 (> 5000)
Toglinje, baneprioritet	2	1-2	3-4	5	Ingen	0	0	Ingen
Kraftnett	1	Sentral	Regional	Distribusjon	Lokal	0	0	Ingen
Oppdemning/ flom	2	Alvorlig	Middels	Liten	Ingen	0	0	Ingen
Sum poeng		45	30	15	0		6	
% av maksimal poengsum		100 %	67 %	33 %	0 %		13 %	
Skadekonsekvensklasse								
Meget alvorlig		Alvorlig		Mindre alvorlig				
23-45 poeng		7-22		0-6				

quick clay grade class

					Faregrad, score			
Faktorer	Vekt-tall	Score	Poeng	Kommentar	3	2	1	0
Tidligere skredaktivitet	1	0	0	Ikke registrert.	Høy	Noe	Lav	Ingen
Skråningshøyde	2	0	0	Største skråning <15 m høyde	> 30	20-30	15-20	<15
Tidligere/nåværende terrengnivå (OCR)	2	2	4	Usikker. Antar noen overkonsolidert (~1,2)	1,0-1,2	1,2-1,5	1,5-2,0	>2,0
Poretrykk, overtrykk	3	0	0	Hydrostatisk	> +30	10-30	0-10	Hydrostatisk
Poretrykk, undertrykk	-3	0	0	Hydrostatisk	> -50	-(20-50)	-(0-20)	Hydrostatisk
Kvikkleiremektighet	2	3	6	Større enn H/2	> H/2	H/2-H/4	< H/4	Tynt lag
Sensitivitet	1	2	2	Varierende men mer enn 30 og mindre enn 100	> 100	30-100	20-30	<20
Erosjon	3	0	0	Ingen erosjon	Aktiv/glidn.	Noe	Lite	Ingen
Inngrep, forverring	3	0	0	Ingen forverring	Stor	Noe	Liten	Ingen
Inngrep, forbedring	-3	2	-6	Liten forbedring da ny vei vil ligge høyere enn dagens vei.	Stor	Noe	Liten	Ingen
Poeng			6					
Faregradsklasse			Lav		Faregradsklasse			
					Lav	Middels	Høy	
					0-17	18-25	26-51	

2 Lanner 2

Damage consequence class

Faktor er	Vektt all	Konsekvens, score				Sco re	Poe ng	Kommen tar
		3	2	1	0			
Boligenhe ter, antall	4	Tett> 5	Spredt >5	Spredt <5	Ing en	0	0	Ingen
Næringsb bygg, personer	3	>50	10 - 50	<10	Ing en	0	0	Ingen
Annen bebyggels e, verdi	1	Stor	Betyde lig	Begrense t	Ing en	0	0	Ingen
Vei, ÅDT	2	>500 0	1001- 5000	100- 1000	<10 0	3	6	E18 (>5000)
Toglinje, banepriori tet	2	1-2	3-4	5	Ing en	0	0	Ingen
Kraftnett	1	Sentr al	Region al	Distribusj on	Lok al	0	0	Ingen
Oppdemni ng/ flom	2	Alvorli g	Middel s	Liten	Ing en	0	0	Ingen
Sum poeng		45	30	15	0		6	
% av maksimal poengsum		100 %	67 %	33 %	0 %		13 %	
Skadekonsekvensklasse								
Meget alvorlig		Alvorlig		Mindre alvorlig				
23-45 poeng		7-22		0-6				

quick clay grade class

Faktorer	Vekt-tall	Score	Poeng	Kommentar	Faregrad, score			
					3	2	1	0
Tidligere skredaktivitet	1	0	0	Ikke registrert.	Høy	Noe	Lav	Ingen
Skråningshøyde	2	0	0	Største skråning <15 m høyde	> 30	20-30	15-20	<15
Tidligere/ nåværende terrengnivå (OCR)	2	2	4	Usikker. Antar noen overkonsolidert (~1,2)	1,0-1,2	1,2-1,5	1,5-2,0	>2,0
Poretrykk, overtrykk	3	0	0	Hydrostatisk	>+30	10-30	0-10	Hydrostatisk
Poretrykk, undertrykk	-3	0	0	Hydrostatisk	>-50	-(20-50)	-(0-20)	Hydrostatisk
Kvikkleiremektighet	2	2	4	Varierende. Velger H/2 – H/4.	>H/2	H/2-H/4	<H/4	Tynt lag
Sensitivitet	1	2	2	Varierende men mer enn 30 og mindre enn 100	>100	30-100	20-30	<20
Erosjon	3	2	6	Noe erosjon	Aktiv/glidn.	Noe	Lite	Ingen
Inngrep, forverring	3	0	0	Ingen forverring	Stor	Noe	Liten	Ingen
Inngrep, forbedring	-3	3	-9	Forbedring da ny vei vil ligge i senkningen sånn at ny vei vill bli som en motfylling	Stor	Noe	Liten	Ingen
Poeng			7					
Faregradsklasse			Lav		Faregradsklasse			
					Lav	Middels	Høy	
					0-17	18-25	26-51	

3 Kjørholt

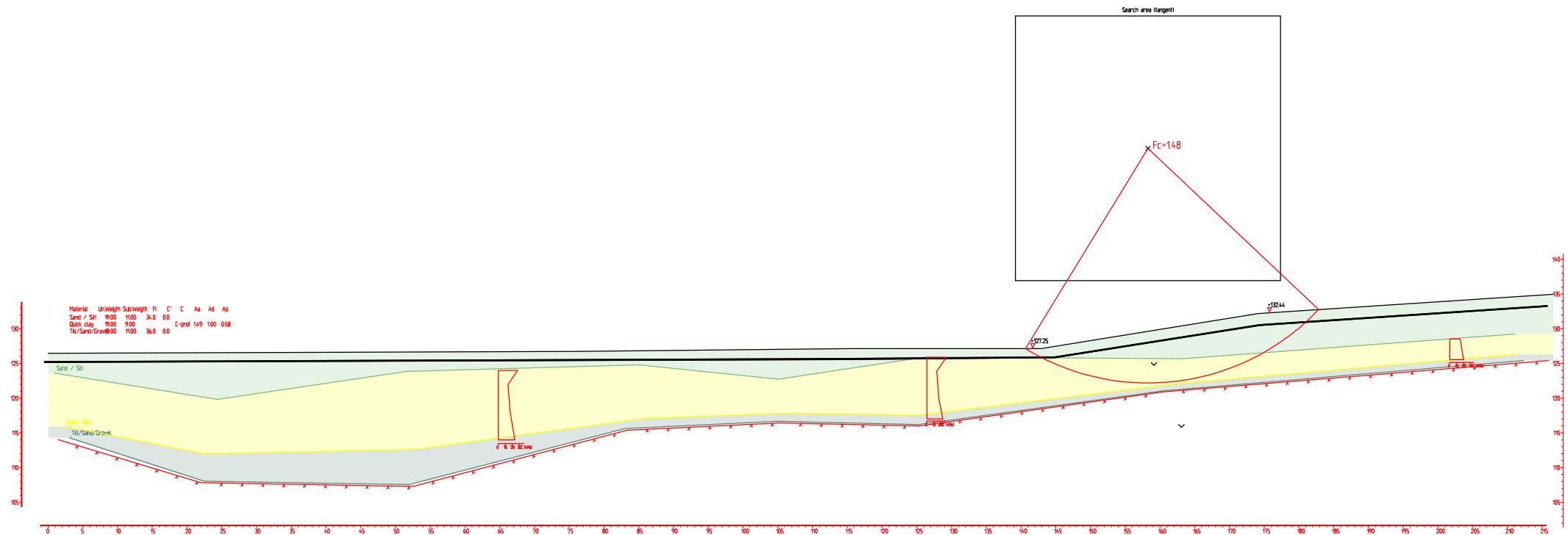
Damage consequence class

Faktor er	Vektt all	Konsekvens, score				Sco re	Poe ng	Kommen tar
		3	2	1	0			
Boligenhe ter, antall	4	Tett> 5	Spredt >5	Spredt <5	Ing en	1	4	Spredt
Næringsb ygg, personer	3	>50	10 - 50	<10	Ing en	0	0	Ingen
Annen bebyggels e, verdi	1	Stor	Betyde lig	Begrense t	Ing en	0	0	Begrenset
Vei, ÅDT	2	>500 0	1001- 5000	100- 1000	<10 0	1	2	Noen lokalvei. E18 på behørig avstand
Toglinje, banepriori tet	2	1-2	3-4	5	Ing en	0	0	Ingen
Kraftnett	1	Sentr al	Region al	Distribusj on	Lok al	0	0	Ingen
Oppdemni ng/ flom	2	Alvorli g	Middel s	Liten	Ing en	0	0	Ingen
Sum poeng		45	30	15	0		6	
% av maksimal poengsum		100 %	67 %	33 %	0 %		13 %	
Skadekonsekvensklasse								
Meget alvorlig		Alvorlig		Mindre alvorlig				
23-45 poeng		7-22		0-6				

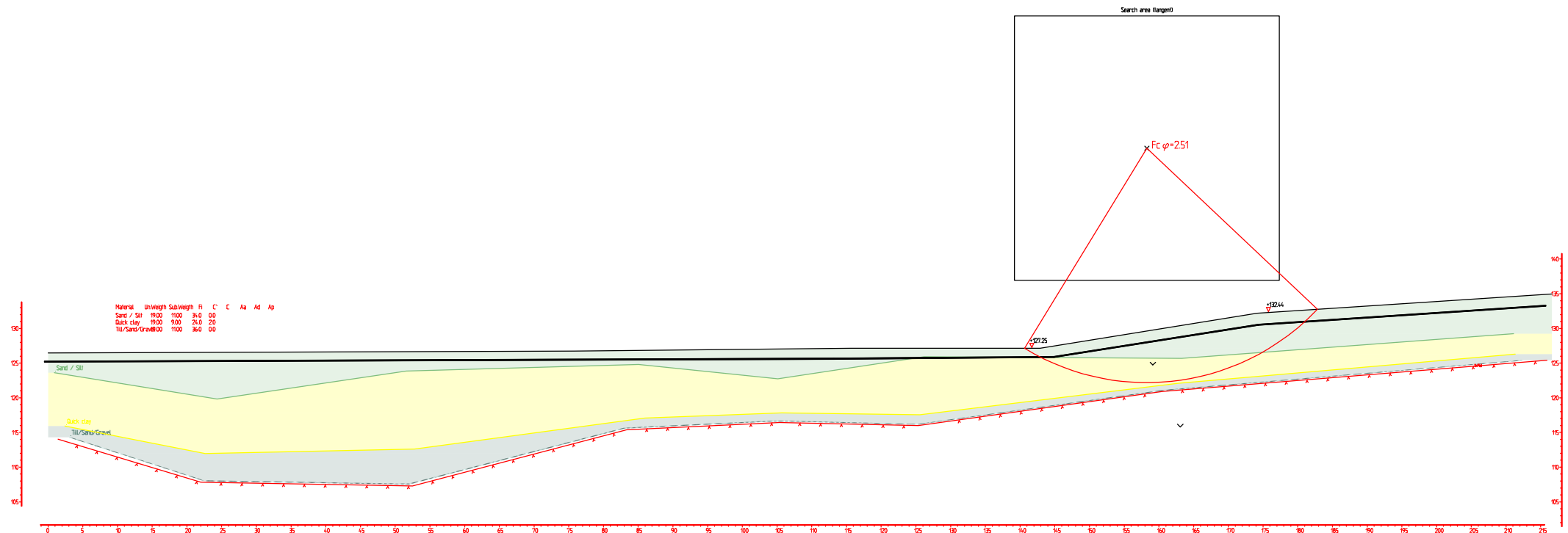
quick clay grade class

					Faregrad, score			
Faktorer	Vekt-tall	Score	Poeng	Kommentar	3	2	1	0
Tidligere skredaktivitet	1	0	0	Ikke registrert.	Høy	Noe	Lav	Ingen
Skråningshøyde	2	0	0	Største skråning <15 m høyde	> 30	20-30	15-20	<15
Tidligere/ nåværende terrengnivå (OCR)	2	2	4	Usikker. Antar noen overkonsolidert (~1,2)	1,0-1,2	1,2-1,5	1,5-2,0	>2,0
Poretrykk, overtrykk	3	0	0	Hydrostatisk	> +30	10-30	0-10	Hydrostatisk
Poretrykk, undertrykk	-3	0	0	Hydrostatisk	> -50	-(20-50)	-(0-20)	Hydrostatisk
Kvikkleiremektighet	2	2	4	Varierende. Velger H/2 – H/4. Mye usikker.	> H/2	H/2-H/4	< H/4	Tynt lag
Sensitivitet	1	1	1	Varierende men mindre enn 30	>100	30-100	20-30	<20
Erosjon	3	0	0	Ingen bekk	Aktiv/ glidn.	Noe	Lite	Ingen
Inngrep, forverring	3	0	0	Ingen forverring	Stor	Noe	Liten	Ingen
Inngrep, forbedring	-3	1	-3	Tiltaket (ny E18) vil innebære forbedring da det vil fungere som en motfylling. En viss effekt på forbedring av stabiliteten.	Stor	Noe	Liten	Ingen
Poeng			6					
Faregradsklasse			Lav		Faregradsklasse			
					Lav	Middels	Høy	
					0-17	18-25	26-51	

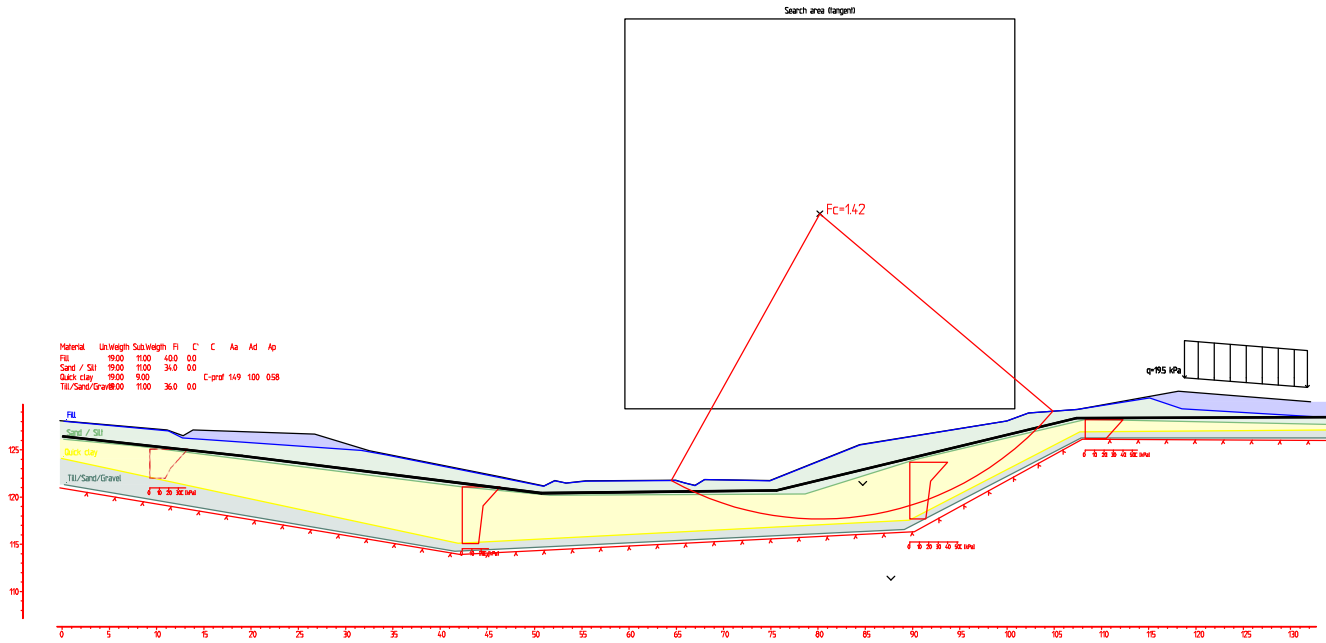
Annex B1 Calculations Area Stability



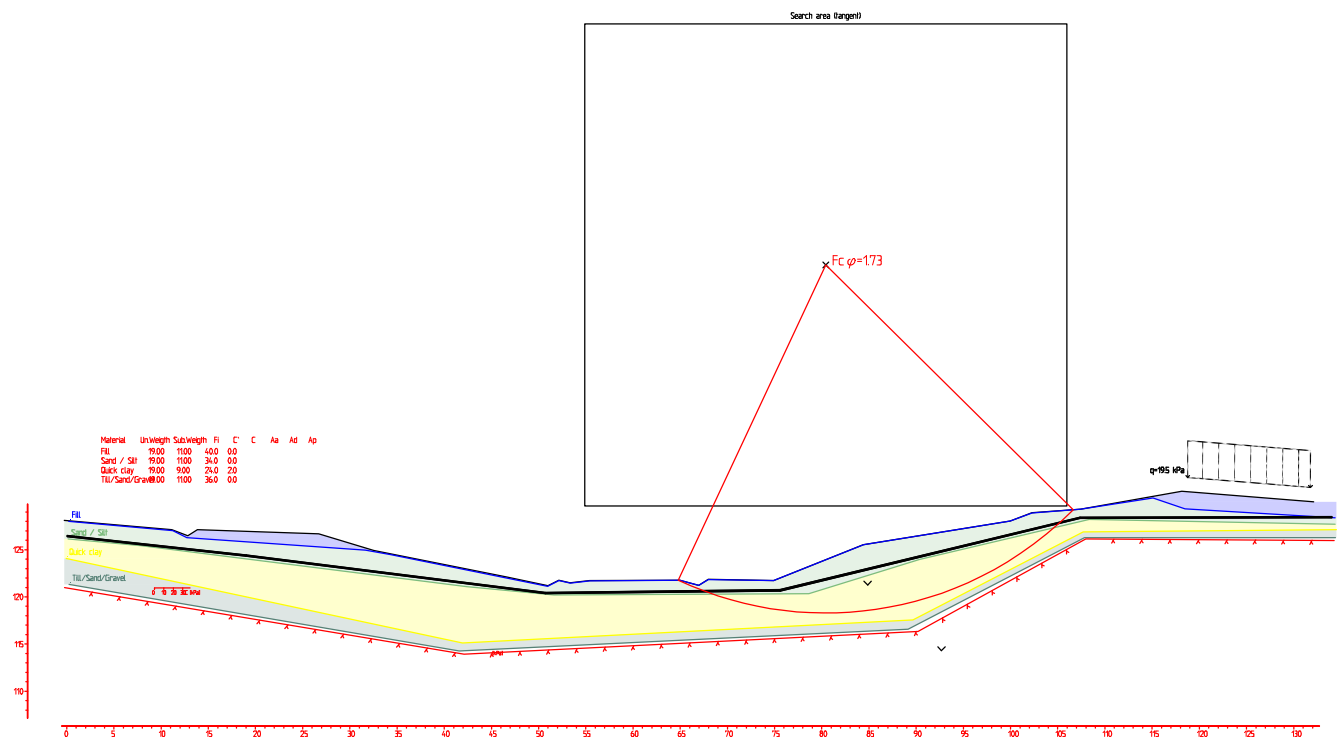
Annex B2 Calculations Area Stability



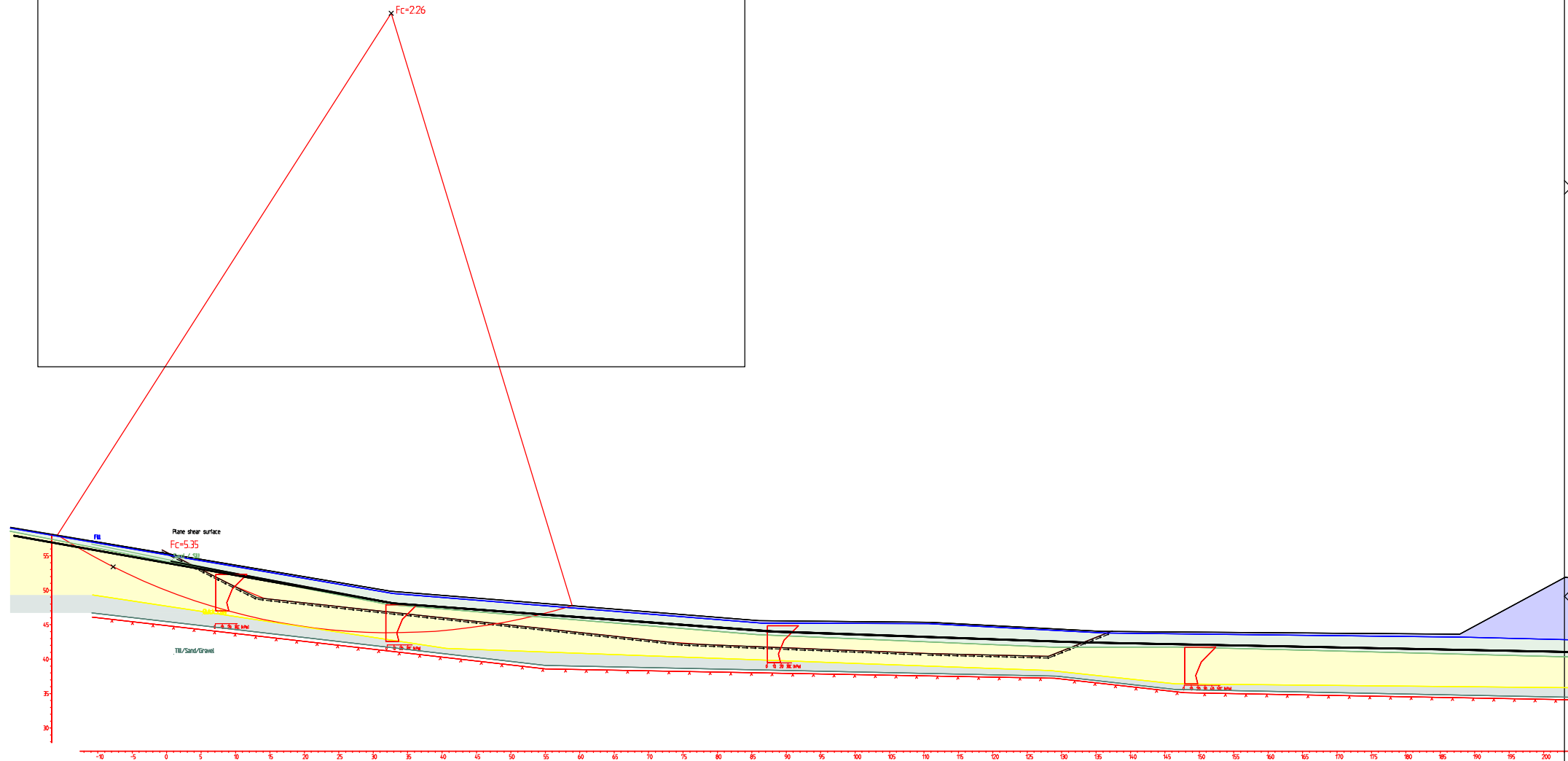
Annex B3 Calculations Area Stability



Annex B4 Calculations Area Stability

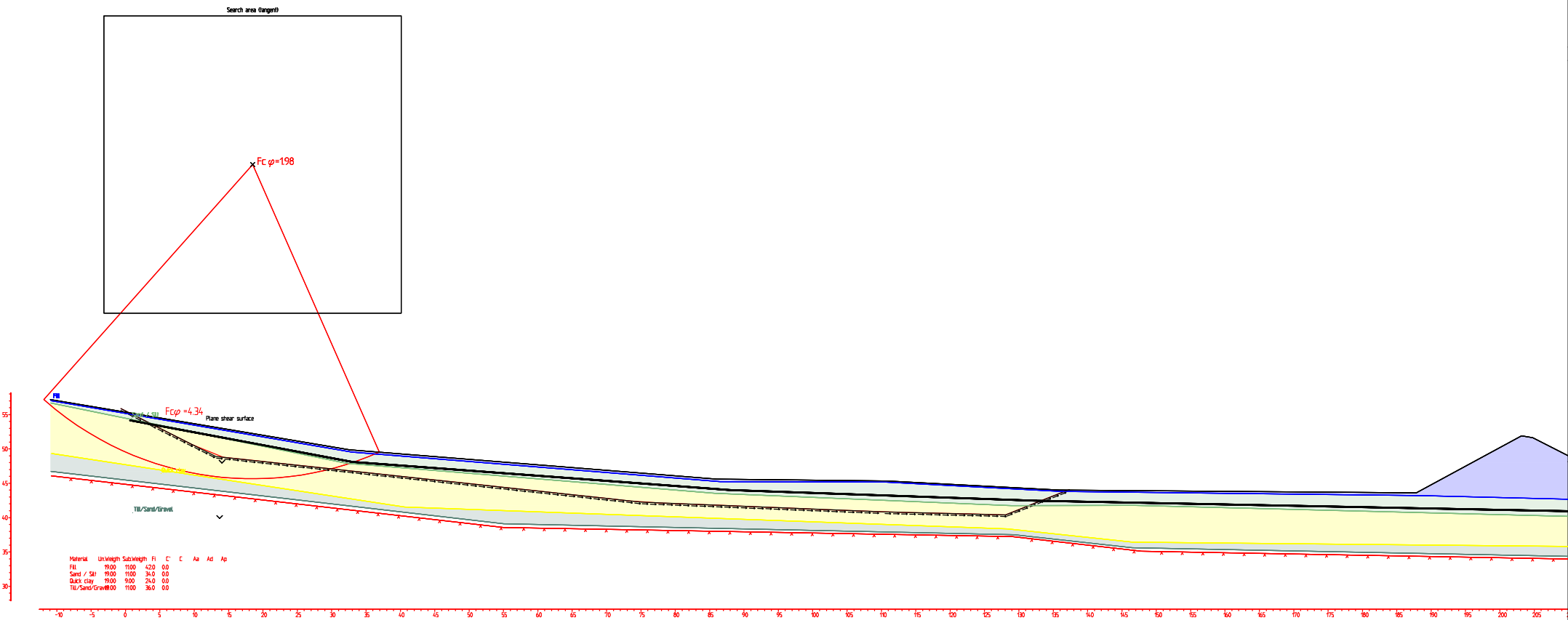


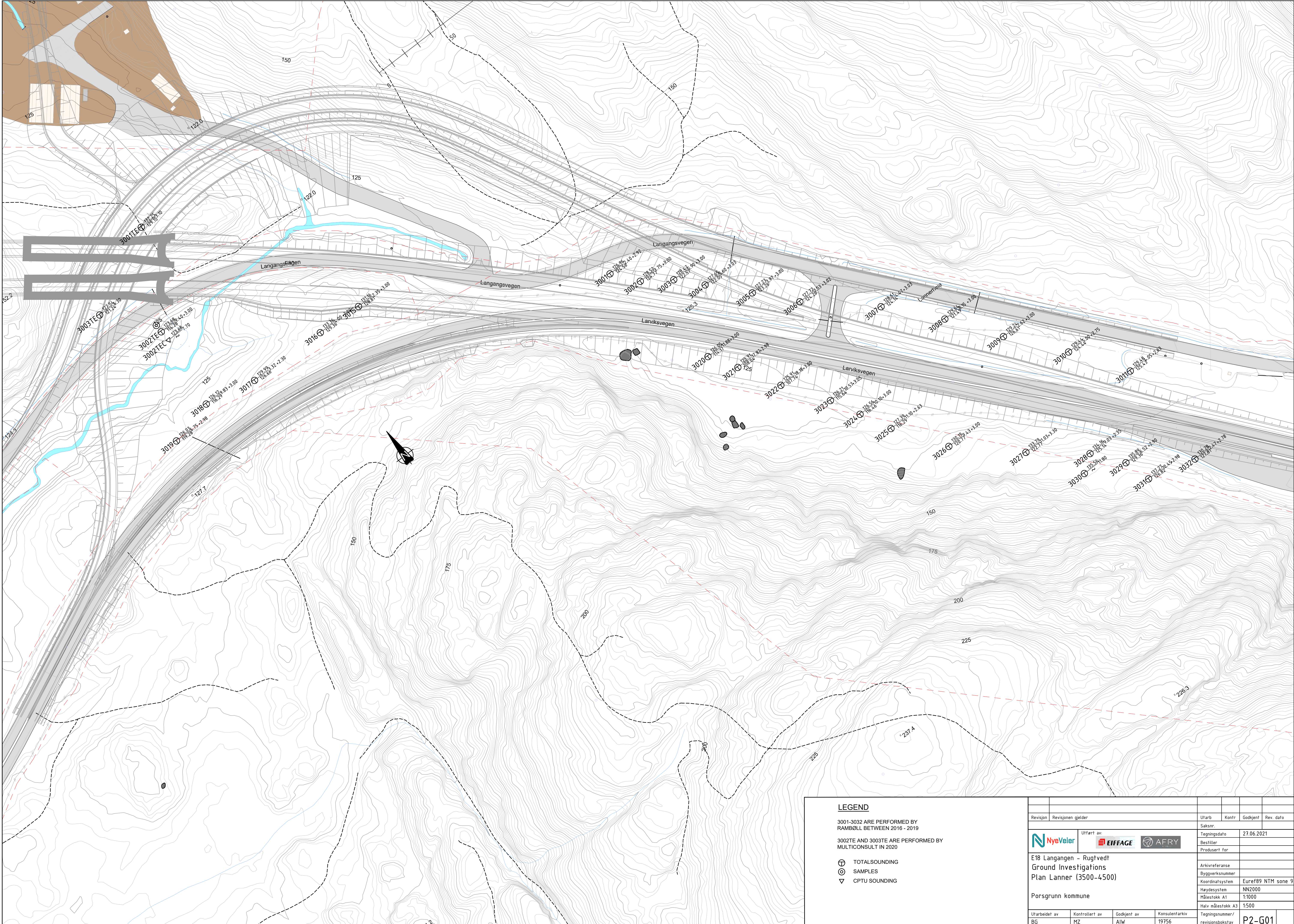
Annex B5 Calculations Area Stability



Material	Un Weight	Sub Weight	FI	C	C	Aa	Ad	Ap
Fil	1900	1100	420	0.0				
Sand / Sil	1900	1100	36.0	0.0				
Quick clay	1900	900			C-prot	149	100	0.58
Till/Sand/Gravel	1900	1100	36.0	0.0				

Annex B6 Calculations Area Stability





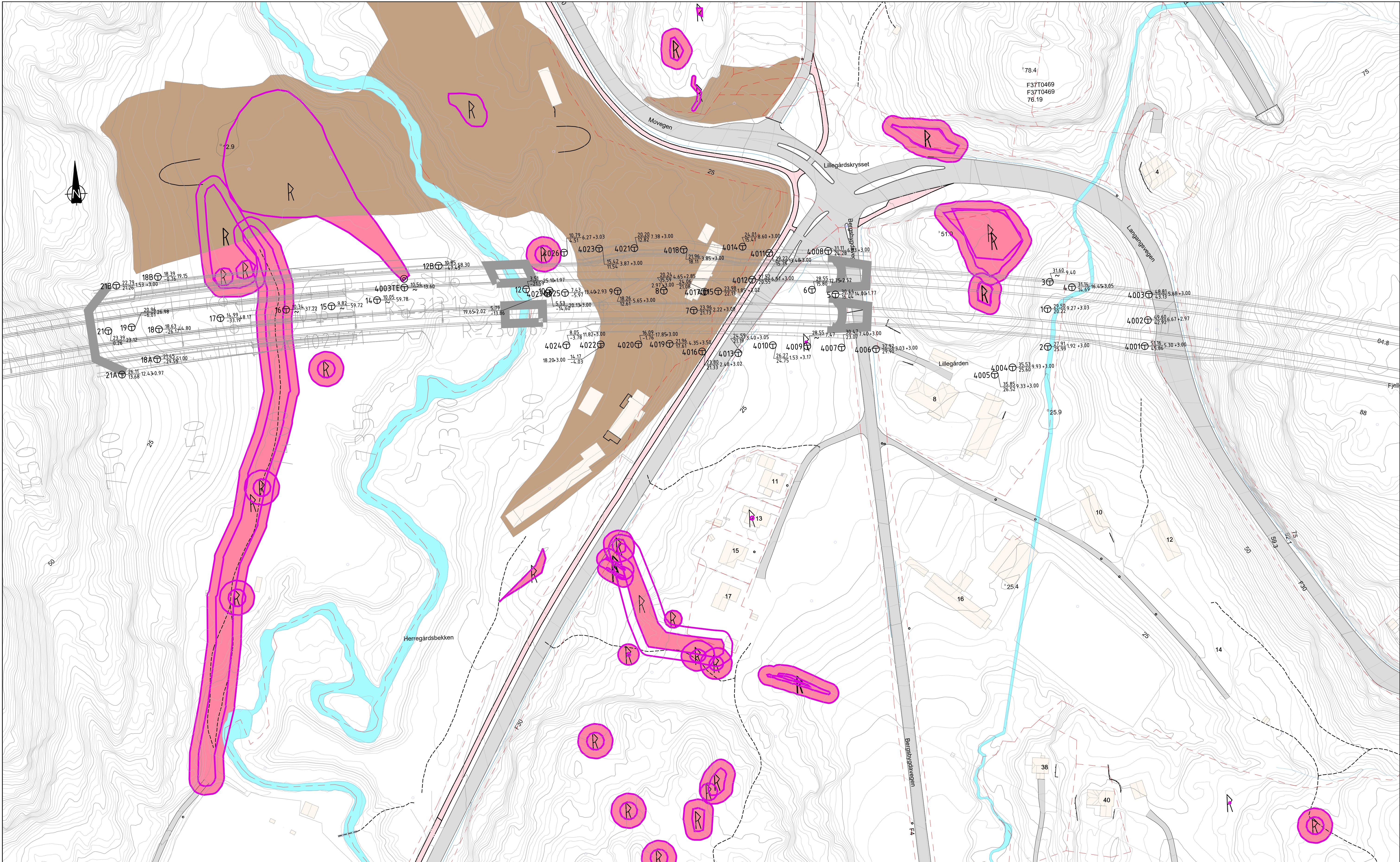
LEGEND

3001-3032 ARE PERFORMED BY
RAMBØLL BETWEEN 2016 - 2019

3002TE AND 3003TE ARE PERFORMED BY
MULTICONSULT IN 2020

- ⊕ TOTALSOUNDING
- ⊙ SAMPLES
- ▽ CPTU SOUNDING

Revisjon	Revisjonen gjelder	Utarb	Kontr	Godkjent	Rev. dato
		Saksnr.			
		Tegningsdato			27.06.2021
		Bestiller			
		Produsert for			
		Arkivreferanse			
		Byggeværksnummer			
		Koordinatsystem			Euref89 NTM sone 9
		Høydesystem			NN2000
		Målestokk A1			1:1000
		Halv målestokk A3			1:500
Utarbeidet av	Kontrollert av	Godkjent av	Konsulentarkiv	Tegningsnummer/ revisjonsbokstav	P2-G01
BG	MZ	AIW	19756		

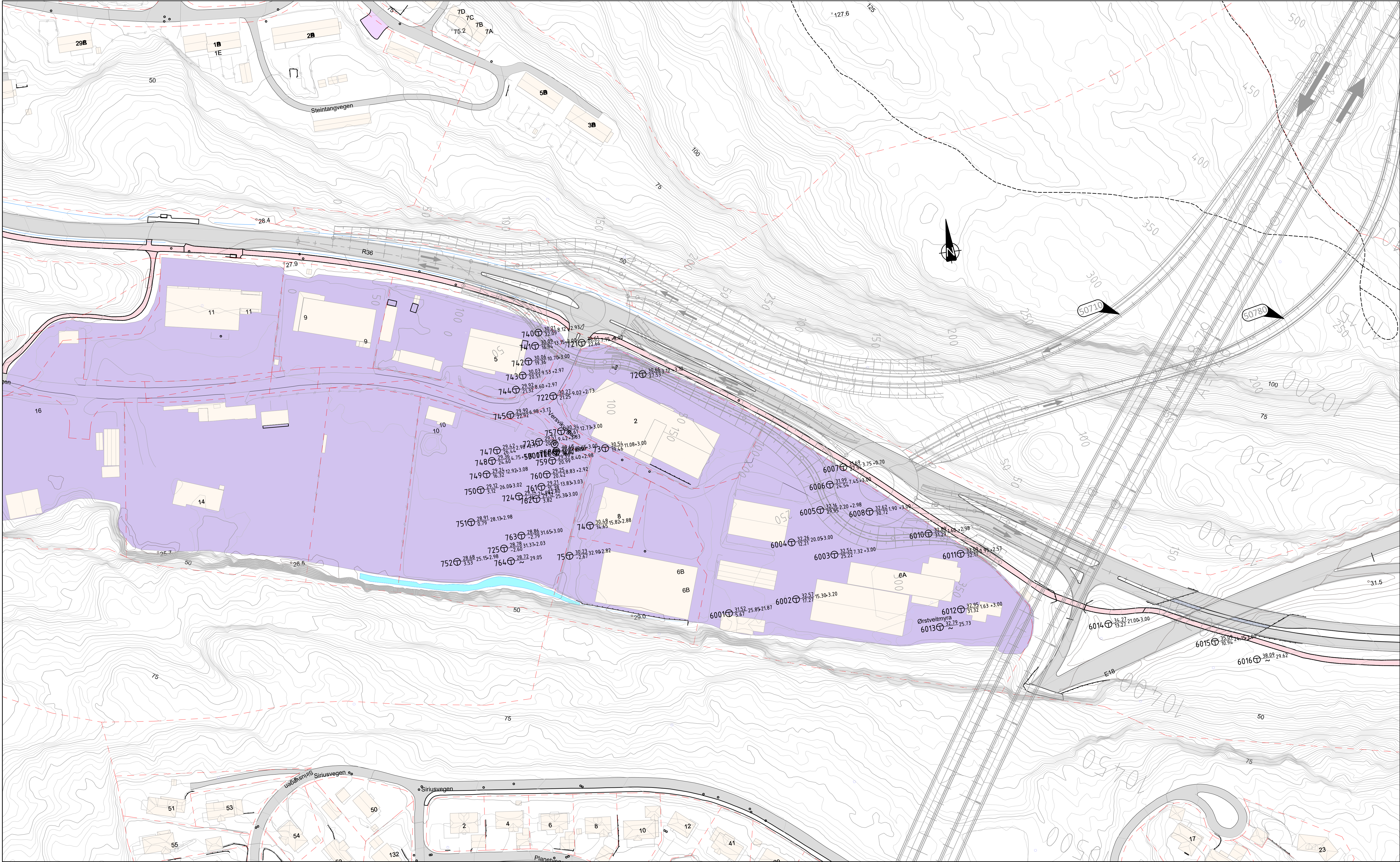


LEGEND

4001-4026 AND 1-25 ARE PERFORMED BY RAMBØLL BETWEEN 2016 - 2019
4003TE IS PERFORMED BY MULTICONSULT IN 2020

- ⊕ TOTALSOUNDING
- ⊙ SAMPLES
- ▽ CPTU SOUNDING

Revisjon	Revisjonen gjelder	Utarb	Kontr	Godkjent	Rev. dato
		Saksnr.			
		Tegningsdato			27.06.2021
		Bestiller			
		Produsert for			
		Arkivreferanse			
		Byggeværksnummer			
		Koordinatsystem			Euref89 NTM sone 9
		Haydesystem			NN2000
		Målestokk A1			1:1000
		Halv målestokk A3			1:500
		Tegningsnummer/ revisjonsbokstav			P2-G02
Utarbeidet av	Kontrollert av	Godkjent av	Konsulentarkiv		
BG	MZ	AIW	19756		

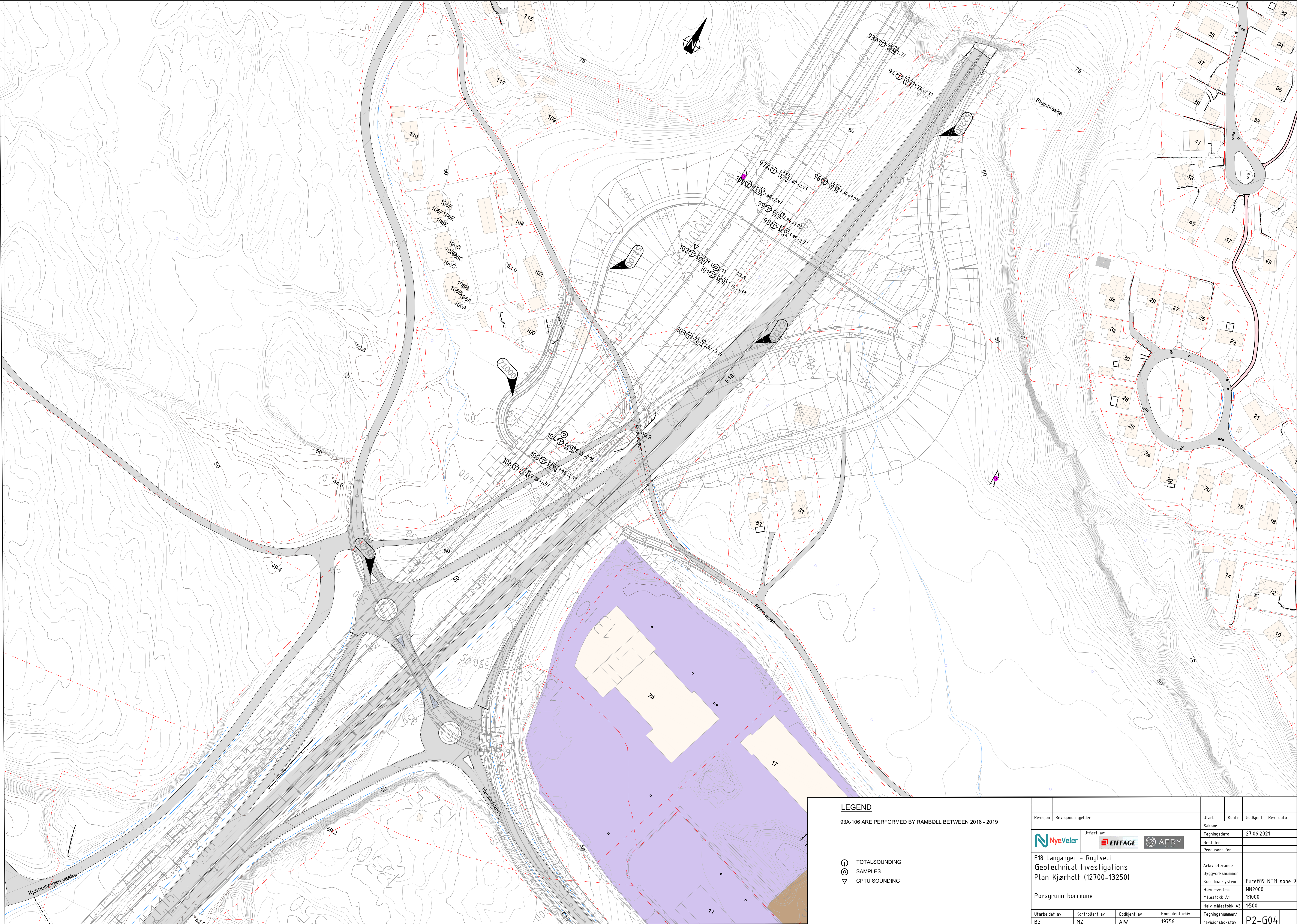


LEGEND

72-75, 740-764 AND 6001-6016 ARE PERFORMED BY RAMBØLL
BETWEEN 2016 - 2019
5001TE IS PERFORMED BY MULTICONSULT IN 2020

- ⊕ TOTALSOUNDING
- ⊙ SAMPLES
- ▽ CPTU SOUNDING

Revisjon	Revisjonen gjelder	Utarb	Kontr	Godkjent	Rev. dato
		Saksnr.			
		Tegningsdato			27.06.2021
		Bestiller			
		Produsert for			
		Arkivreferanse			
		Byggverksnummer			
		Koordinatsystem			Euref89 NTM sone 9
		Høydesystem			NN2000
		Målestokk A1			1:1000
		Halv målestokk A3			1:500
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BG	MZ	Alw	19756		

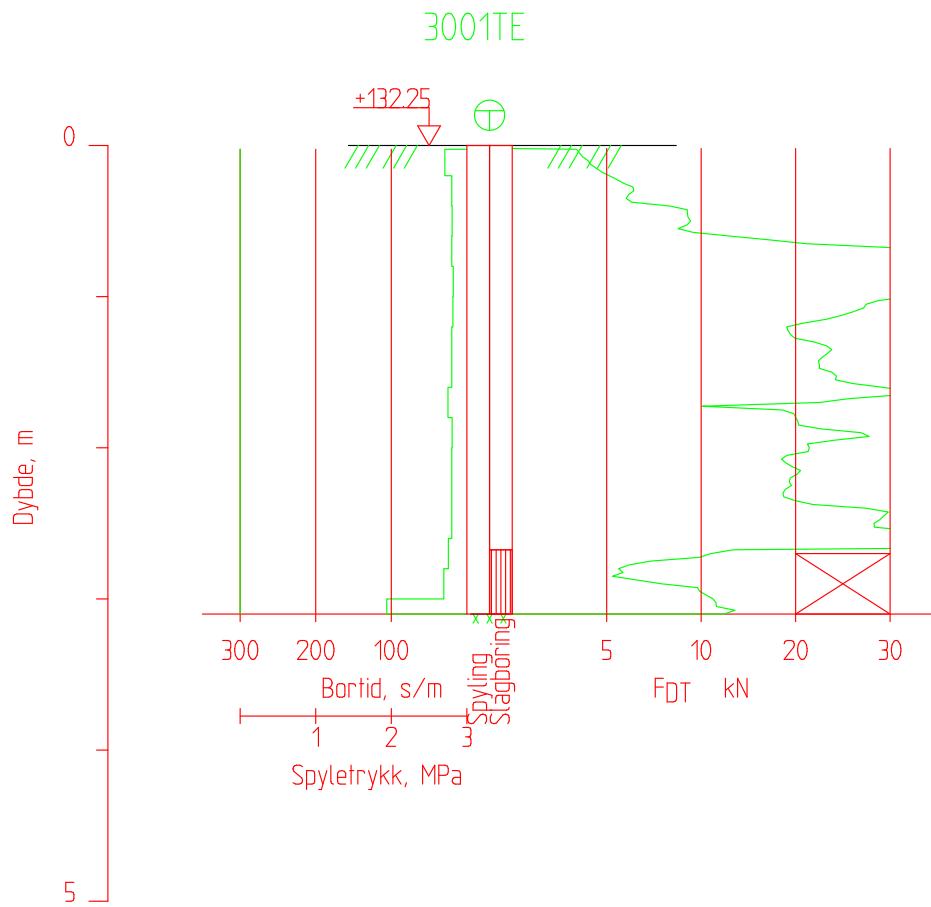


LEGEND

93A-106 ARE PERFORMED BY RAMBØLL BETWEEN 2016 - 2019

- ⊕ TOTALSOUNDING
- ⊙ SAMPLES
- ▽ CPTU SOUNDING

Revisjon	Revisjonen gjelder	Utarb	Kontr	Godkjent	Rev. dato
		Saksnr.			
		Tegningsdato			27.06.2021
		Bestiller			
		Produsert for			
		Arkivreferanse			
		Byggverksnummer			
		Koordinatsystem			Euref89 NTM sone 9
		Høydesystem			NN2000
		Målestokk A1			1:1000
		Halv målestokk A3			1:500
Utarbeidet av	Kontrollert av	Godkjent av	Konsulentarkiv		
BG	MZ	AIW	19756		
		Tegningsnummer/ revisjonsbokstav			P2-G04



Posisjon: X 112334.116 Y 114884.08

Totalsondering

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E18 Langangen Rugtvedt

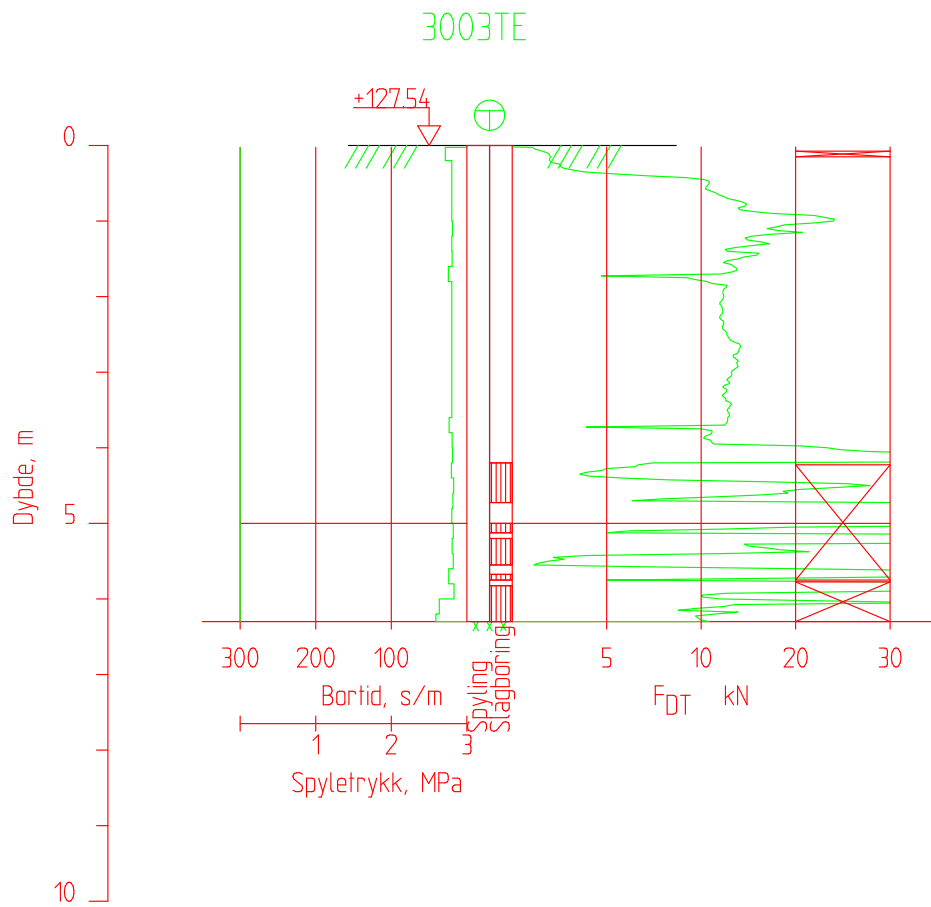
Borhull 3001TE

Dato borete :22.06.2020

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BG

19756



Posisjon: X 1123313.63 Y 114830.45

Totalsondering

Borhull 3003TE

Dato boret :22.06.2020

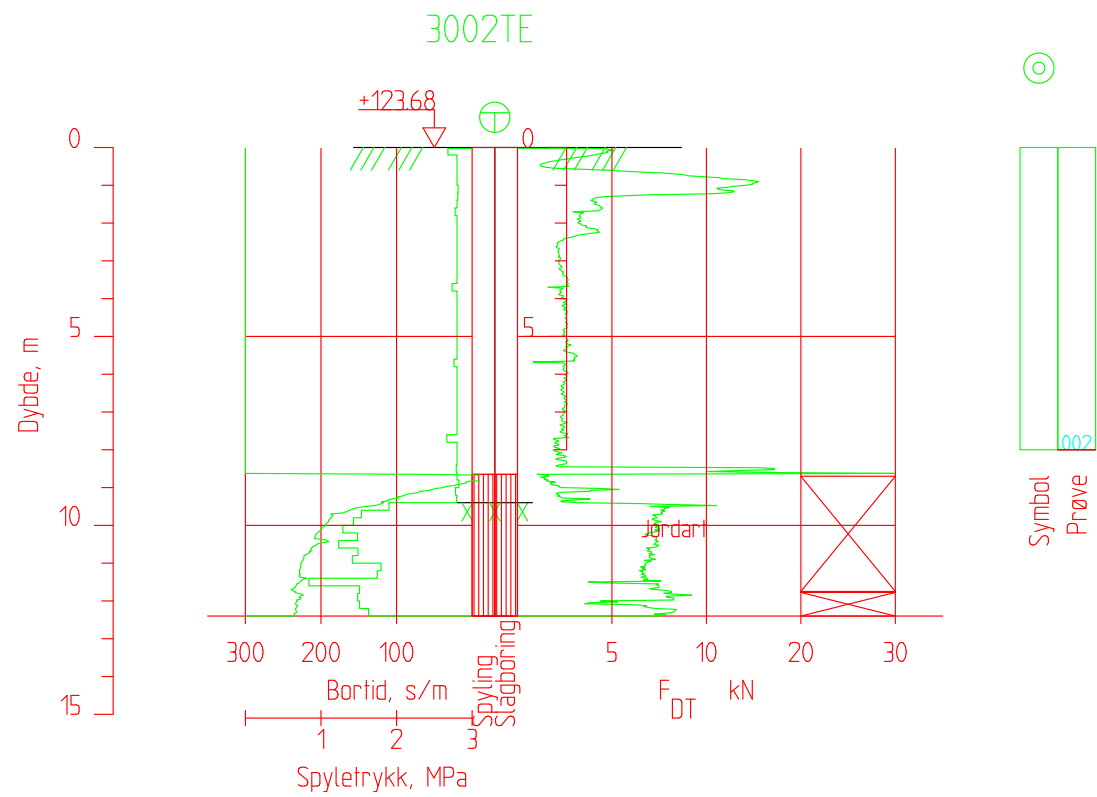
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E18 Langangen Rugtvedt

BG

19756



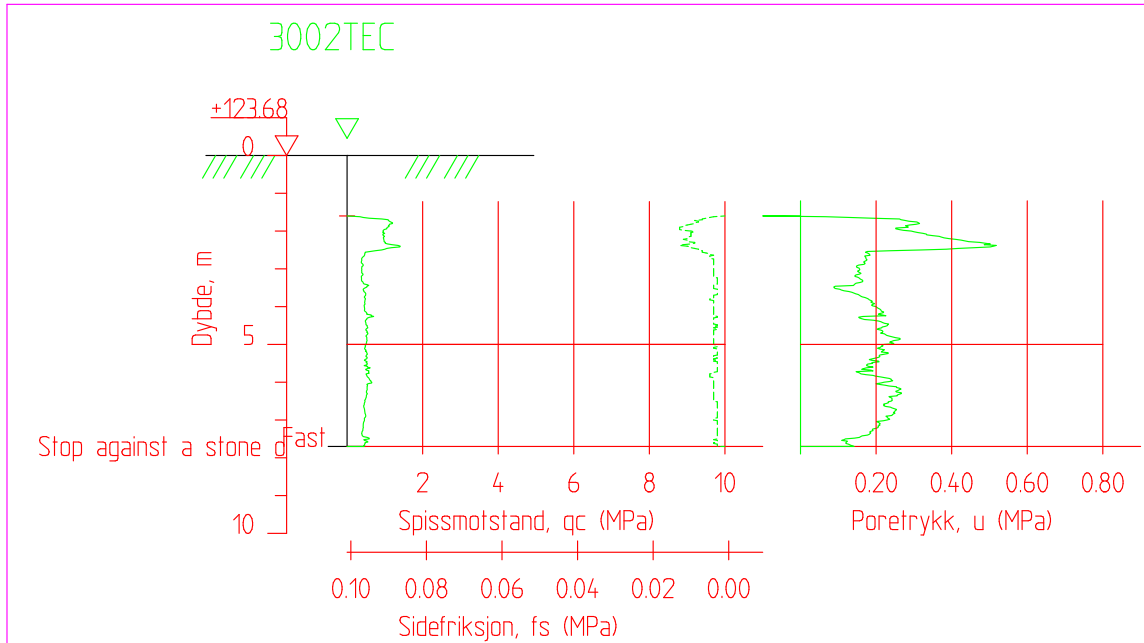
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Totalsondering Borprofil
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E18 Langangen Rugtvedt

Borhull 3002TE

Dato boret :22.06.2020

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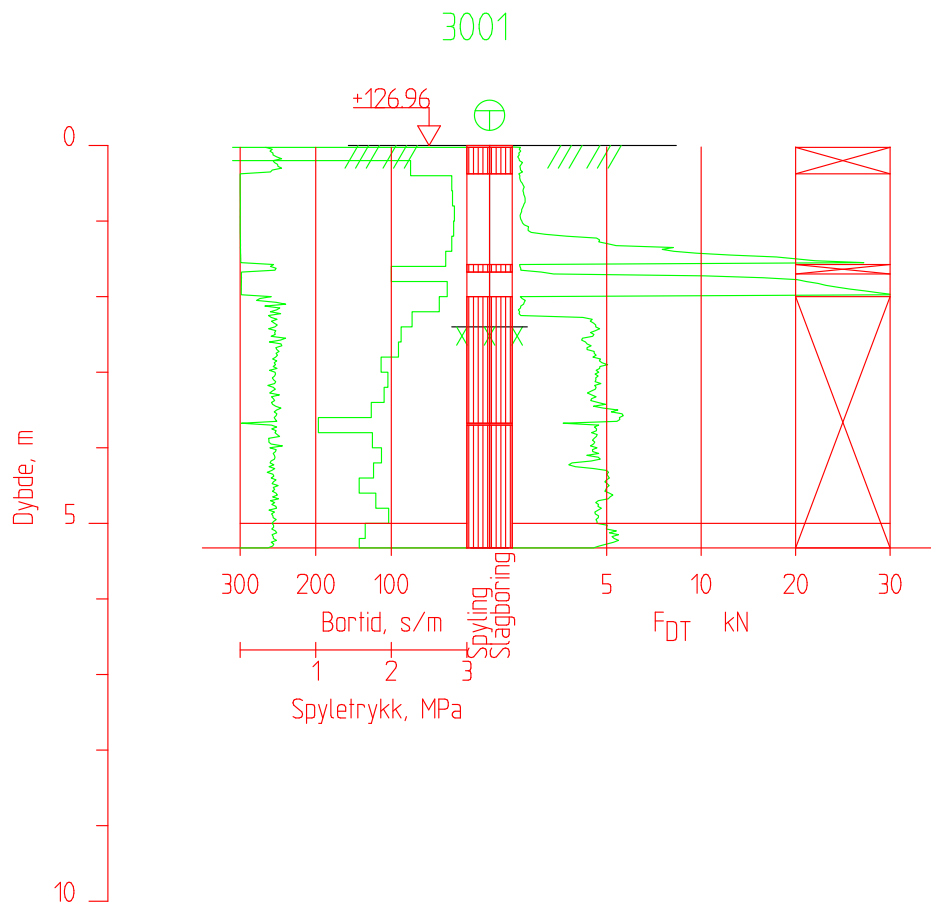


Posisjon: X 1123282.10 Y 114854.40

CPT-sondering
EIFFAGE
E18 Langangen Rugtvedt

Borhull 3002TEC Dato boret :23.06.2020

M = 1 : 200



Posisjon: X 1123141.17 Y 115097.31

Totalsondering

Borhull 3001

Dato boret :27.06.2017

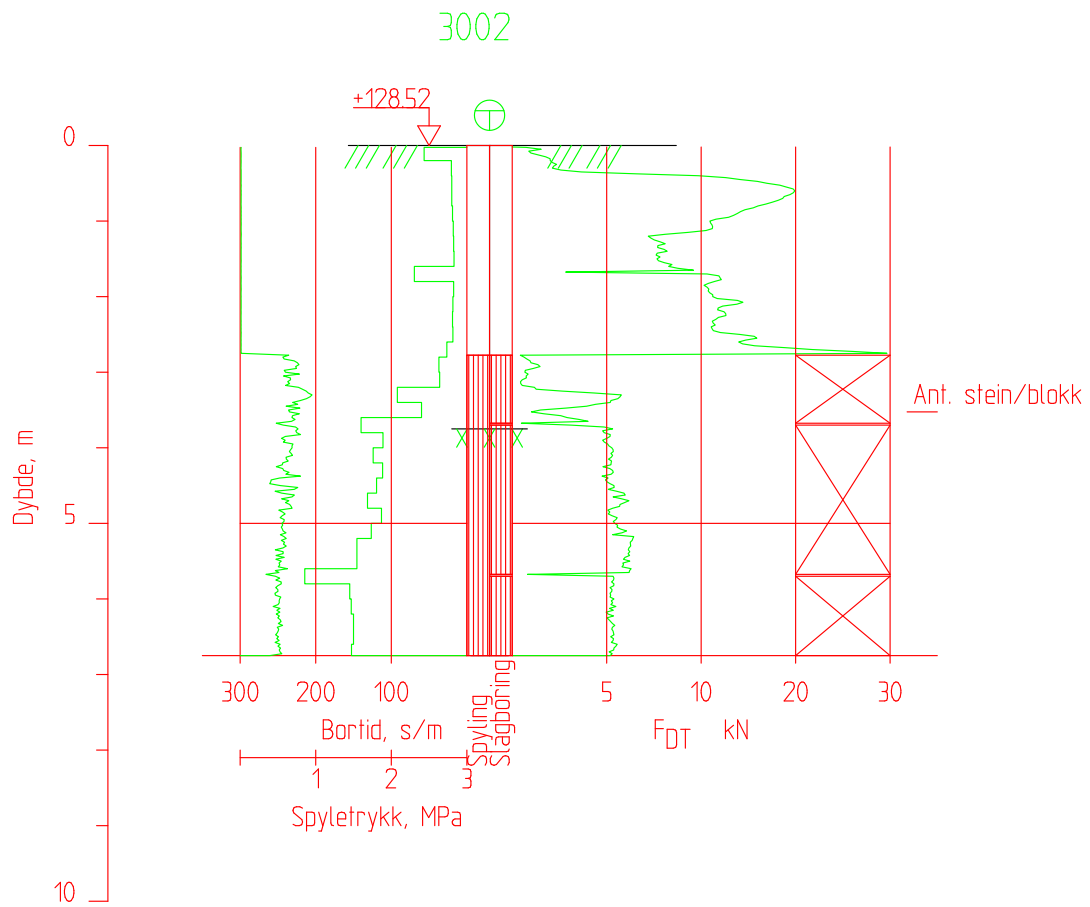
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1123126.07 Y 115109.42

Totalsondering

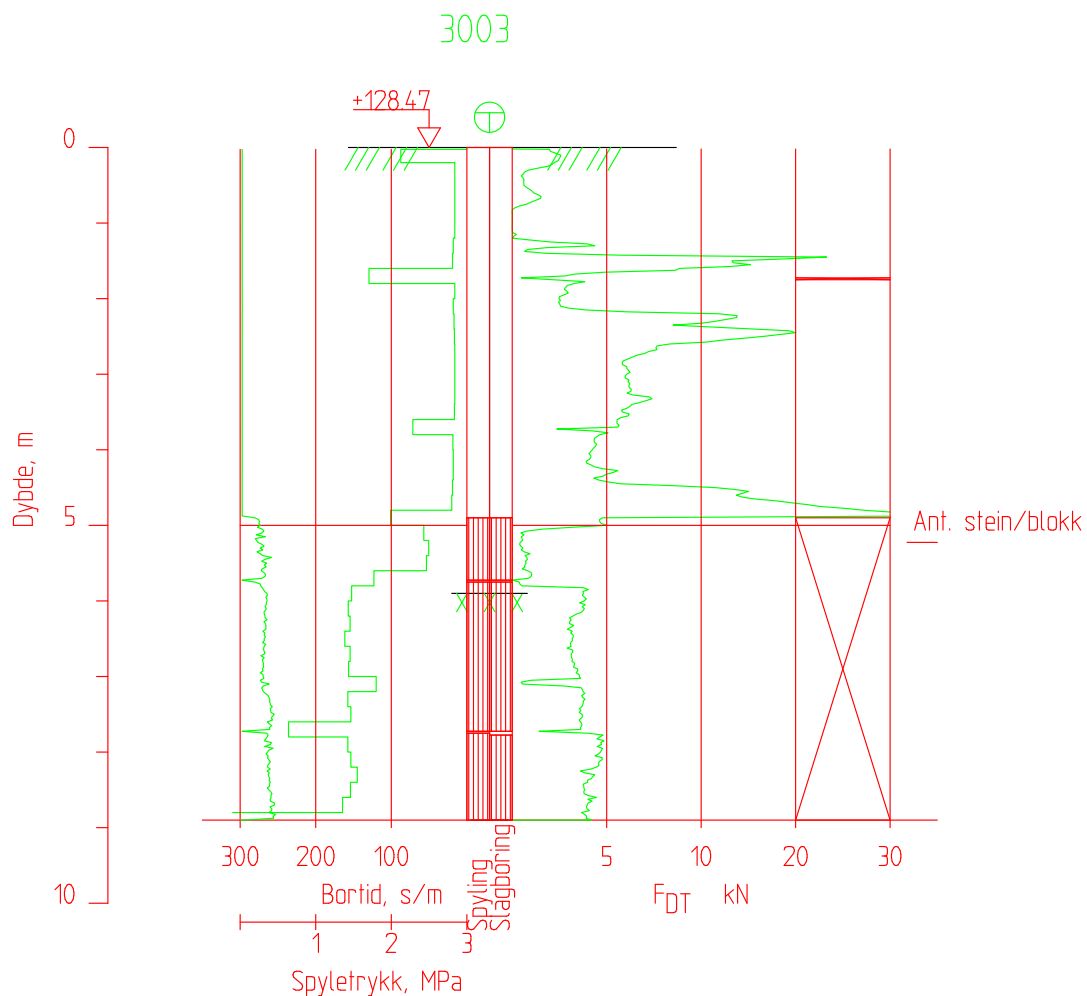
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E18 Langangen Rugtvedt

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Totalsondering

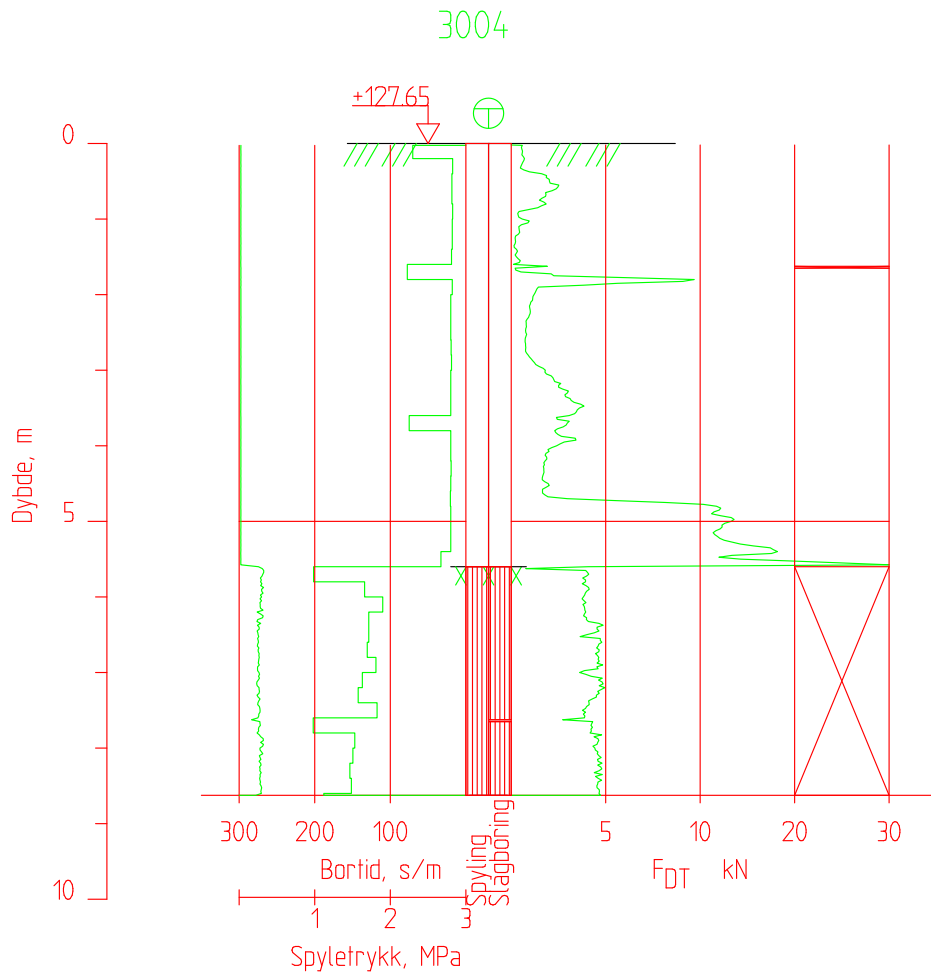
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E18 Langangen Rugtvedt

Borhull 3003

Dato boret :27.06.2017

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Posisjon: X 1123099.81 Y 115139.97

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

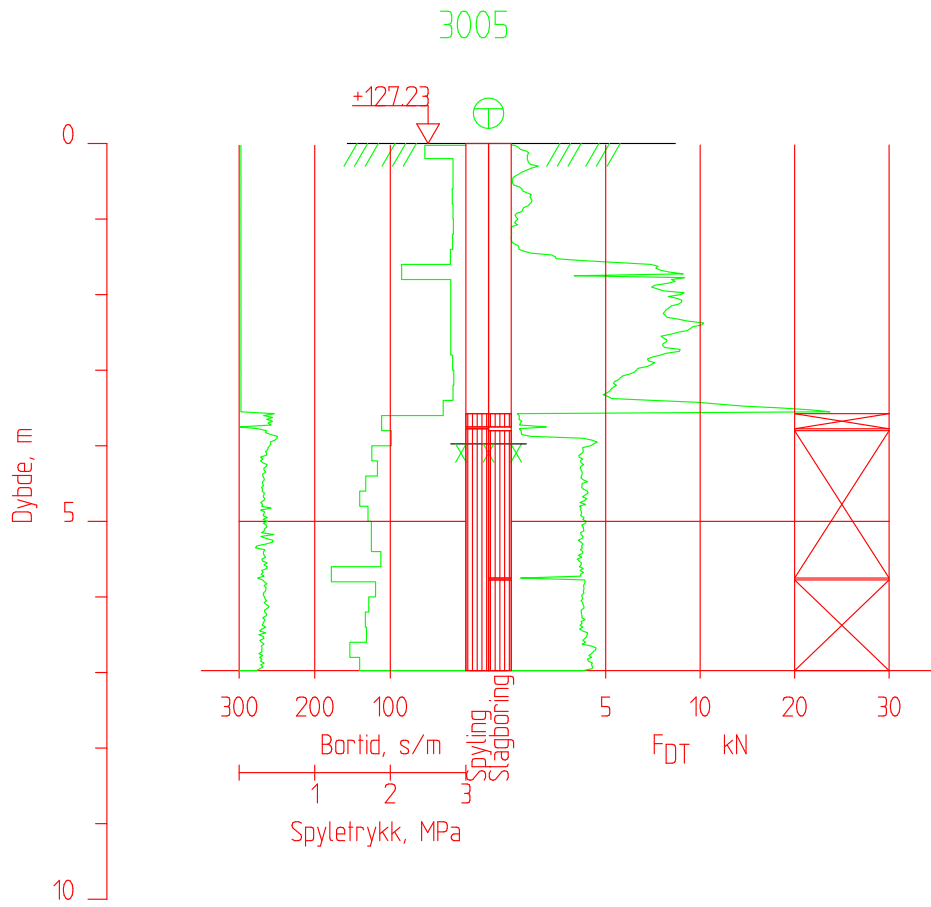
Borhull 3004

Dato boret :26.06.2017

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BG

19756



Posisjon: X 1123078.07 Y 115160.24

Totalsondering

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E18 Langangen Røgtvedt

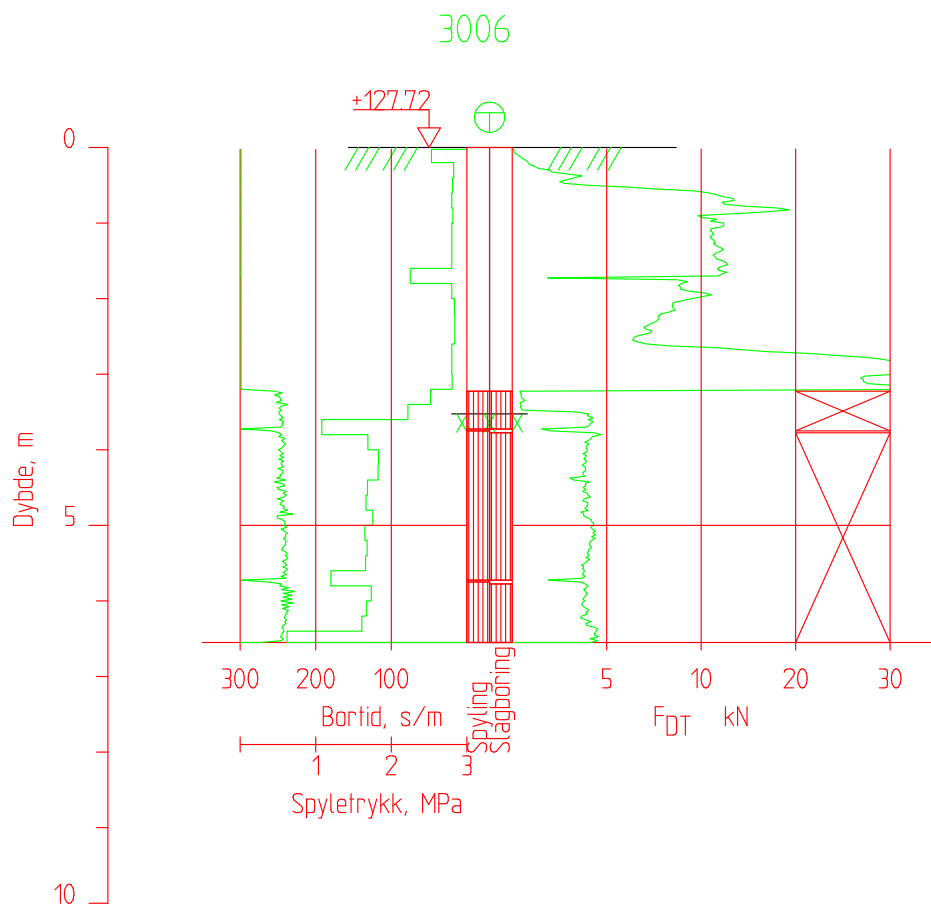
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Dato boret :26.06.2017

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BG

19756



Posisjon: X 1123055.72 Y 115180.26

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

Borhull 3006

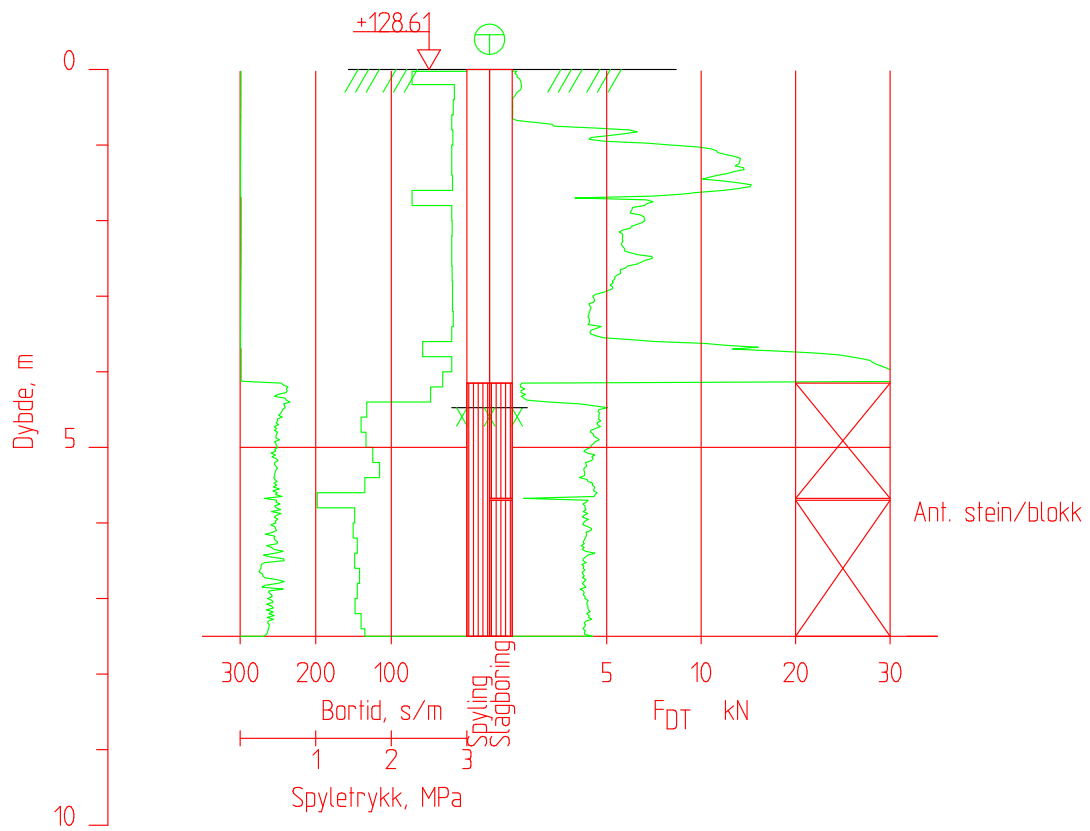
Dato borete :26.06.2017

M = 1 : 100

BG

19756

3007



Posisjon: X 1123022.62 Y 115218.38

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

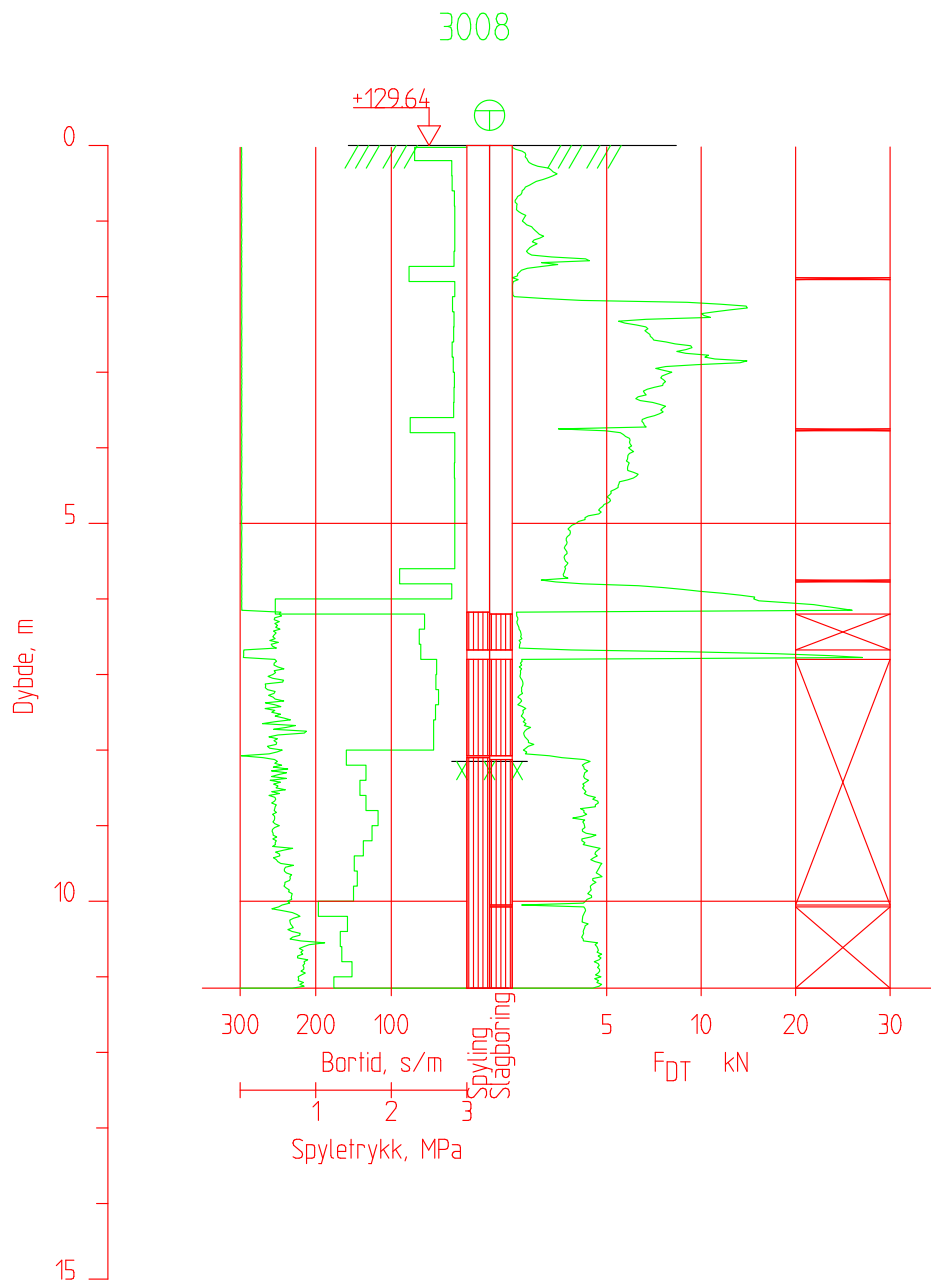
Borhull 3007

Dato boreal :26.06.2017

$M = 1 : 100$

BG

19756



Posisjon: X 1122992.47 Y 115245.13

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

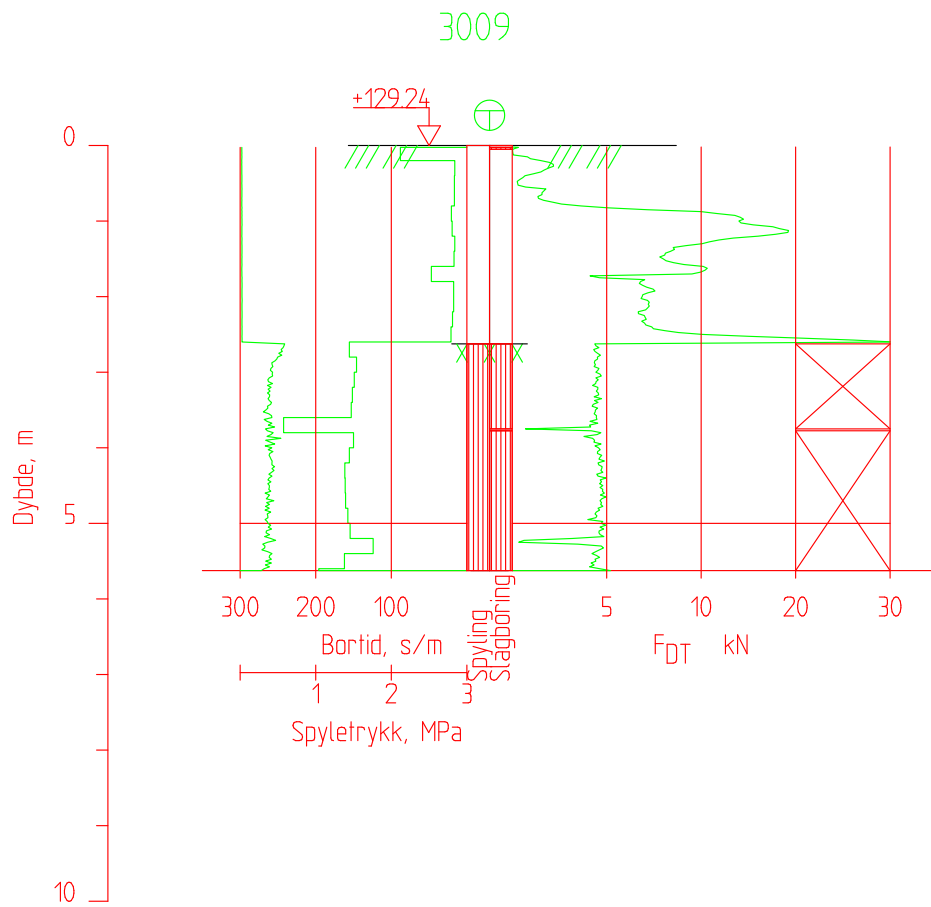
Borhull 3008

Dato boret :26.06.2017

M = 1 : 100

BG

19756



Posisjon: X 1122961.71 Y 115267.37

Totalsondering

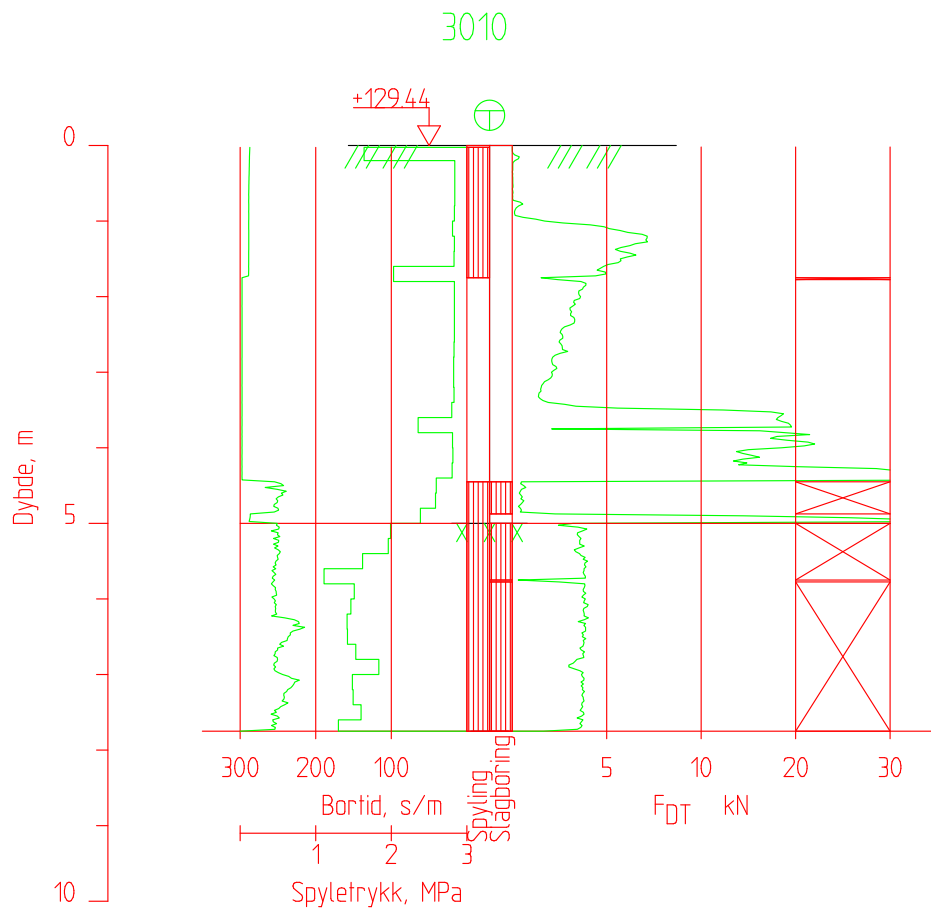
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E18 Langangen Rugtvedt

Borhull 3009

Dato boret :26.06.2017

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Posisjon: X 1122929.53 Y 115293.64

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

Borhull 3010

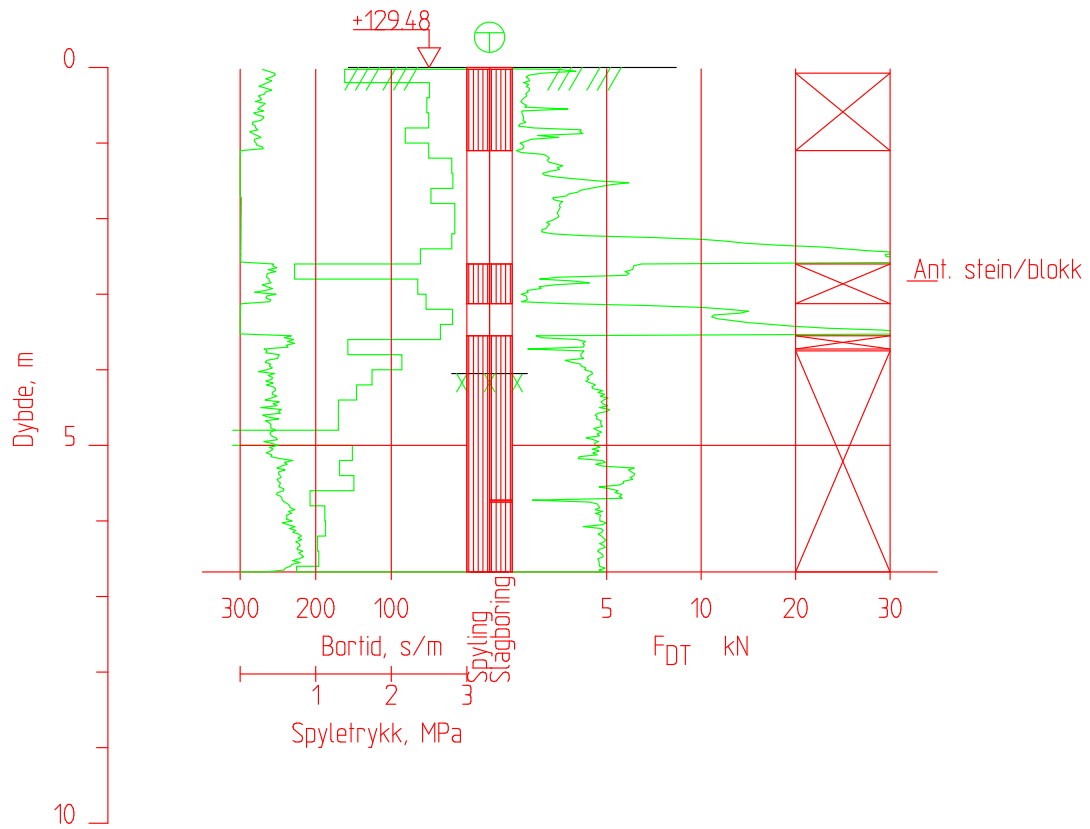
Dato borete :26.06.2017

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BG

19756

3011



Posisjon: X 1122896.86 Y 115316.81

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

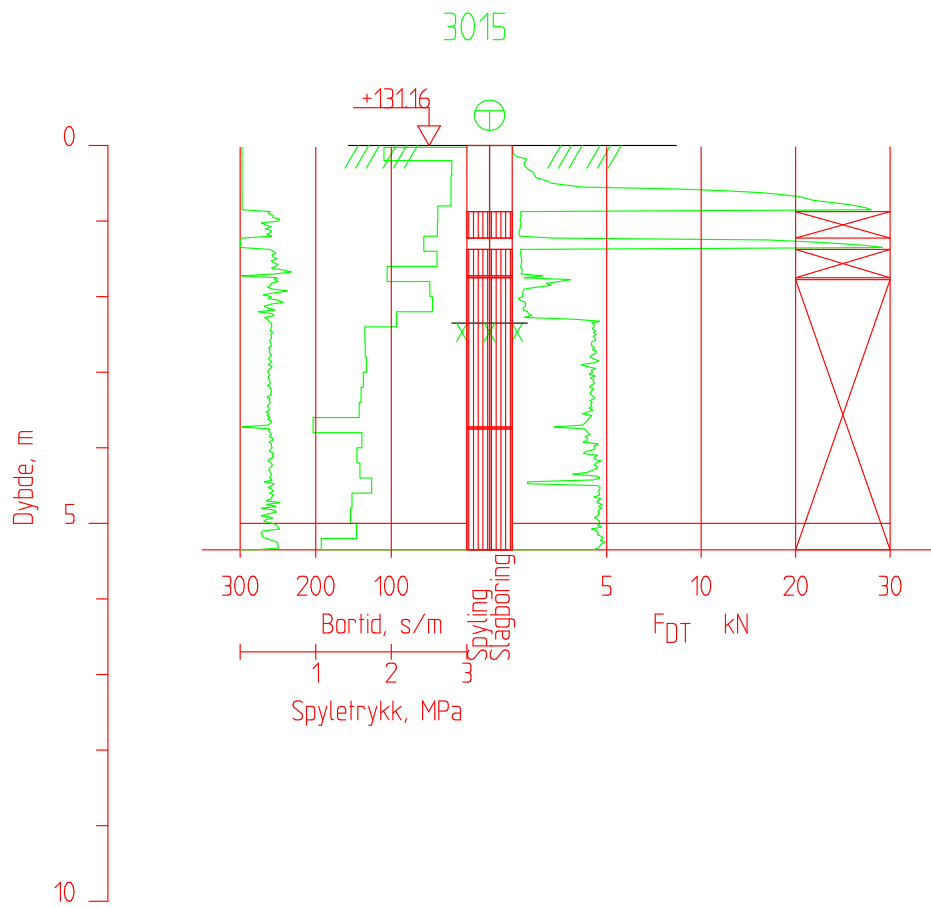
Borhull 3011

Dato boret :22.06.2017

M = 1 : 100

BG

19756



Posisjon: X 1123220.05 Y 114961.10

Totalsondering

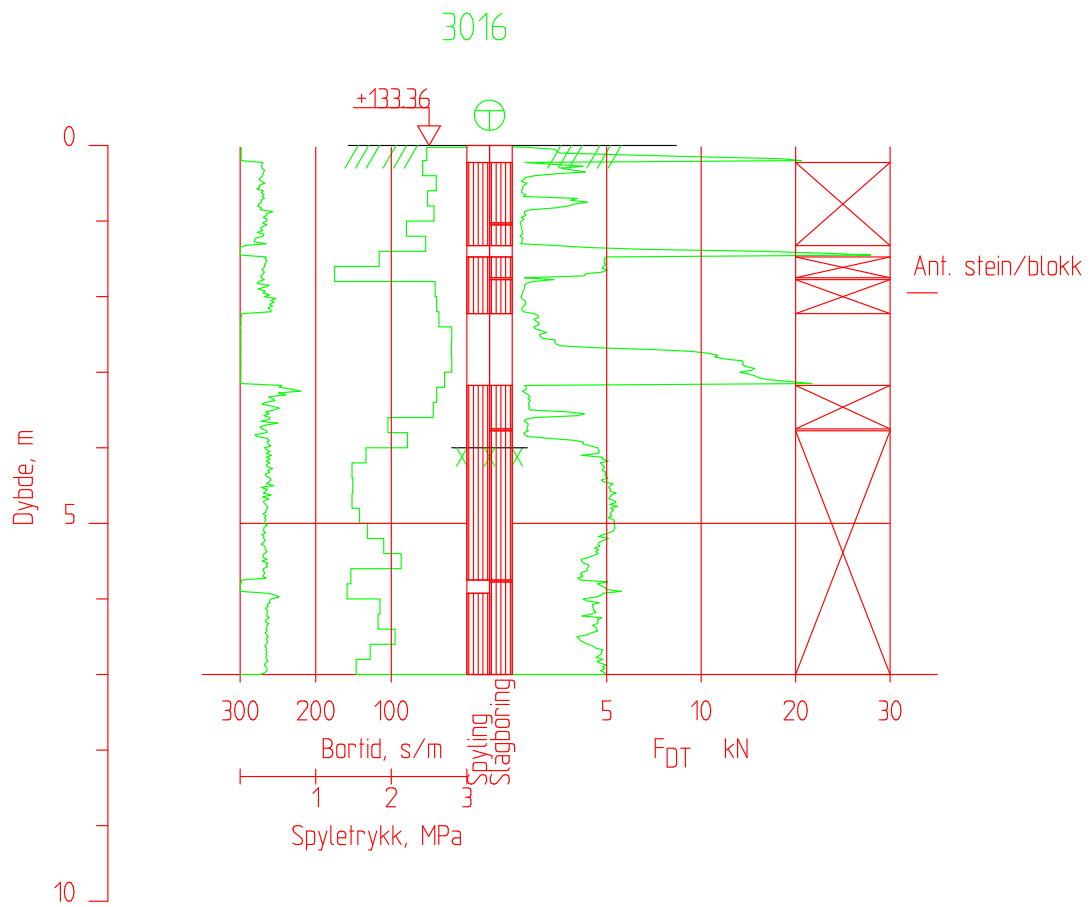
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E18 Langangen Rugtvedt

Borhull 3015

Dato borete :27.06.2017

M = 1 : 100



Posisjon: X 1123221.62 Y 114932.44

Totalsondering

Borhull 3016

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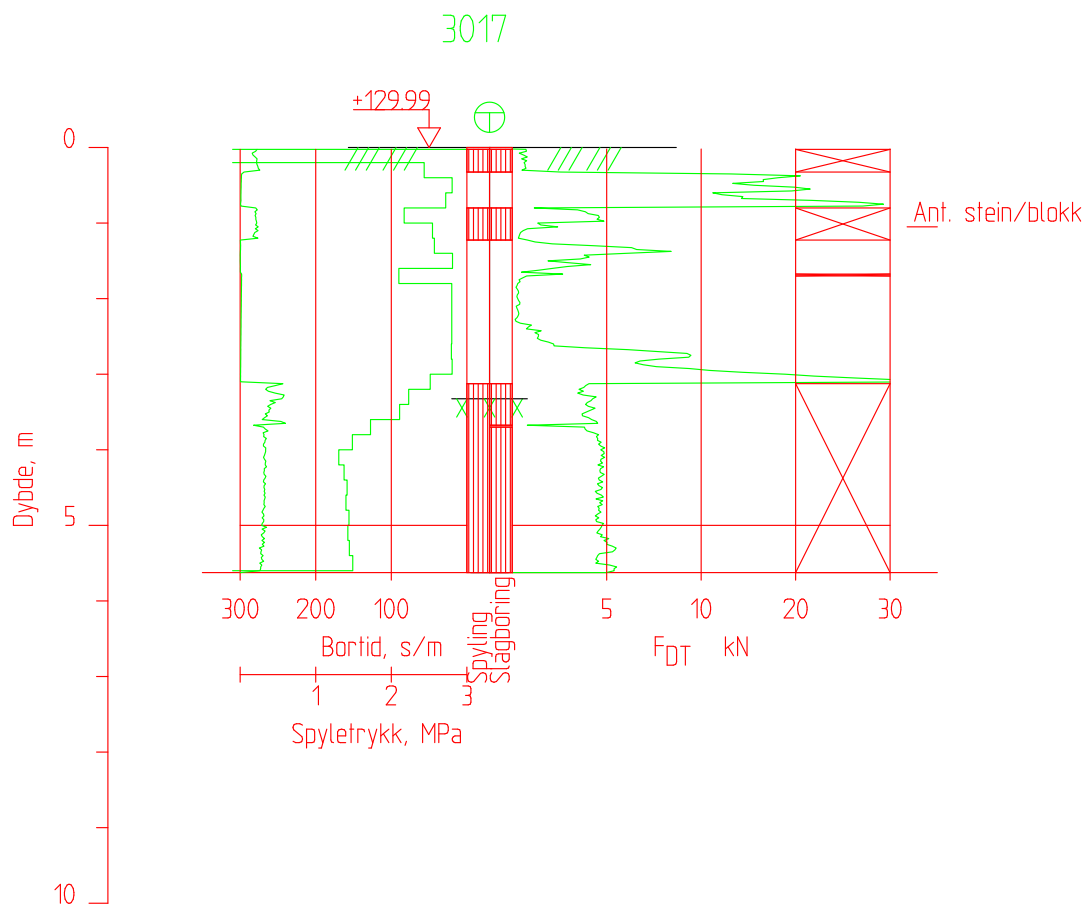
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1123222.93 Y 114882.04

Totalsondering

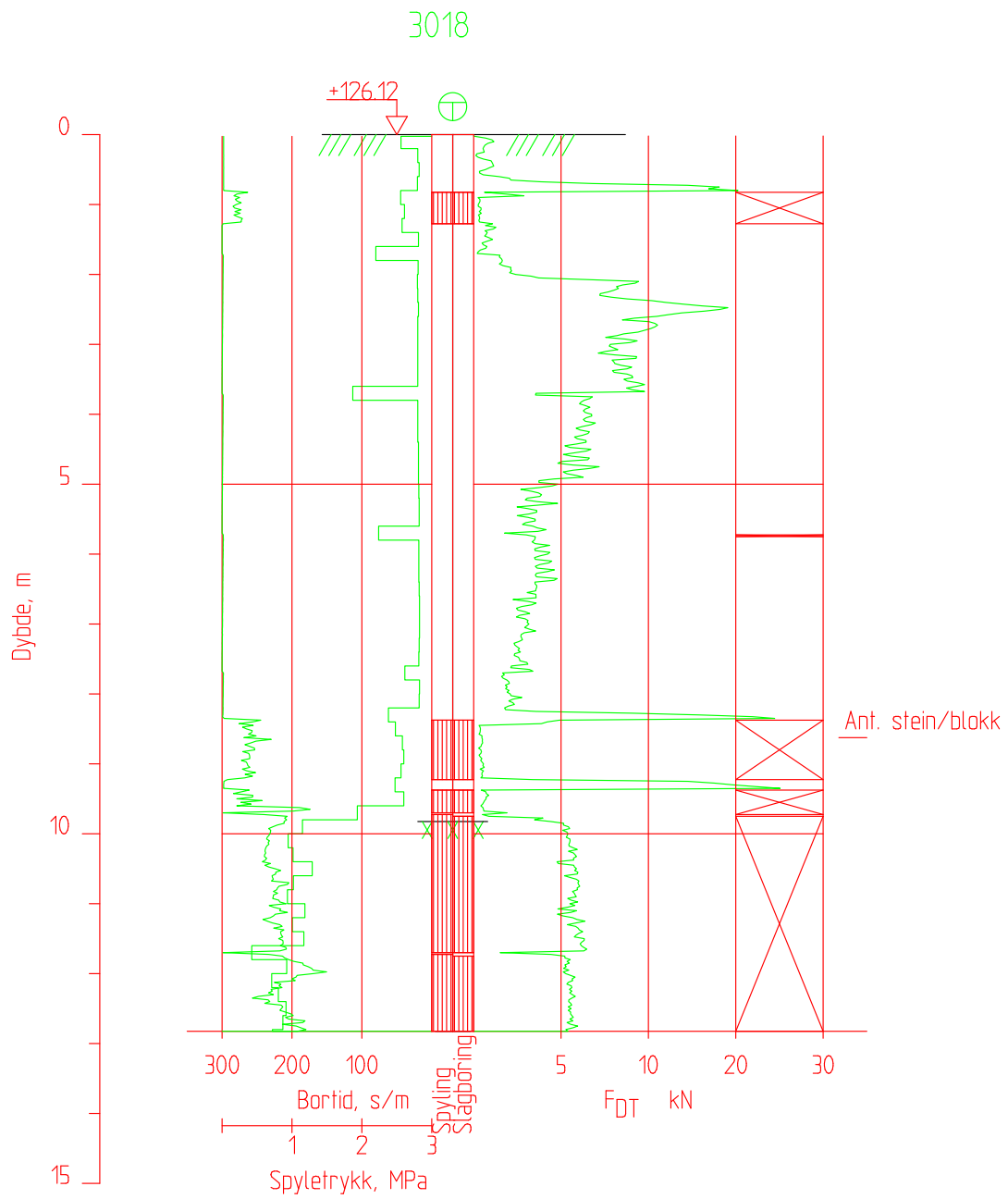
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E18 Langangen Rugtvedt

Borhull 3017

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M = 1 : 100



Posisjon: X 1123229.52 Y 114849.31

Totalsondering

Borhull 3018

Dato boret :27.06.2017

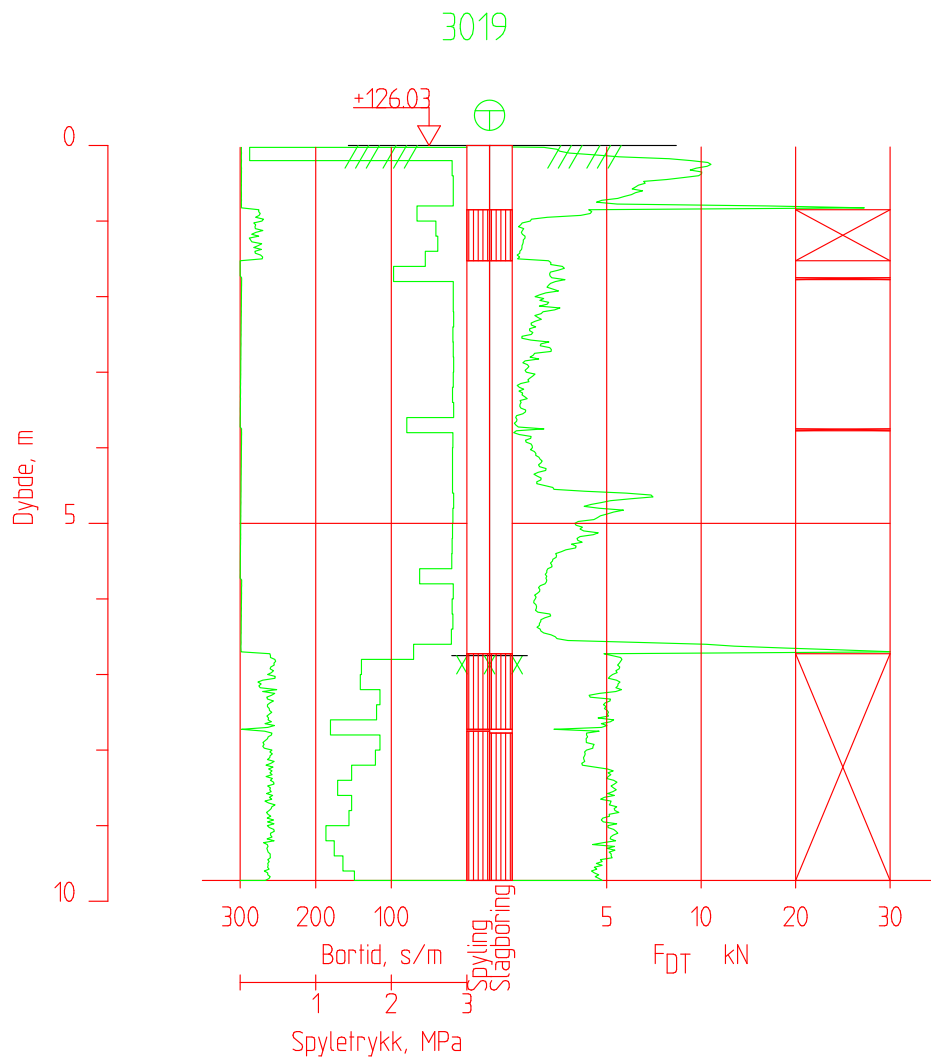
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1123222.63 Y 114820.72

Totalsondering

Borhull 3019

Dato borete :27.06.2017

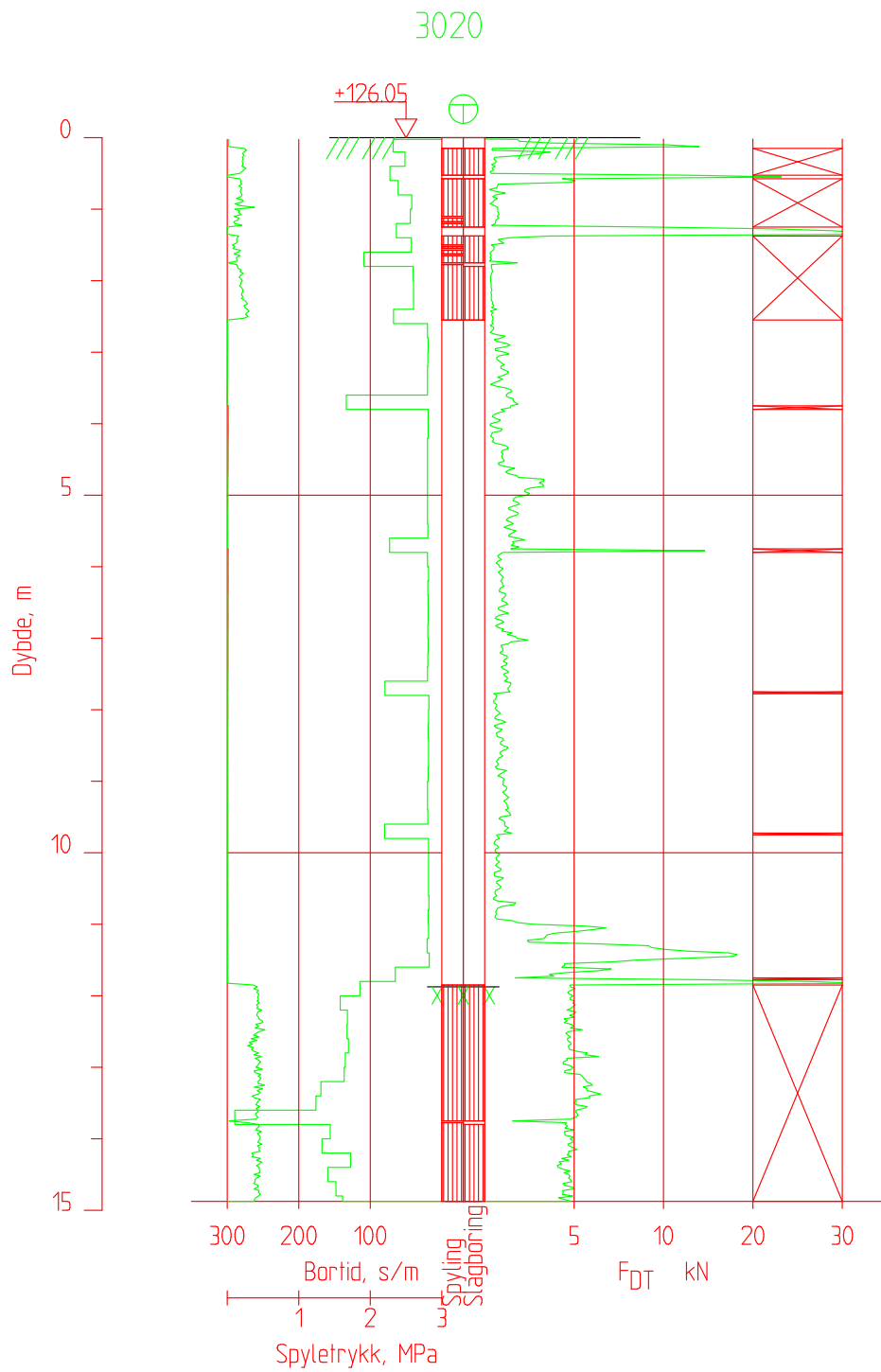
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1123063.43 Y 115114.29

Totalsondering

Borhull 3020

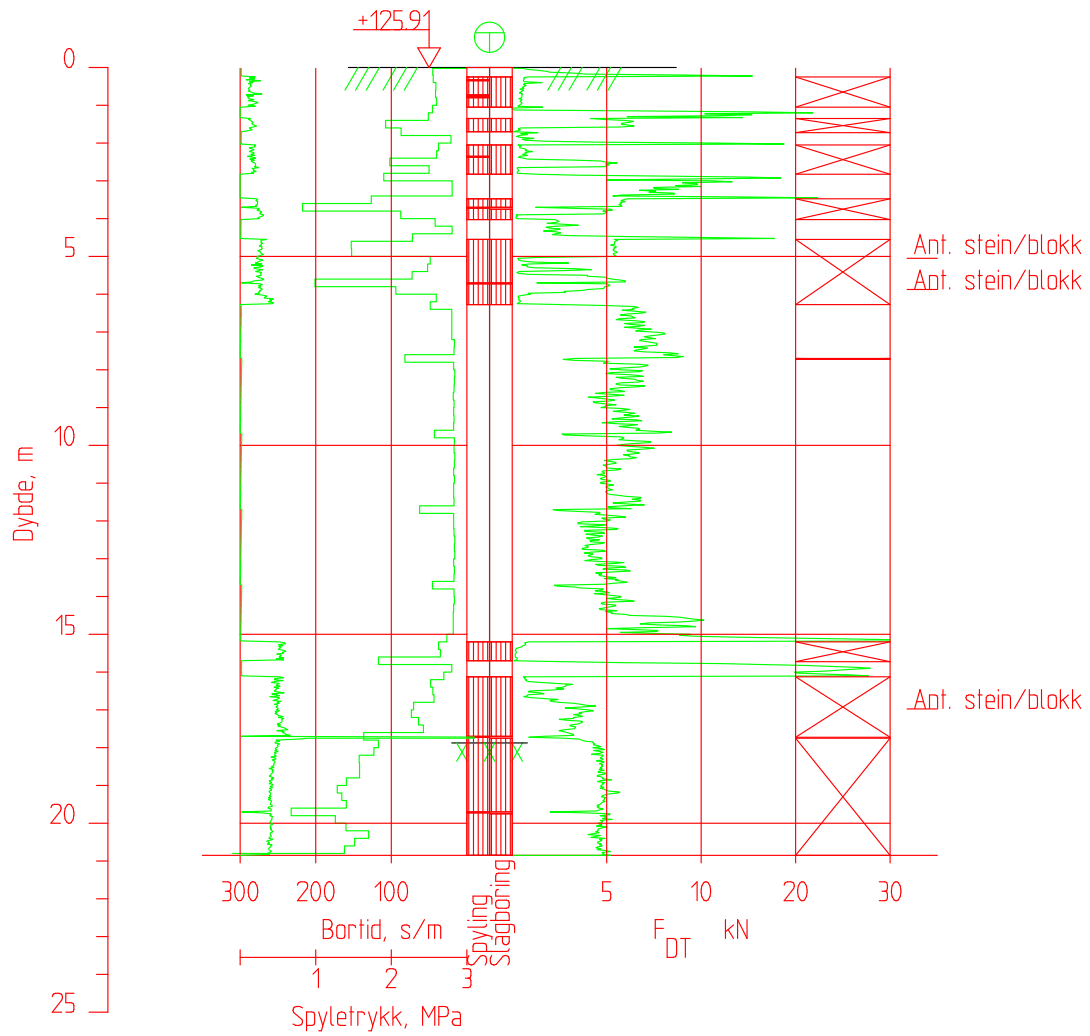
Dato boret :27.06.2017

EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

3021



Posisjon: X 1123046.82 Y 115124.92

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

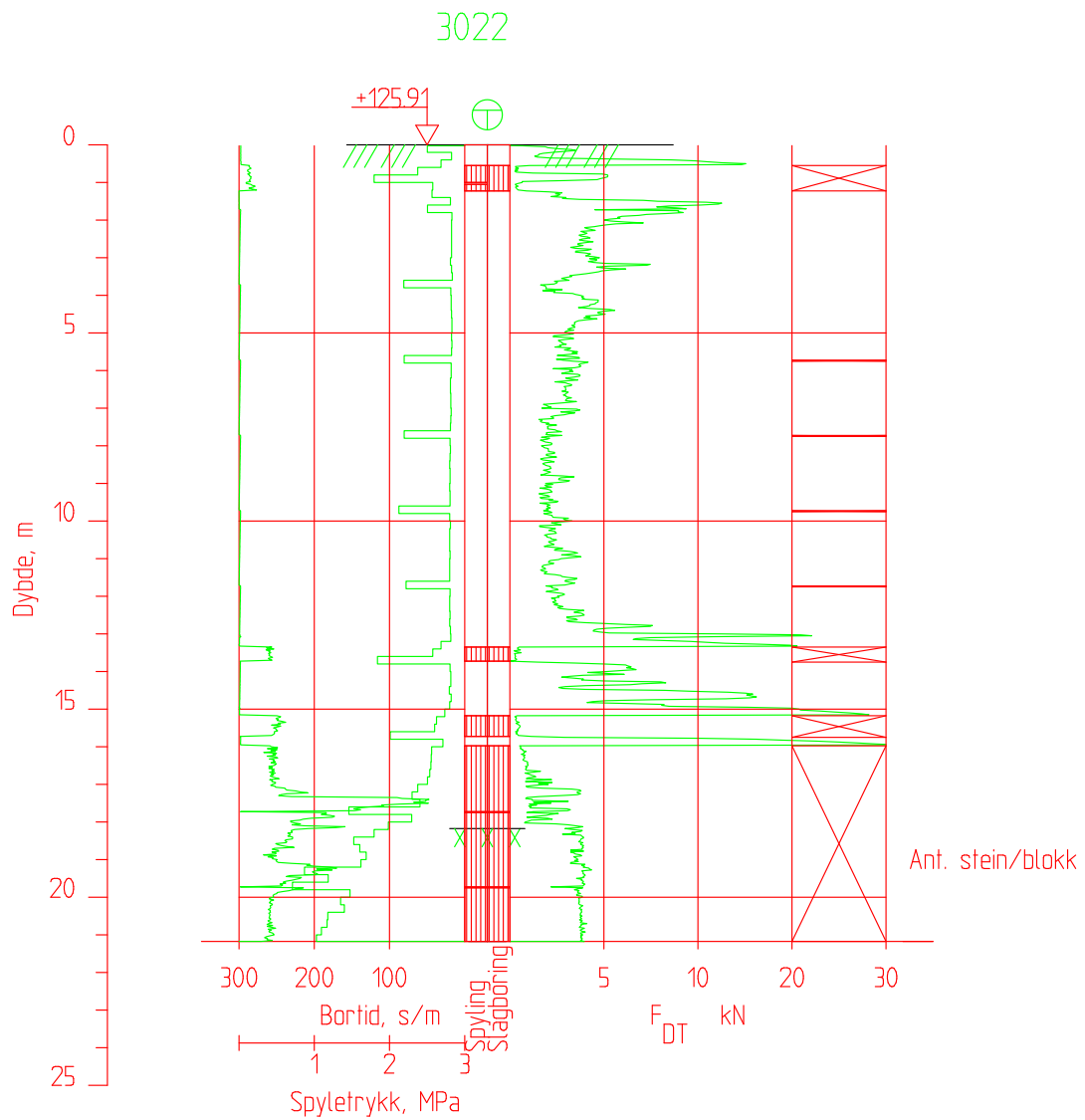
Borhull 3021

Dato boret :27.06.2017

$M = 1 : 200$

BG

19756



Posisjon: X 1123021.77 Y 115139.37

Totalsondering

Borhull 3022

Dato boret :28.06.2017

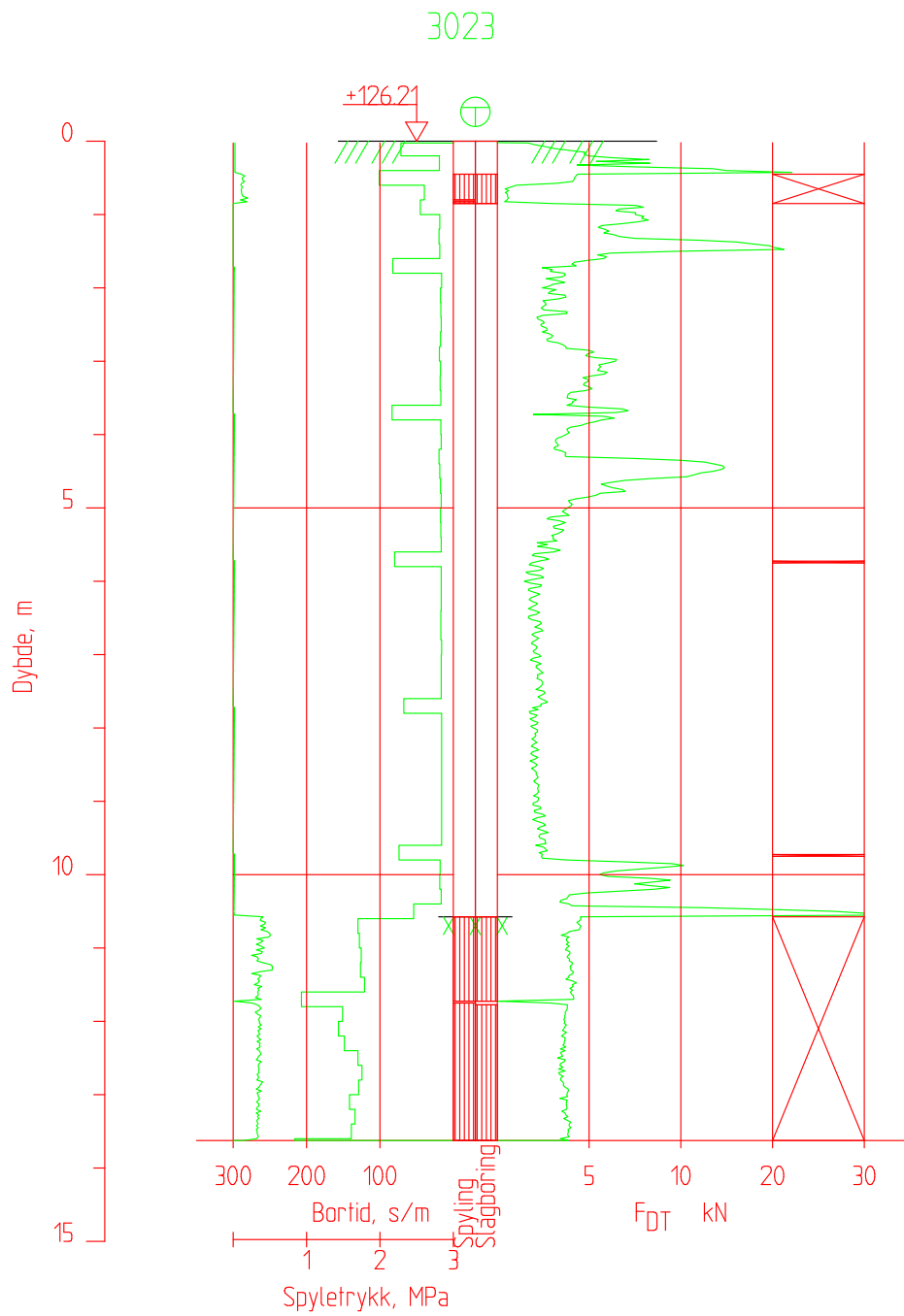
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122995.55 Y 115157.98

Totalsondering

Borhull 3023

Dato boret :28.06.2017

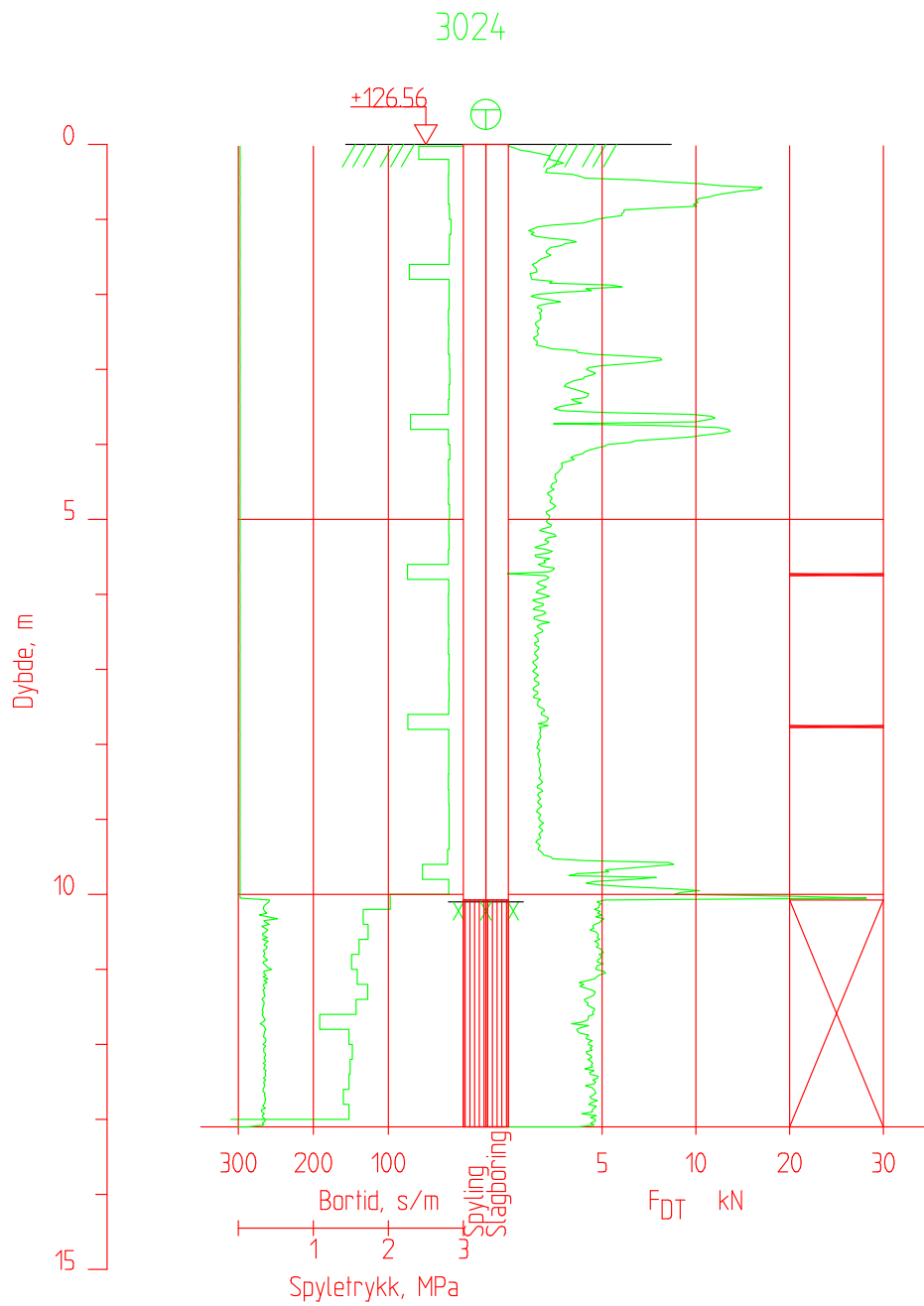
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122977.61 Y 115167.42

Totalsondering

Borhull 3024

Dato boret :28.06.2017

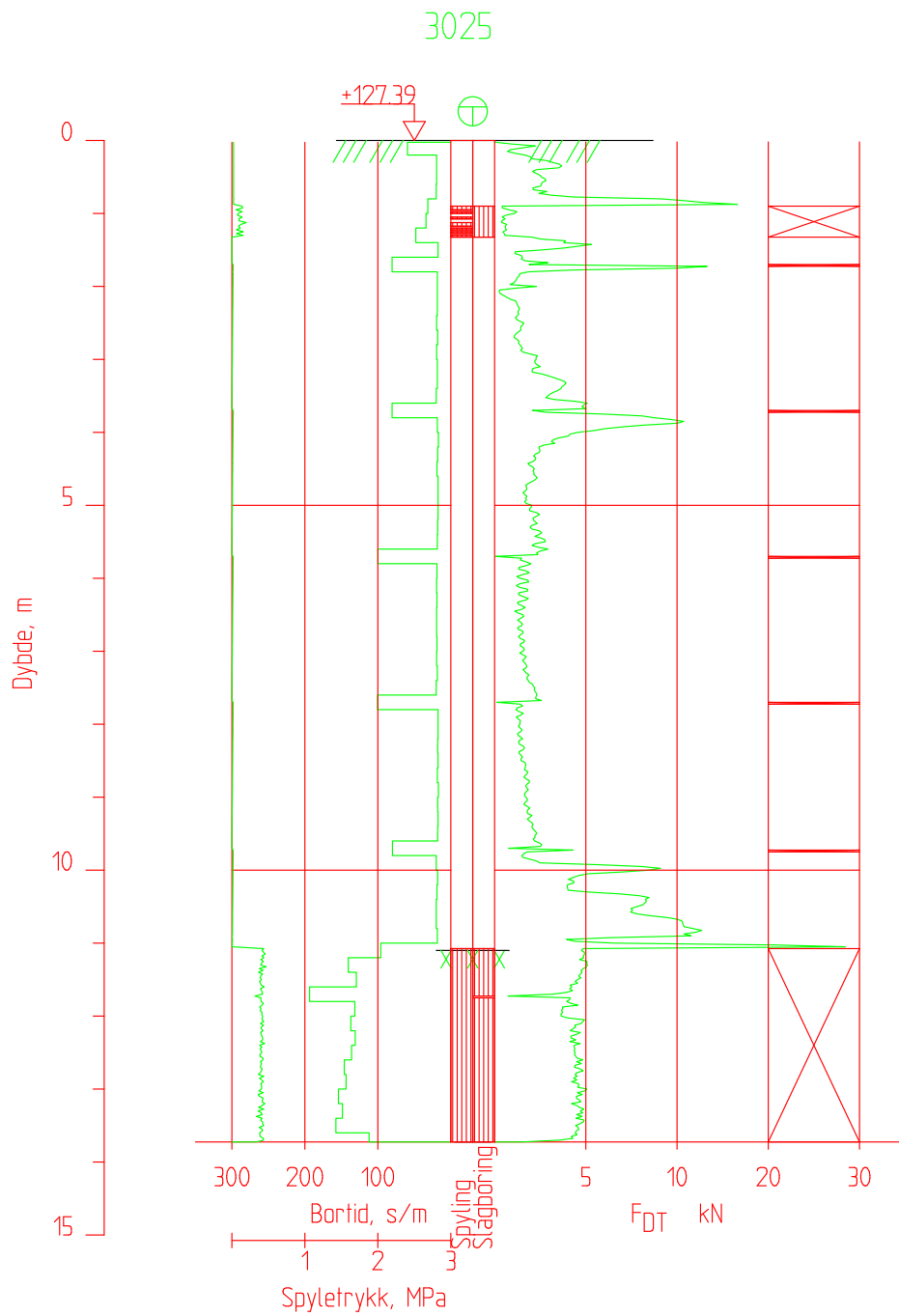
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122958.89 Y 115177.28

Totalsondering

Borhull 3025

Dato boret :28.06.2017

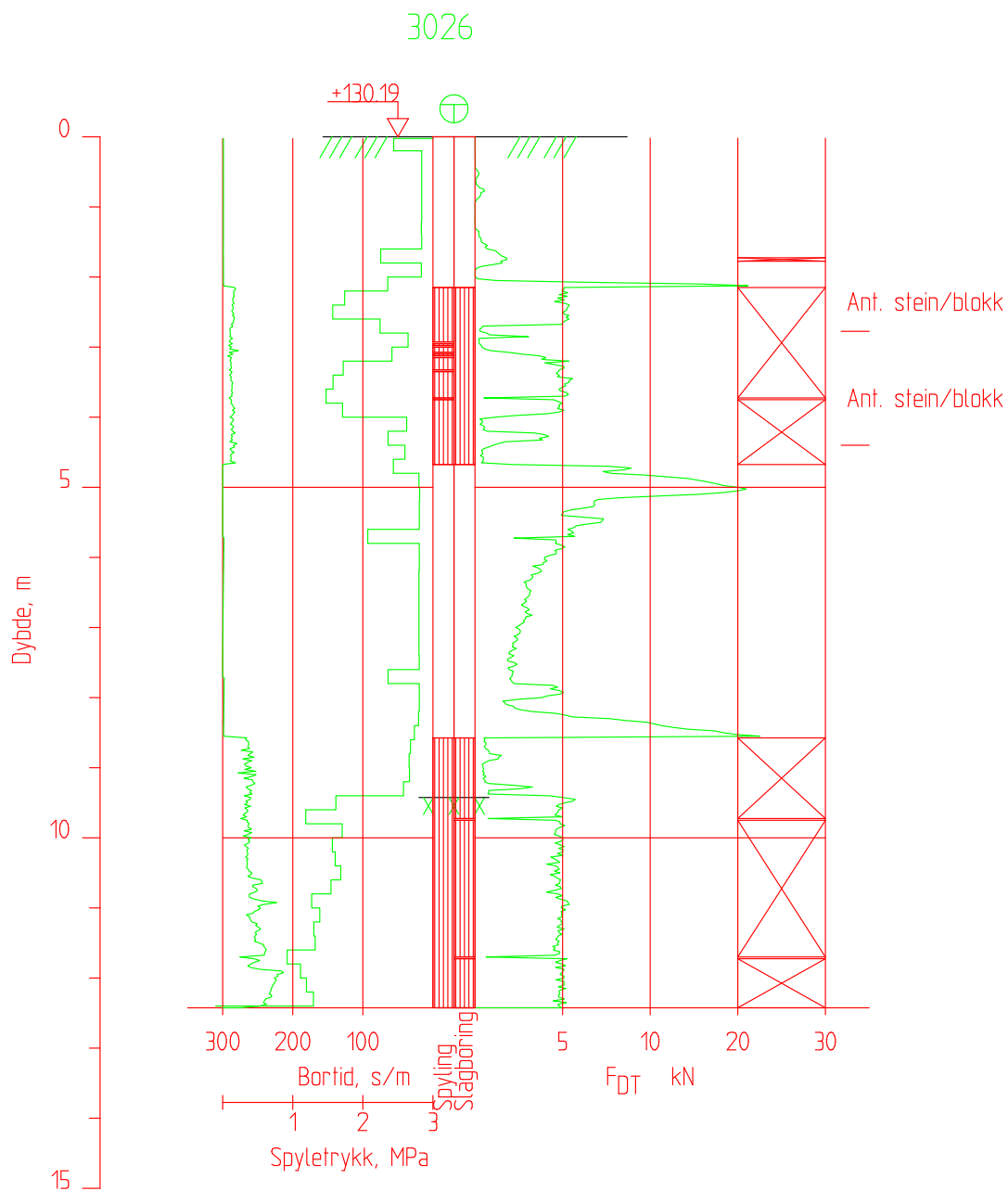
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122928.25 Y 115199.01

Totalsondering

Borhull 3026

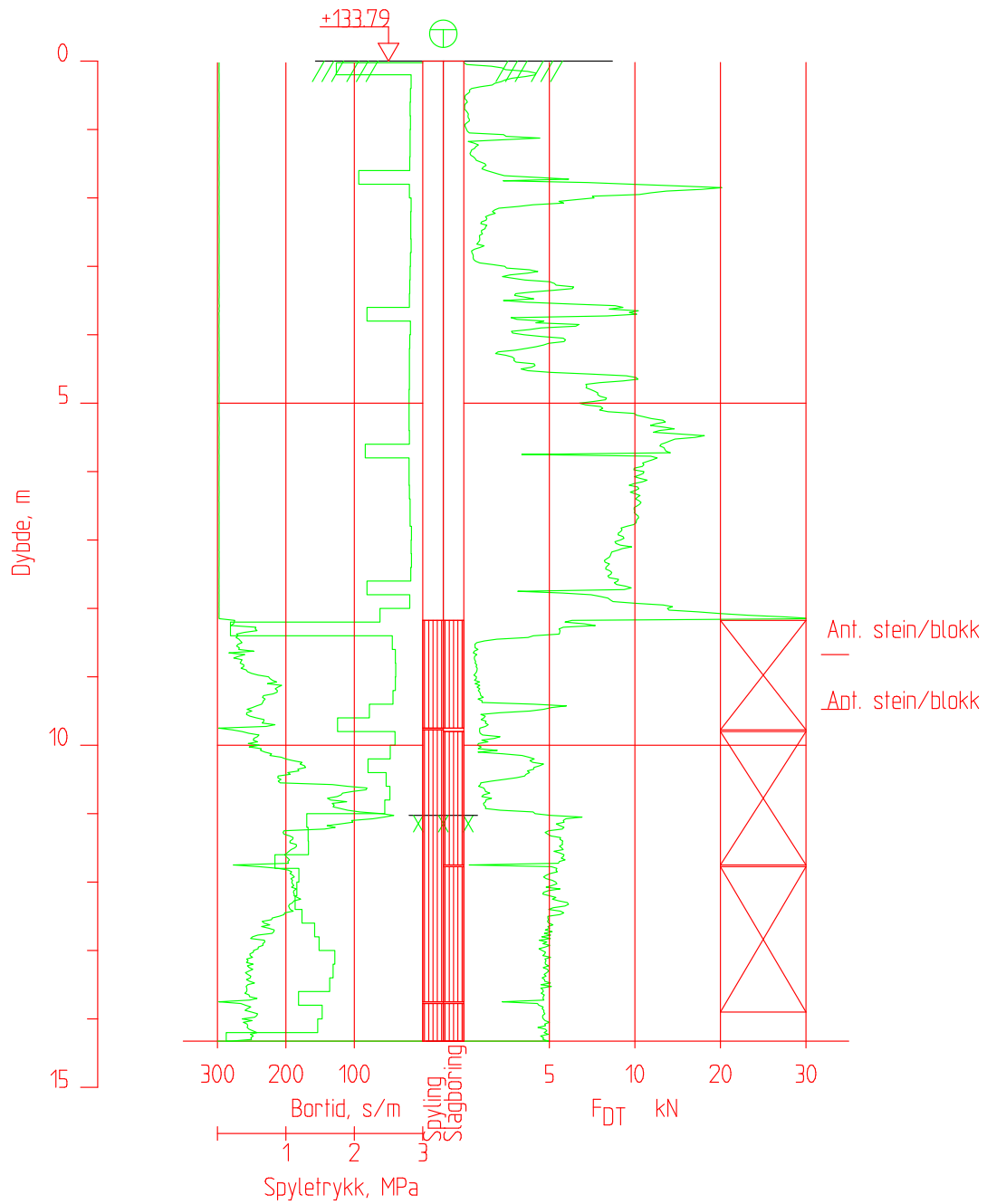
Dato boret :28.06.2017

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M = 1 : 100

E18 Langangen Rugtvedt

3027



Posisjon: X 1122896.20 Y 115234.71

Totalsondering

Borhull 3027

Dato boret :28.06.2017

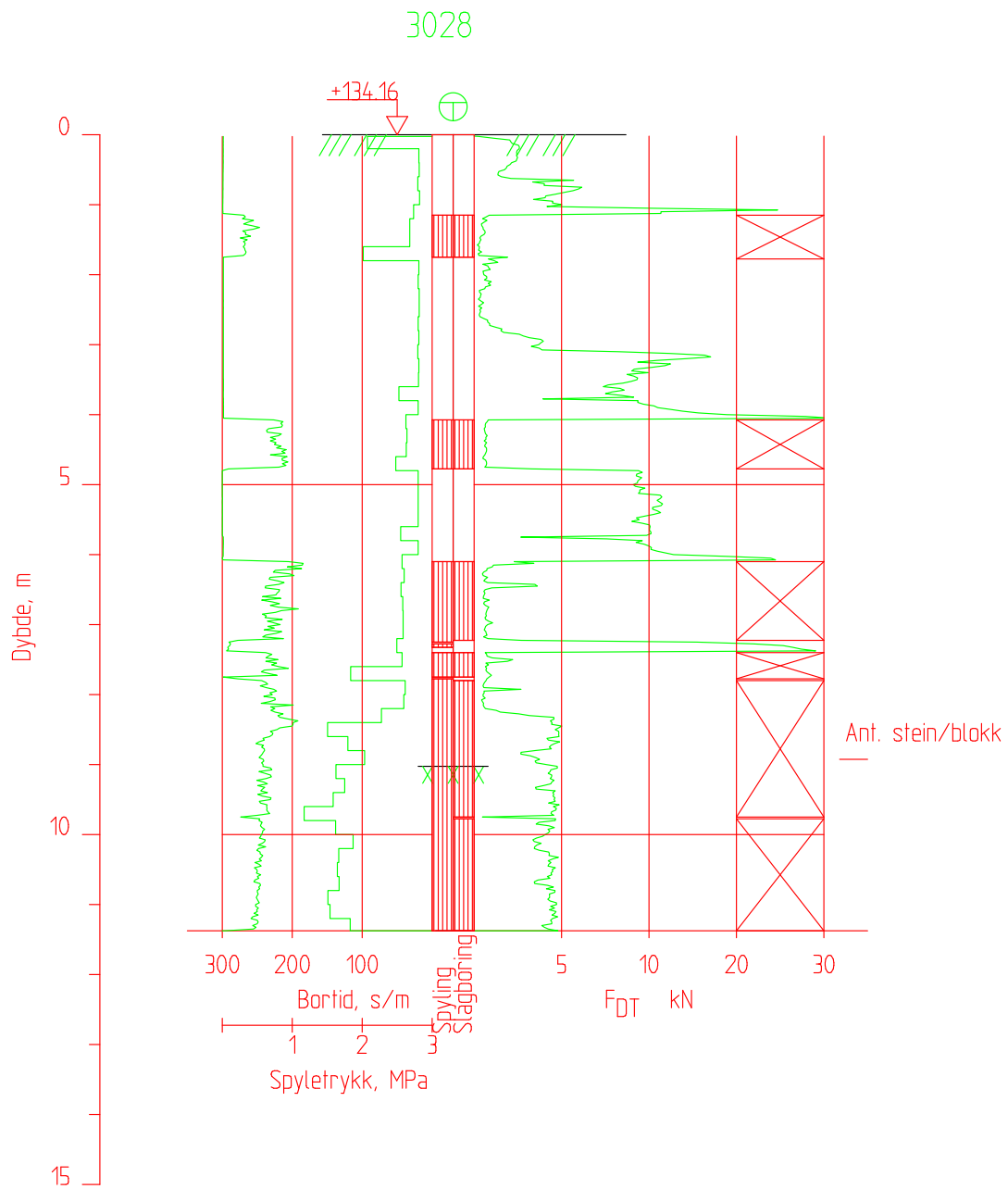
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122871.39 Y 115265.85

Totalsondering

Borhull 3028

Dato boret :28.06.2017

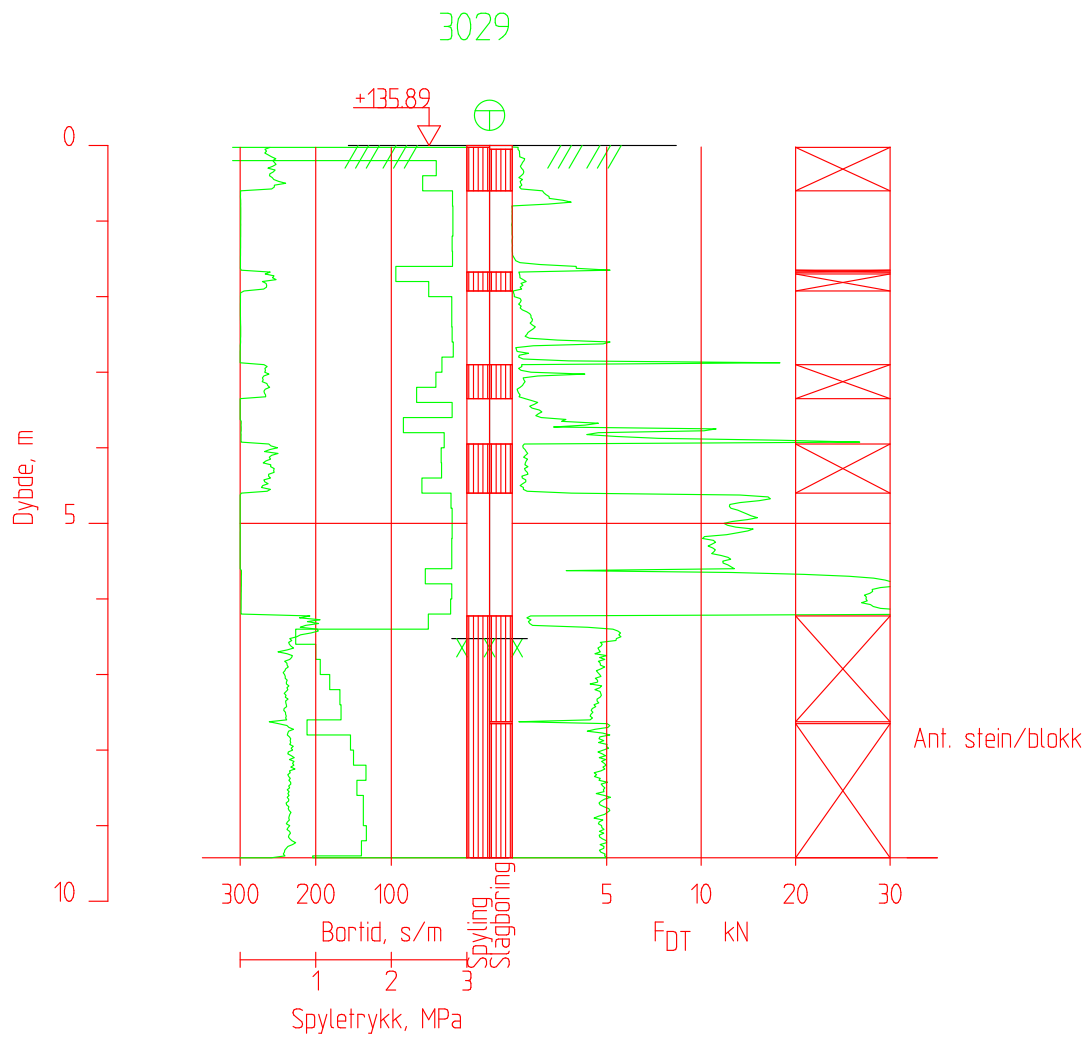
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122853.33 Y 115280.07

Totalsondering

Borhull 3029

Dato boret :28.06.2017

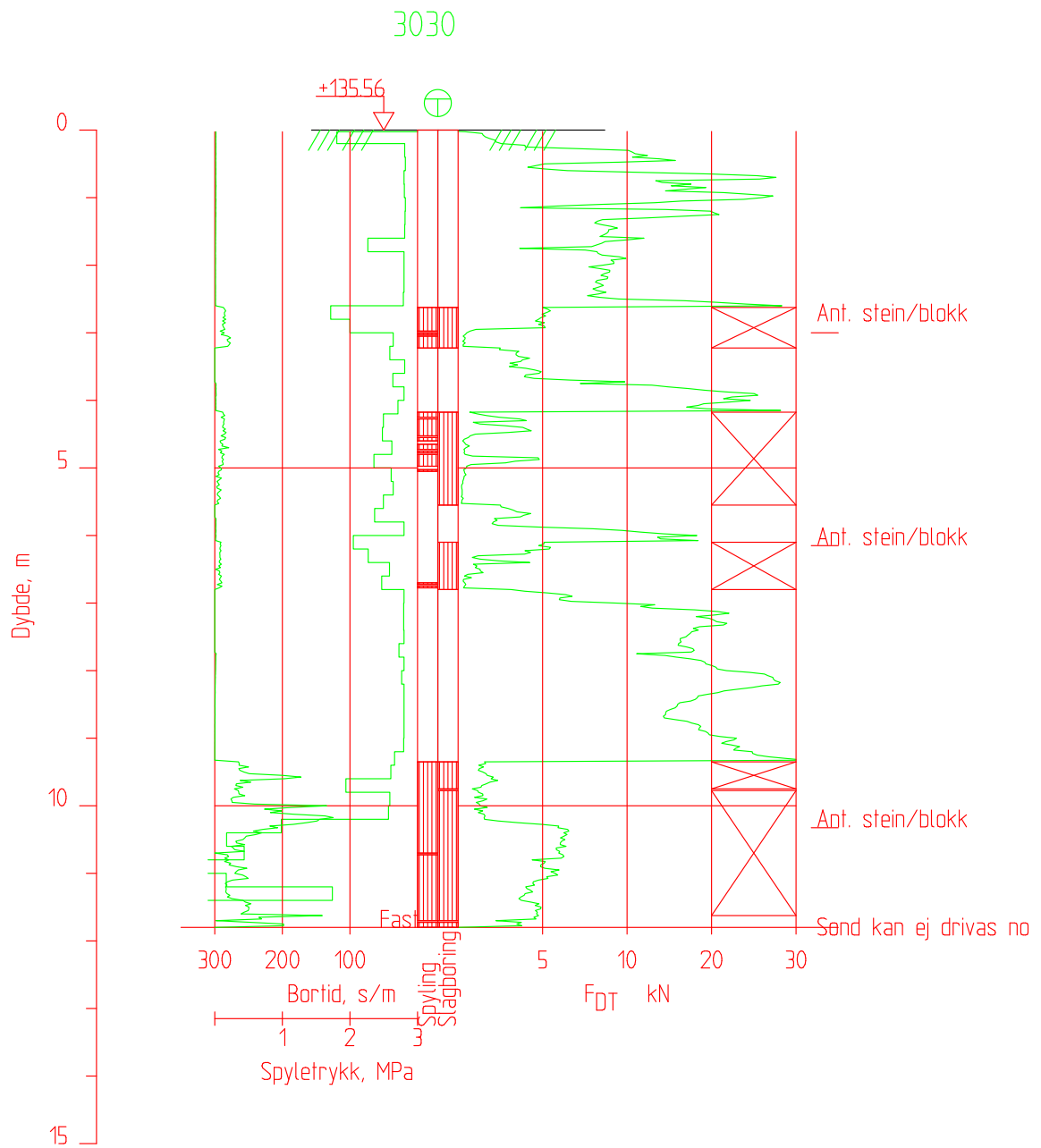
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122863.73 Y 115255.52

Totalsondering

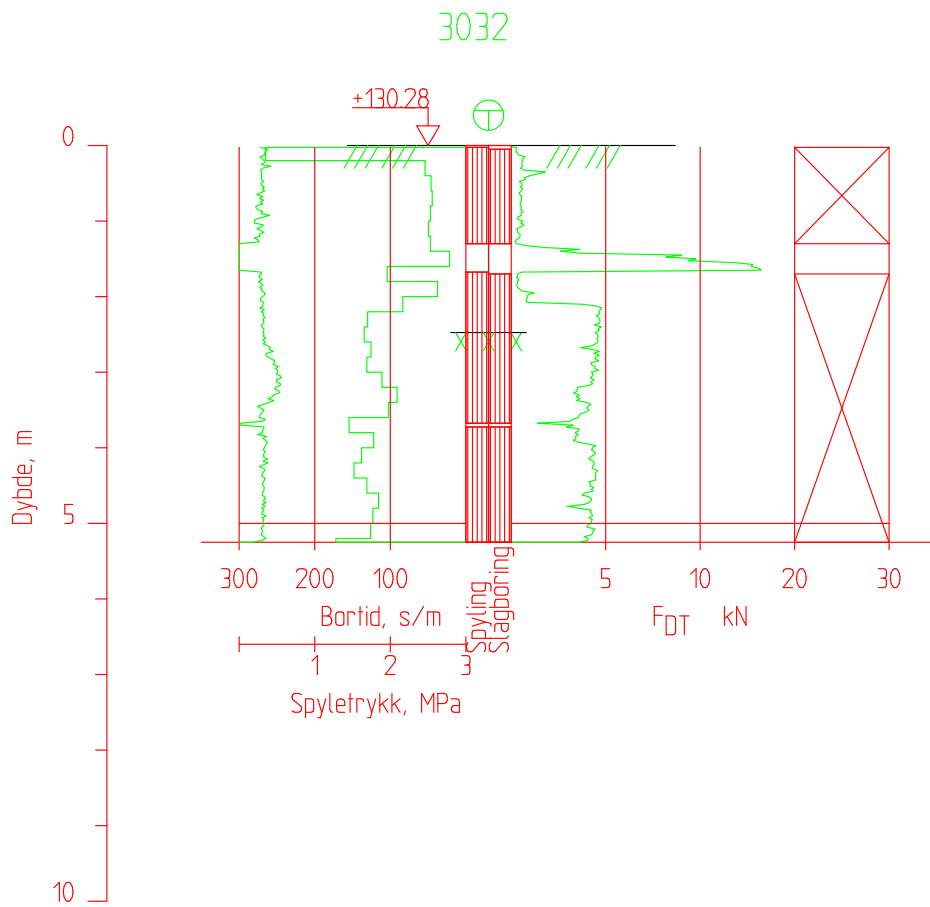
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E18 Langangen Rugtvedt

Borhull 3030

Dato boret :28.06.2017

M = 1 : 100



Posisjon: X 1122829.11 Y 115315.45

Totalsondering

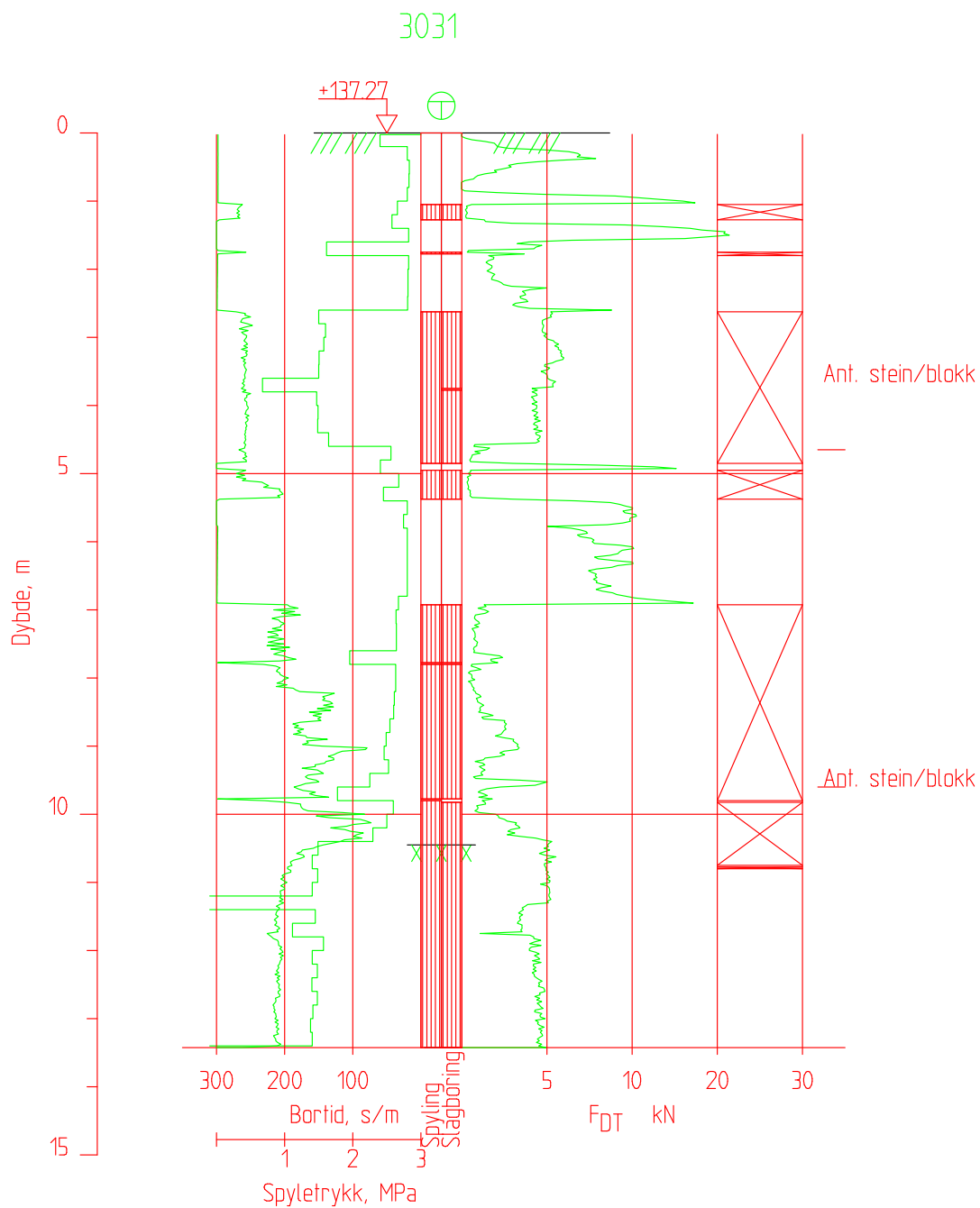
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E18 Langangen Rugtvedt

Borhull 3032

Dato boret :28.06.2017

M = 1 : 100



Posisjon: X 1122836.82 Y 115285.13

Totalsondering

Borhull 3031

Dato boret :28.06.2017

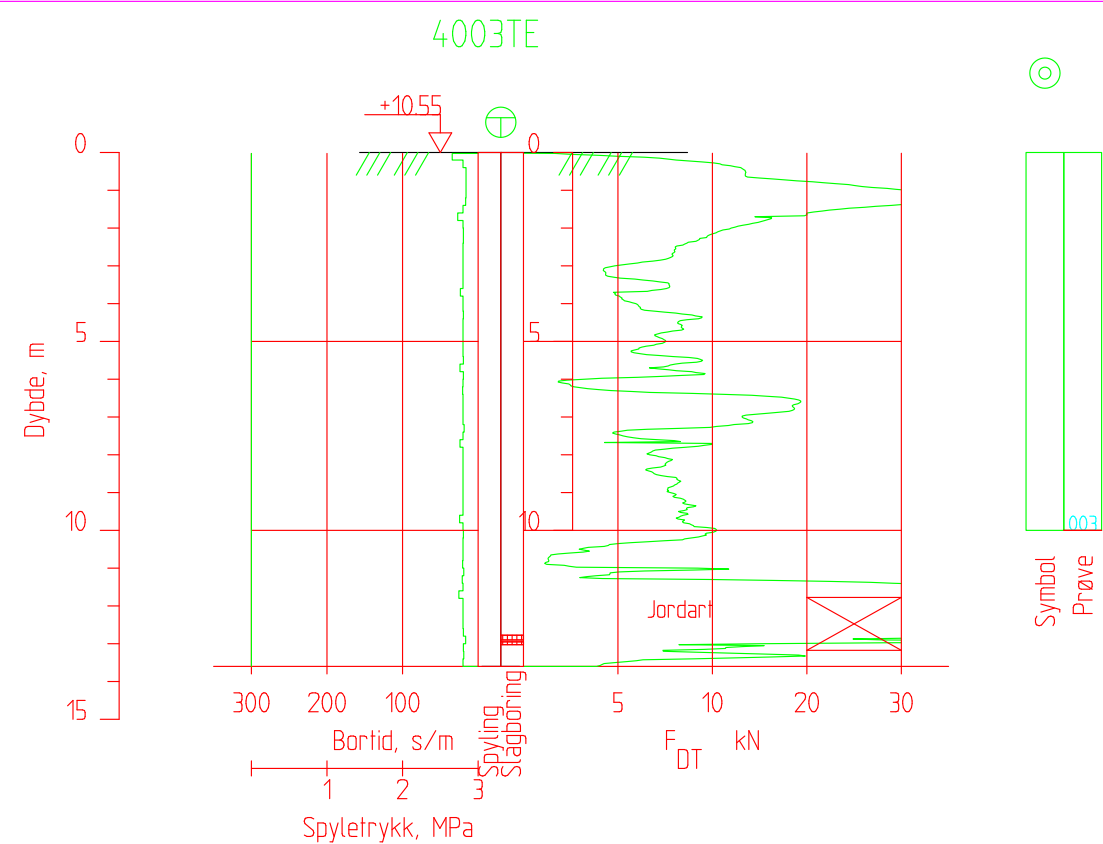
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



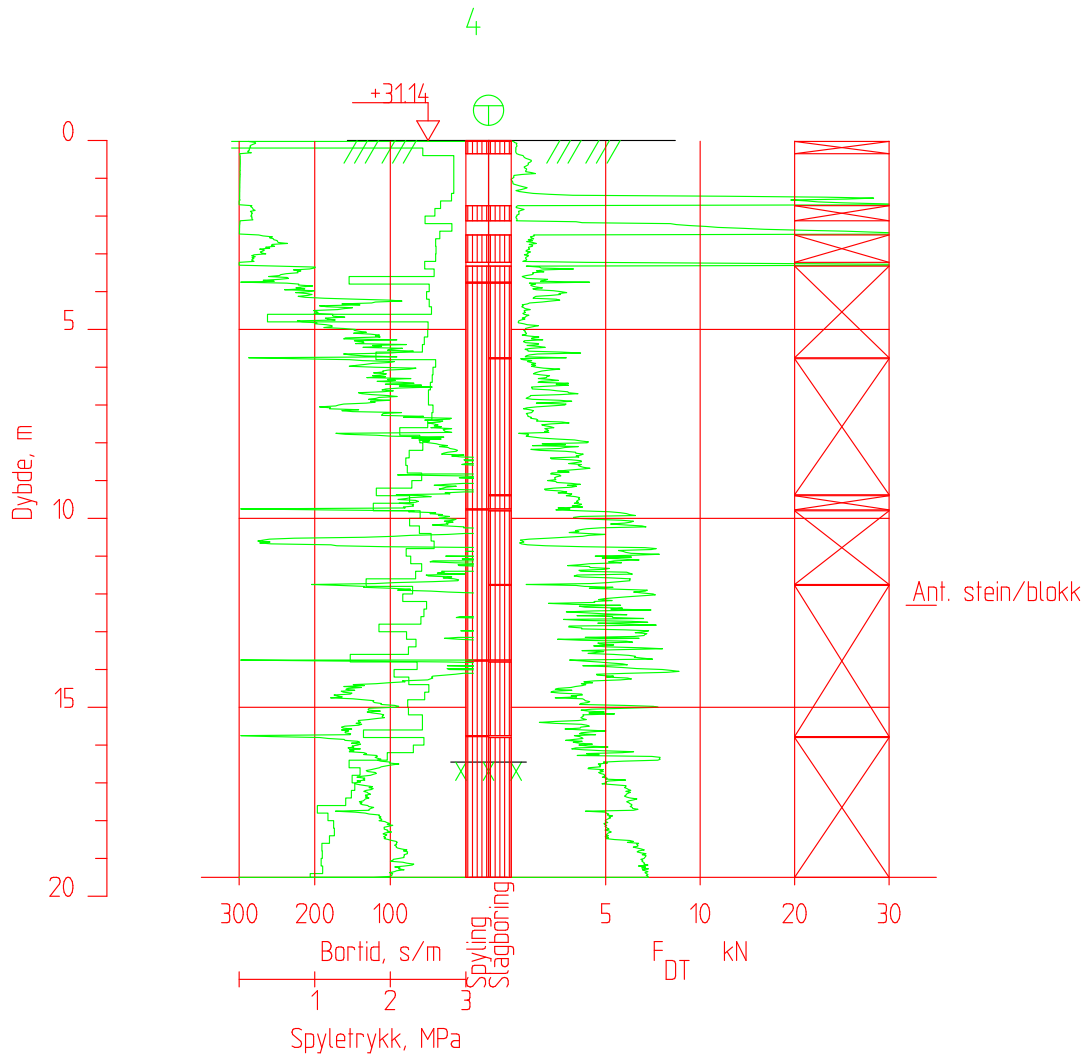
Posisjon: X 1124426.46 Y 112261.90

Totalsondering Borprofil
EIFFAGE
E18 Langangen Rugtvedt

Borhull 4003TE

Dato boret :01.07.2020

M = 1 : 200



Posisjon: X 1124410.91 Y 112644.46

Totalsondering

Borhull 4

Dato boret :03.11.2016

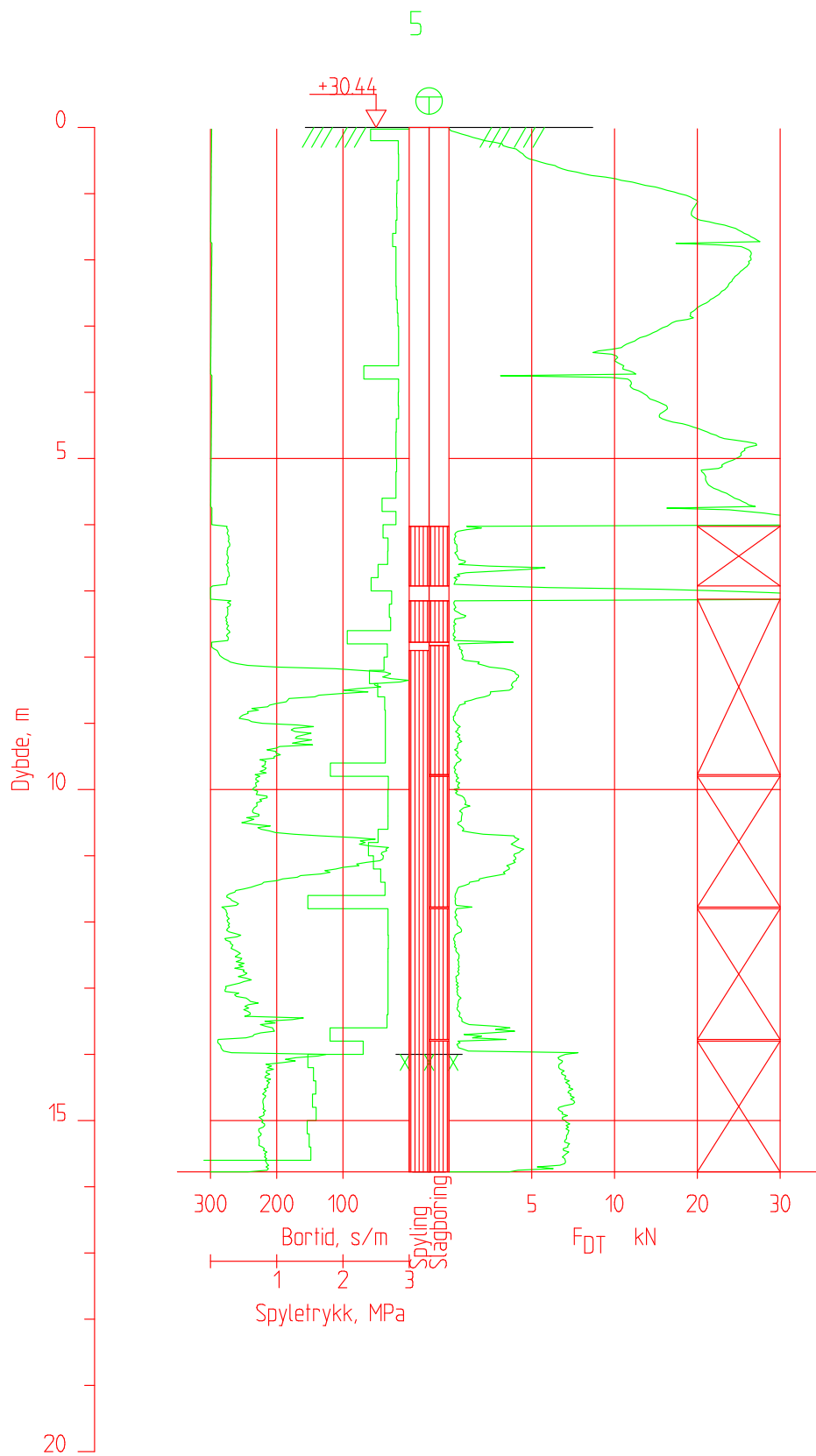
EIFFAGE

M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124412.34 Y 112508.77

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

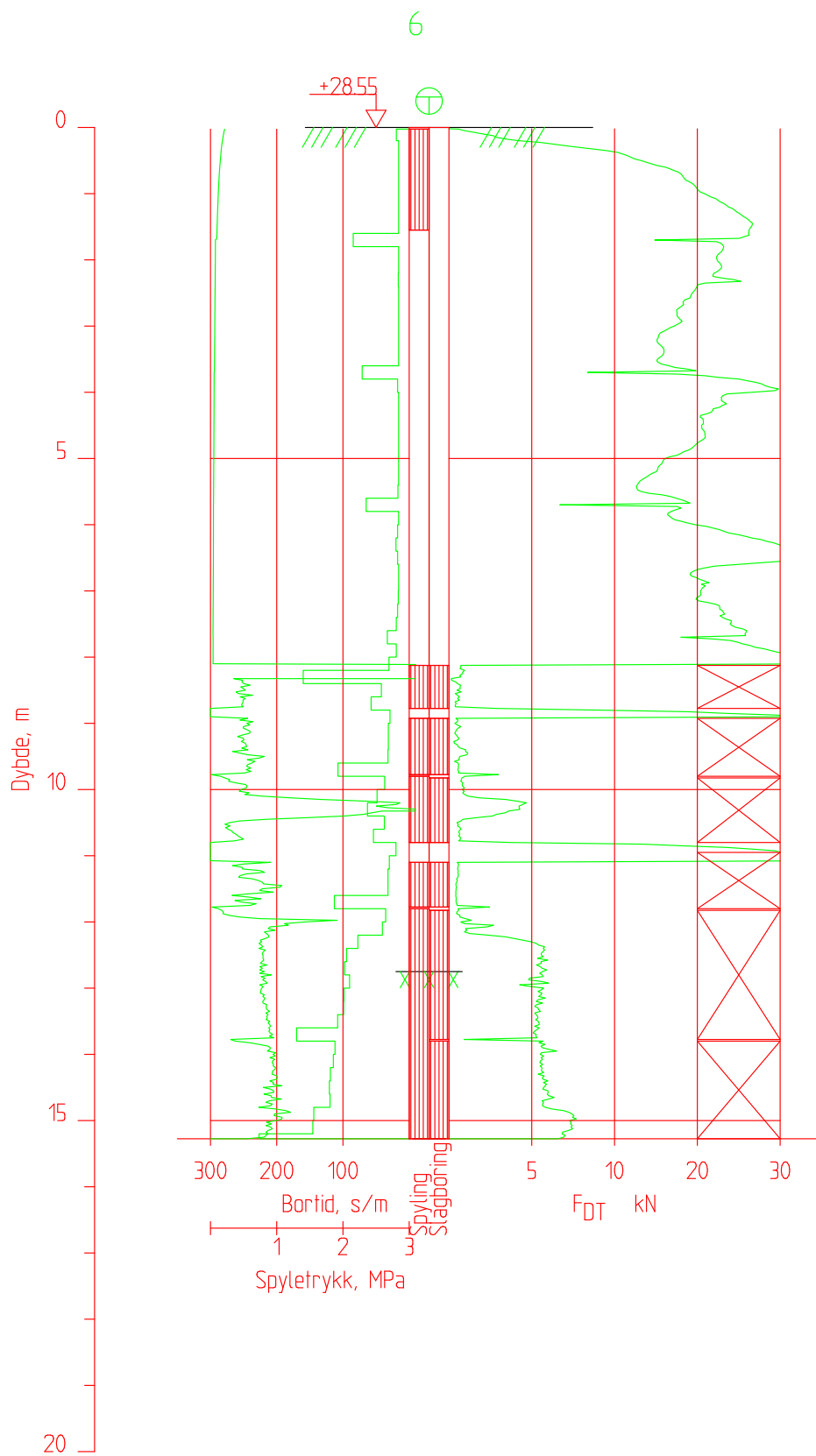
Borhull 5

Dato boret :03.11.2016

M = 1 : 100

BG

19756



Posisjon: X 1124415.56 Y 112495.43

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

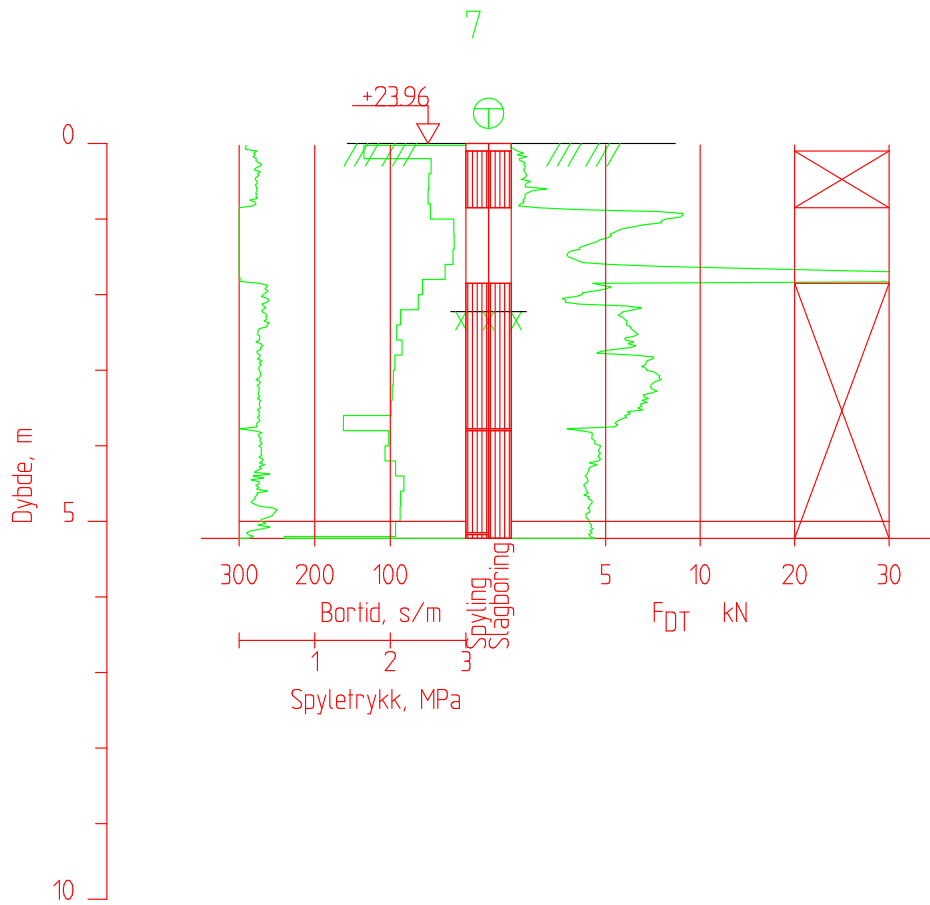
Borhull 6

Dato boret :03.11.2016

M = 1 : 100

BG

19756



Posisjon: X 1124406.54 Y 112427.19

Totalsondering

Borhull 7

Dato boret :02.11.2016

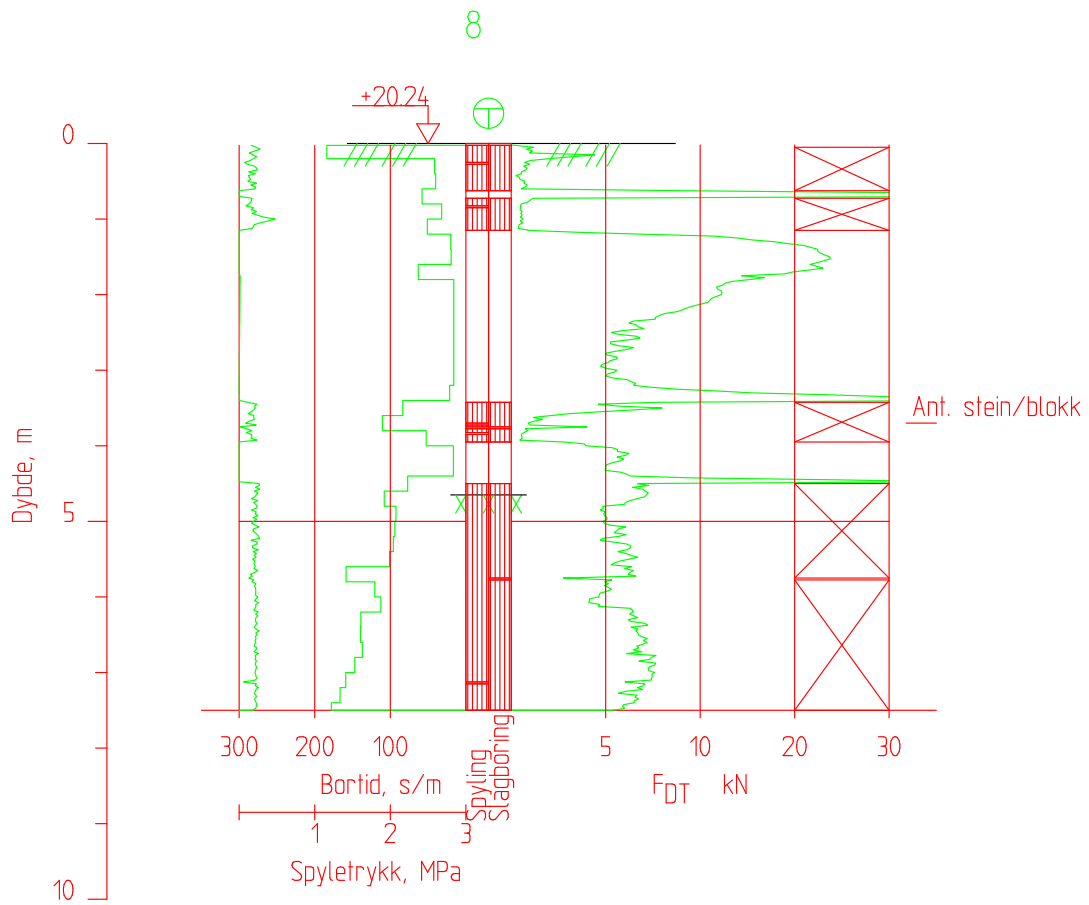
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124418.58 Y 112410.49

Totalsondering

Borhull 8

Dato boret :02.11.2016

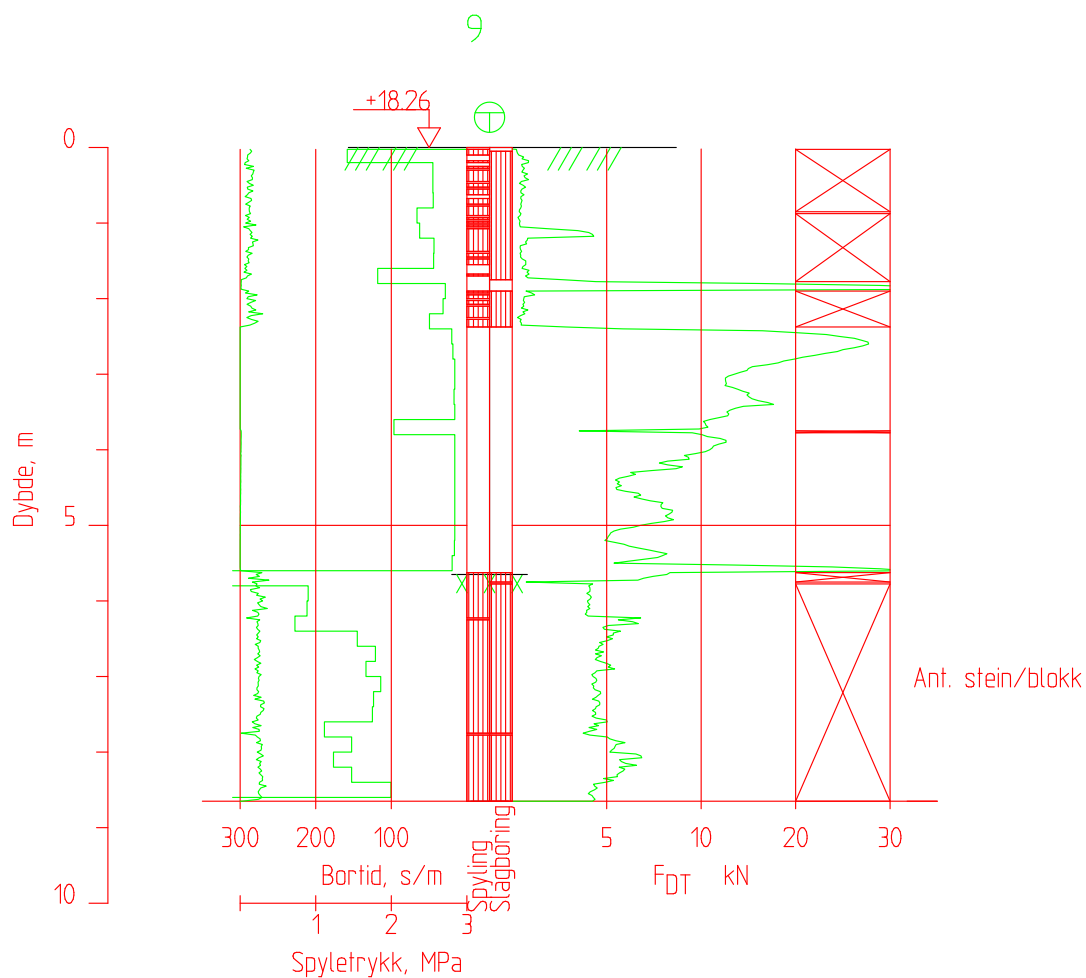
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124419.35 Y 112384.05

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

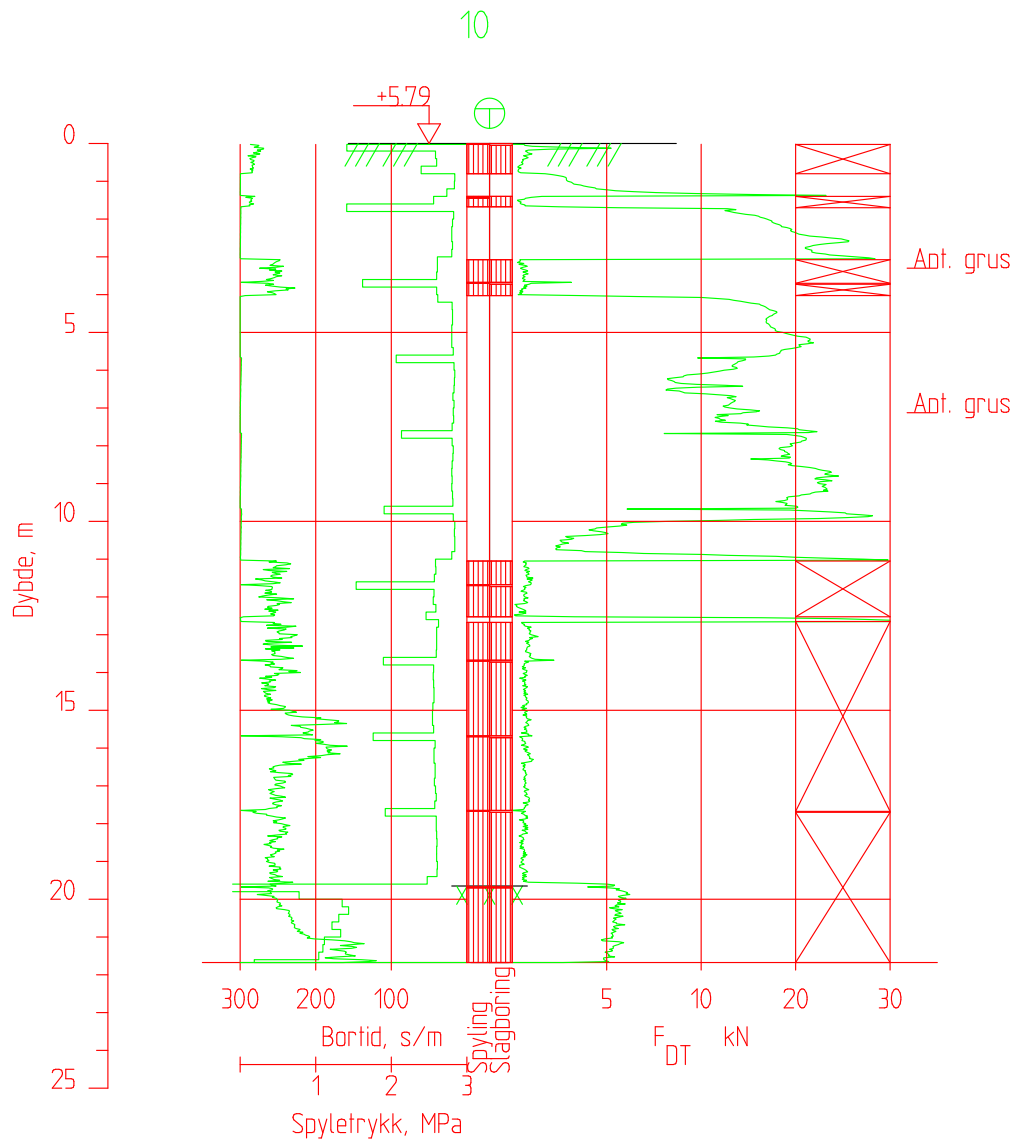
Borhull 9

Dato boret :02.11.2016

M = 1 : 100

BG

19756



Posisjon: X 1124421.16 Y 112345.05

Totalsondering

Borhull 10

Dato boret :25.01.2017

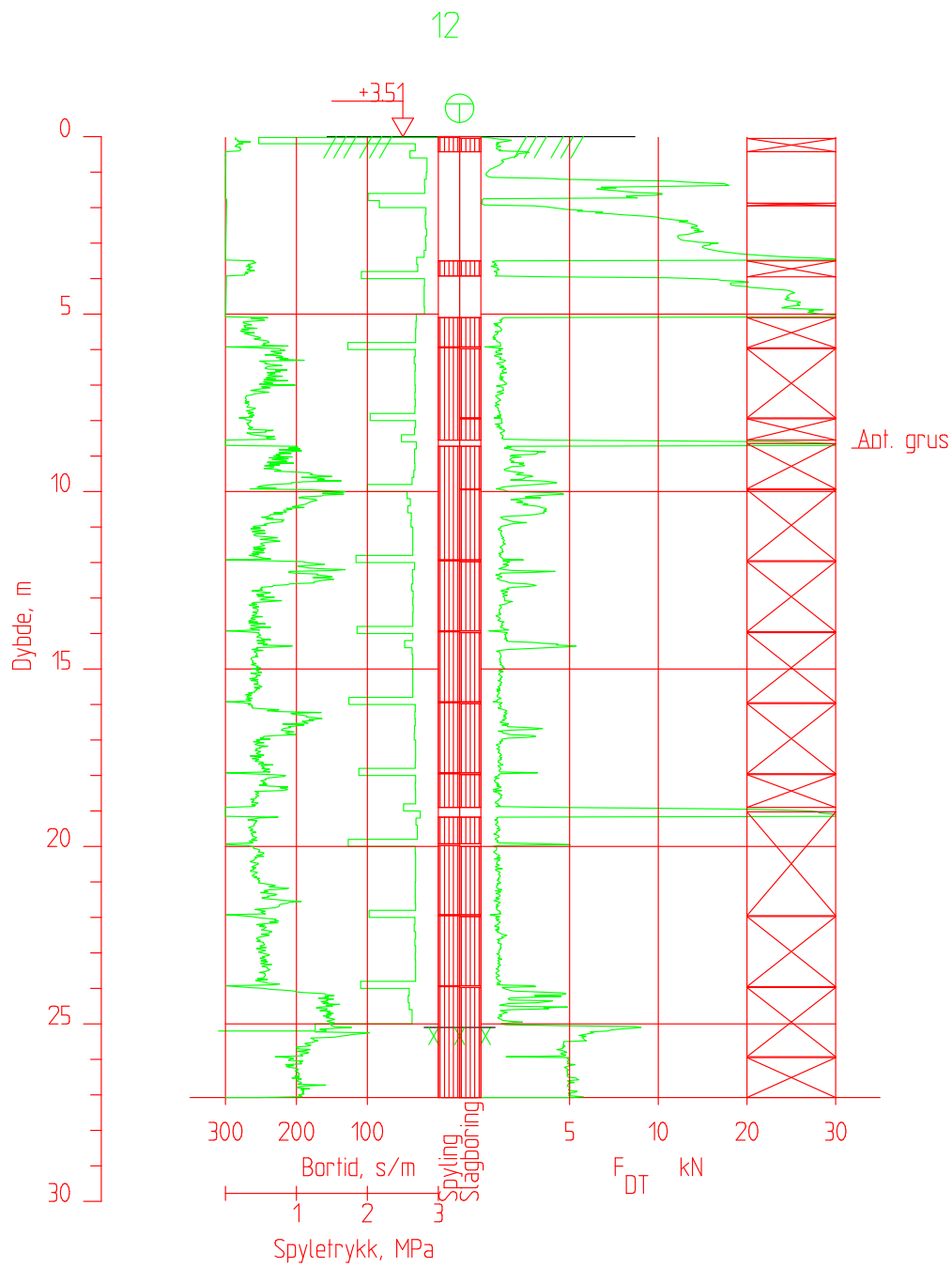
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124422.60 Y 112331.63

Totalsondering

Borhull 12

Dato boret :25.01.2017

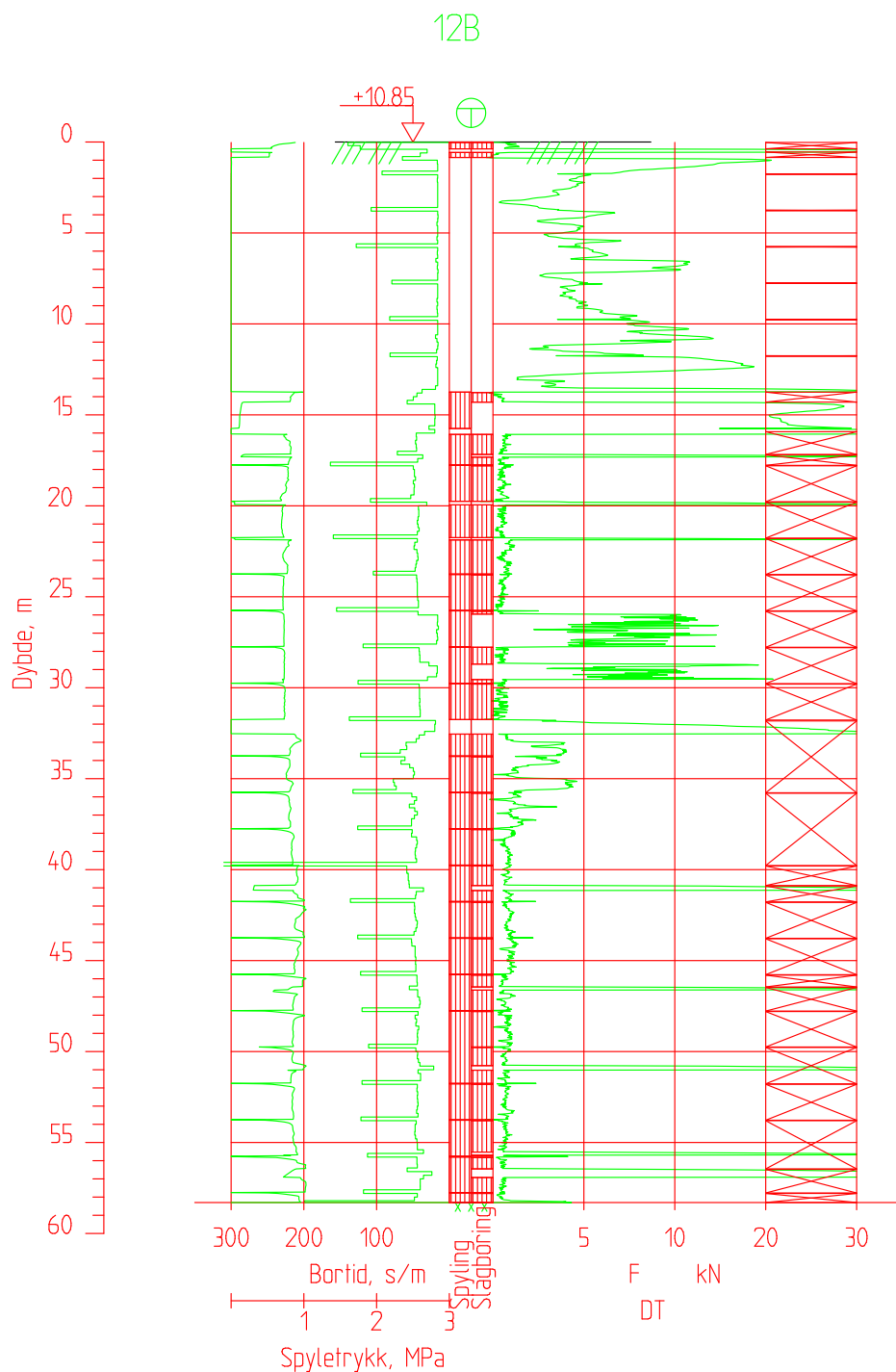
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124438.15 Y 112282.00

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

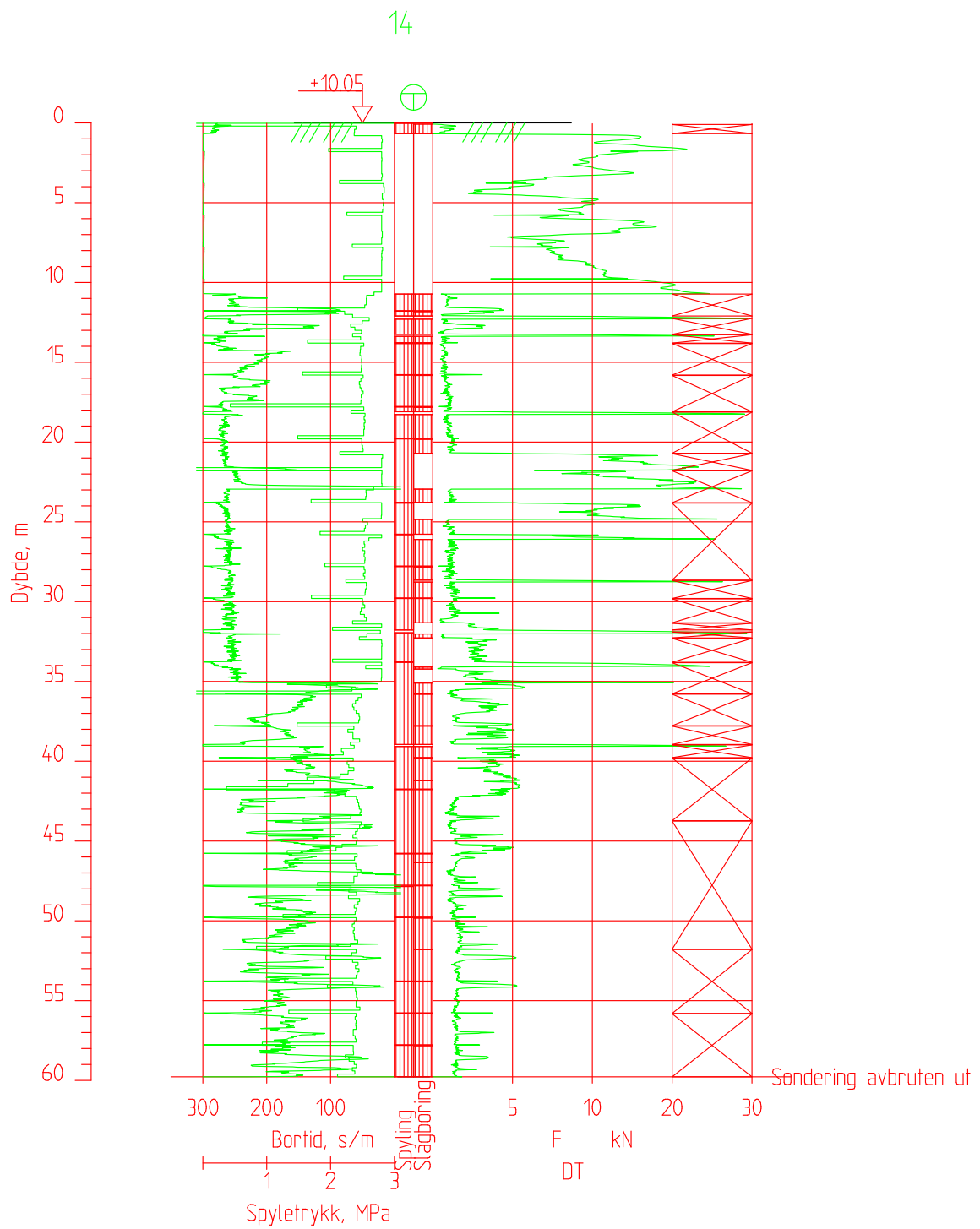
Borhull 12B

Dato boret :23.01.2017

M = 1 : 400

BG

19756



Posisjon: X 1124419.89 Y 112245.94

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

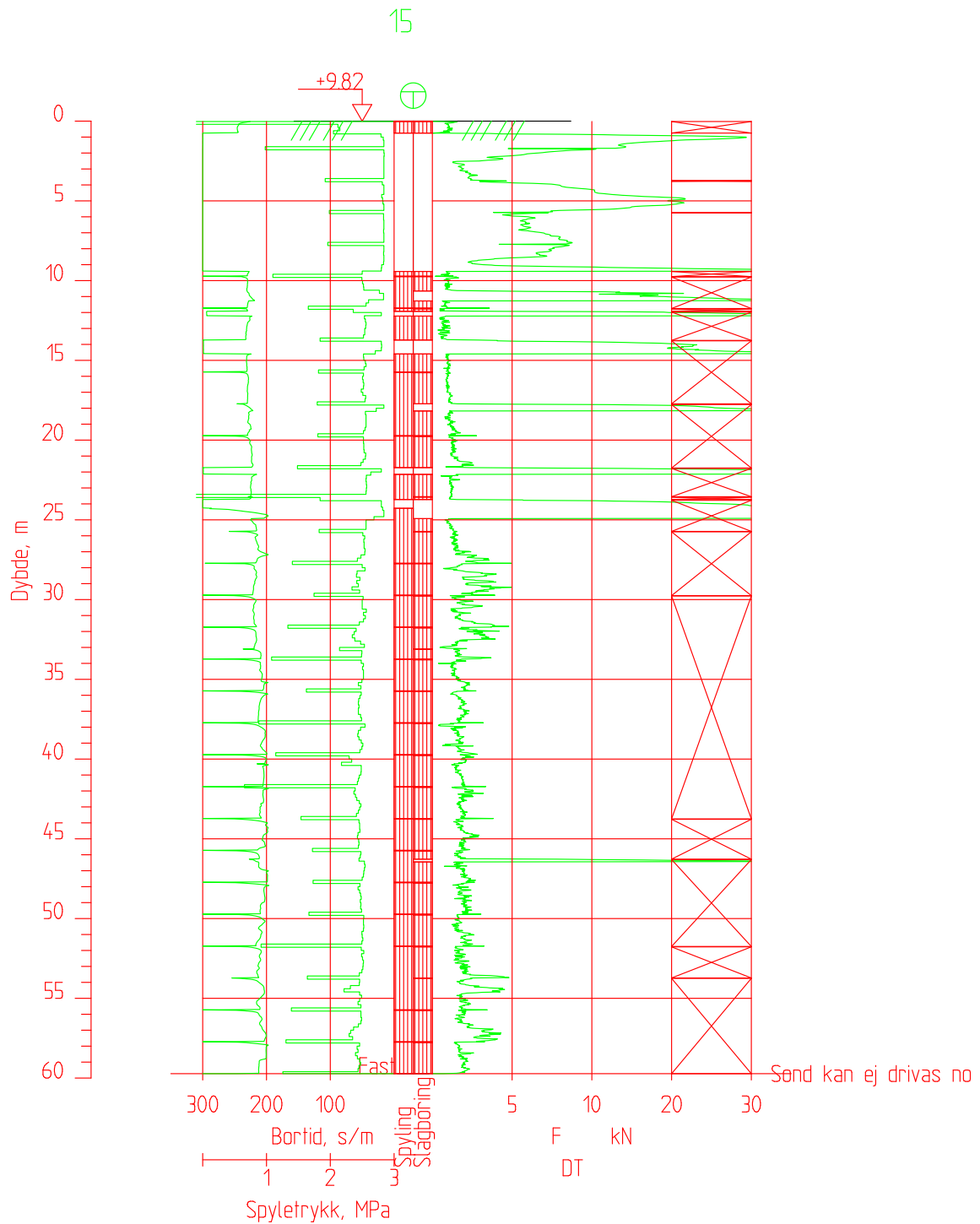
Borhull 14

Dato boret :24.01.2017

M = 1 : 400

BG

19756



Posisjon: X 1124417.45 Y 112219.69

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

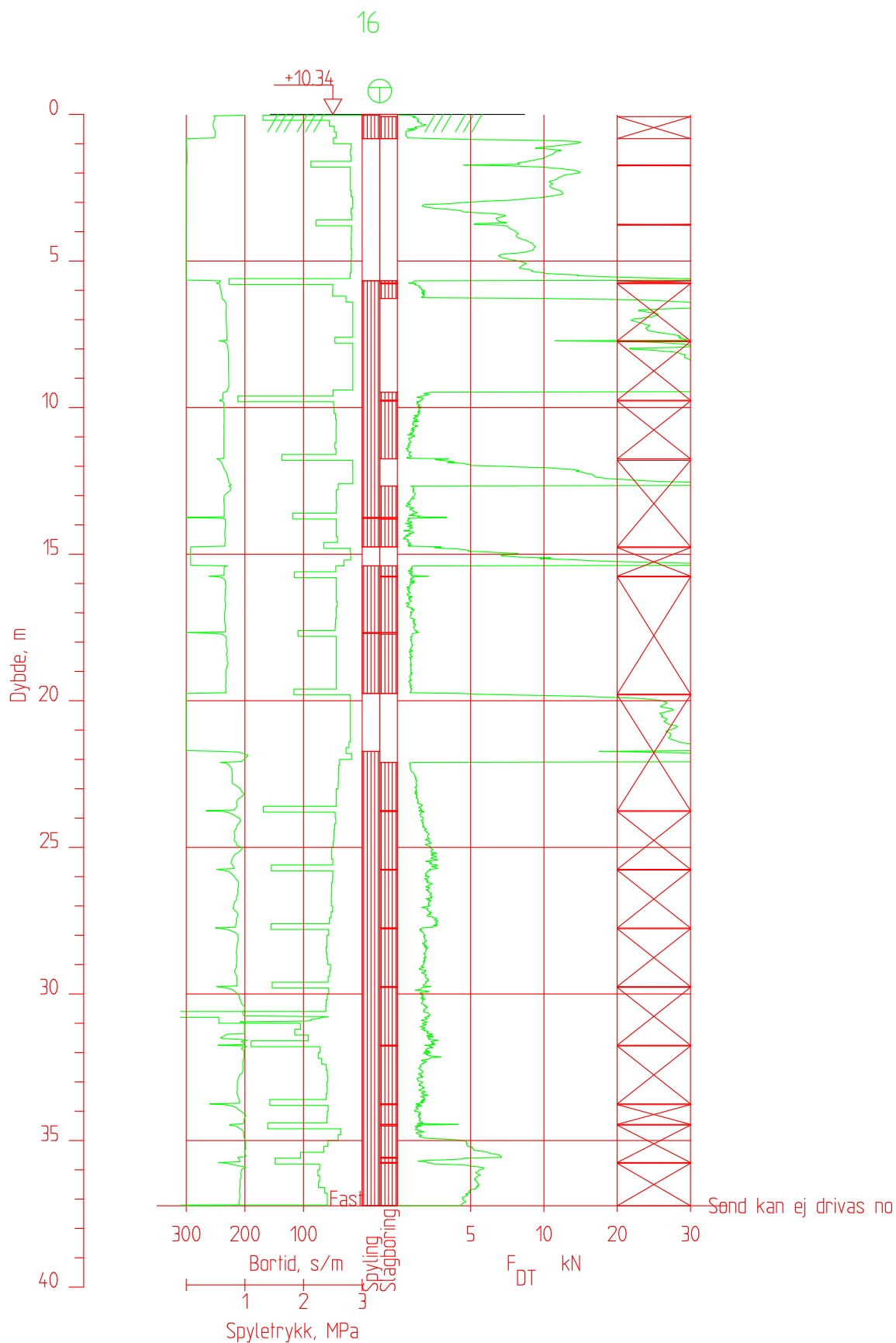
Borhull 15

Dato boret :24.01.2017

M = 1 : 400

BG

19756



Posisjon: X 1124416.58 Y 112193.55

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

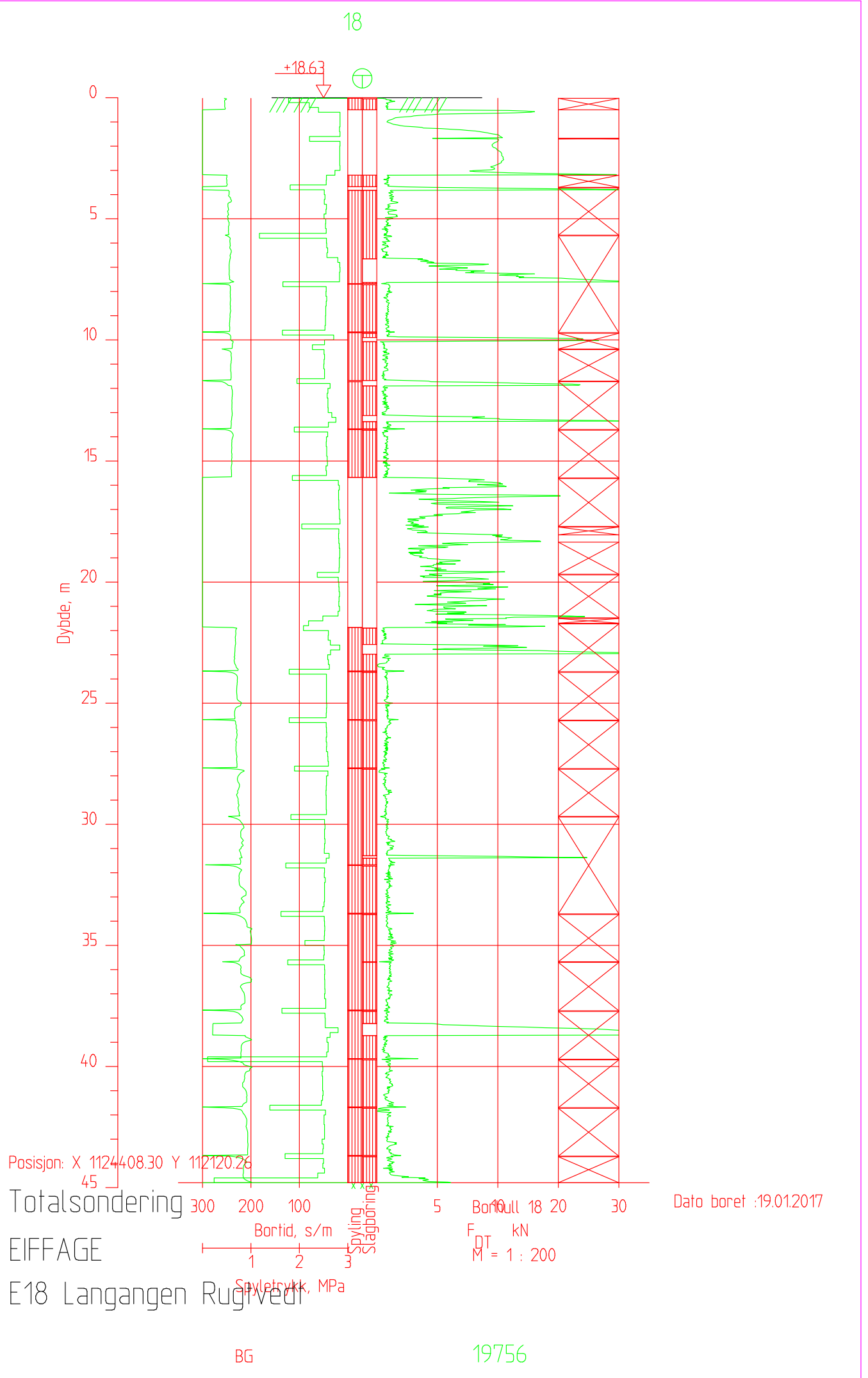
Borhull 16

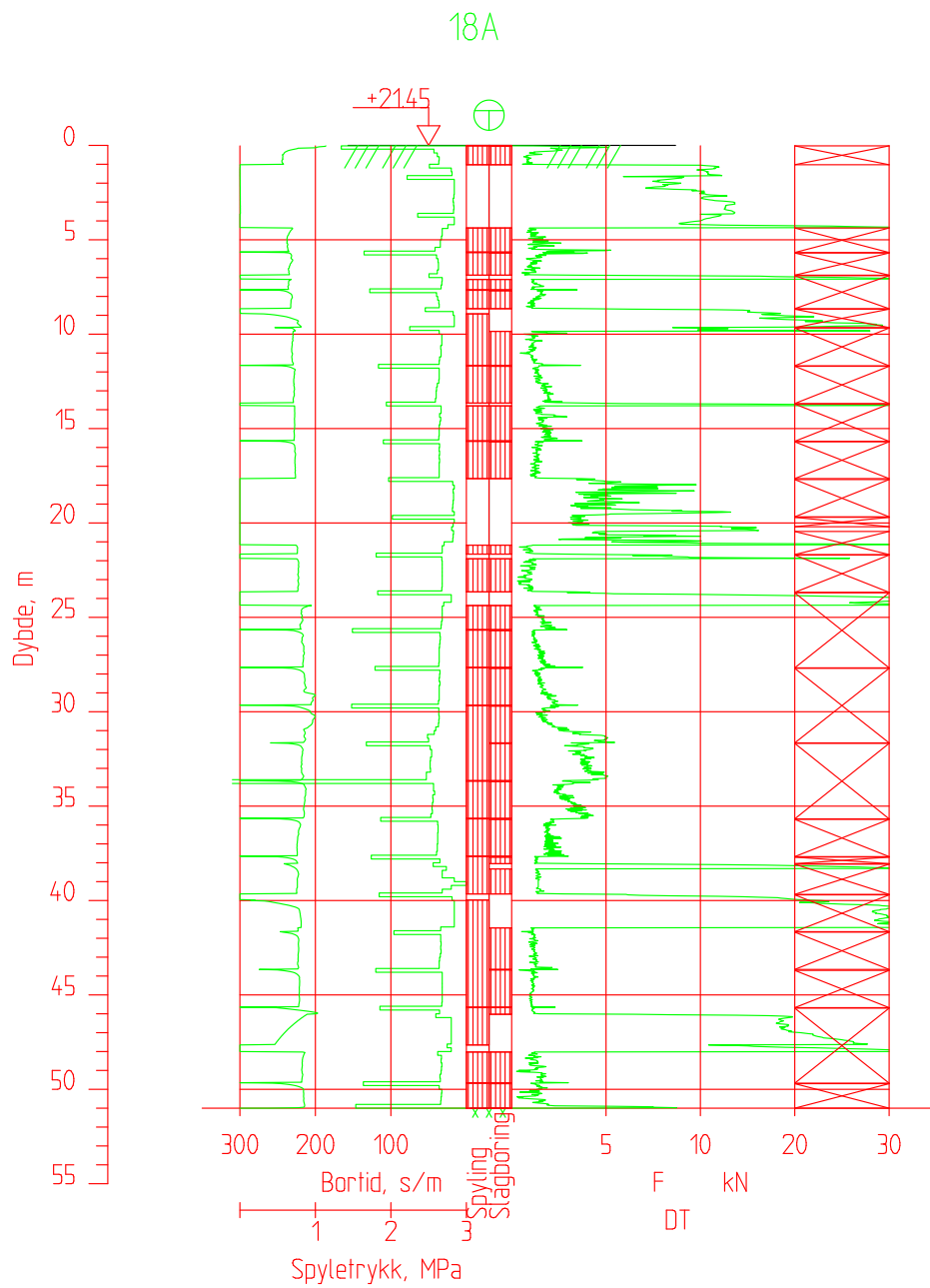
Dato boret :24.01.2017

M = 1 : 200

BG

19756





Posisjon: X 1124391.16 Y 112118.51

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

Borhull 18A

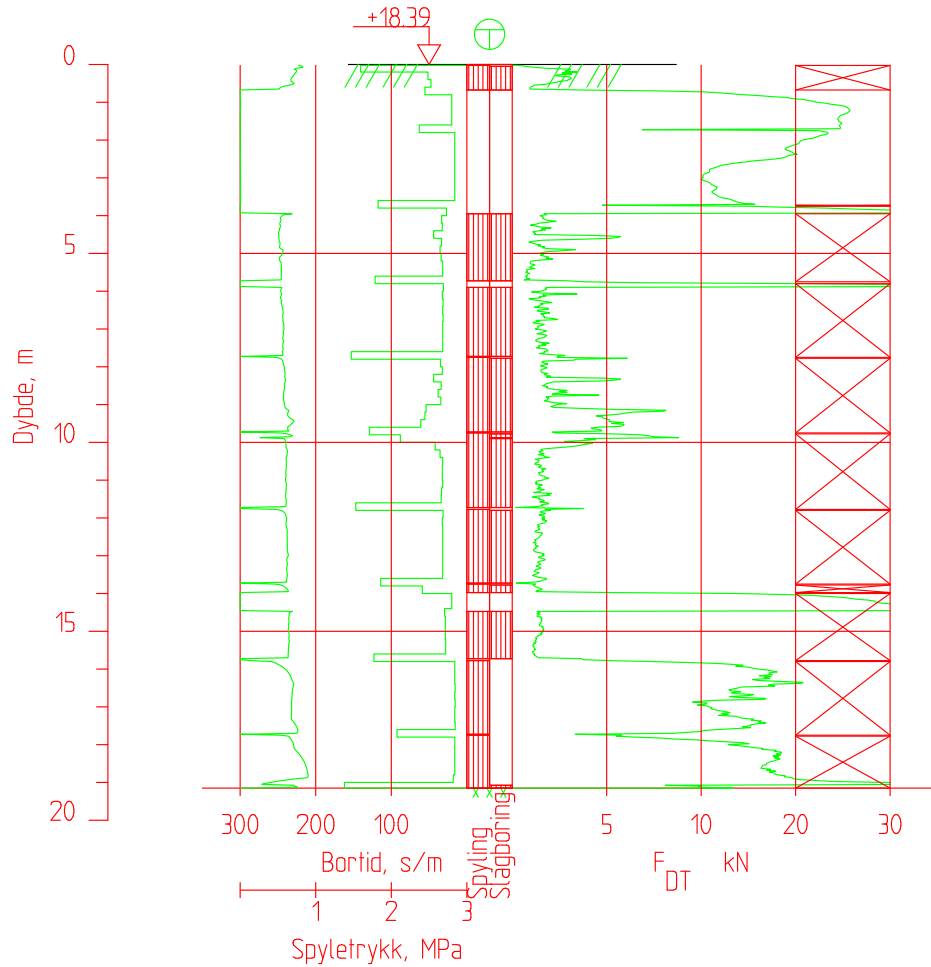
Dato boret :25.01.2017

M = 1 : 400

BG

19756

18B



Posisjon: X 1124438.39 Y 112120.85

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

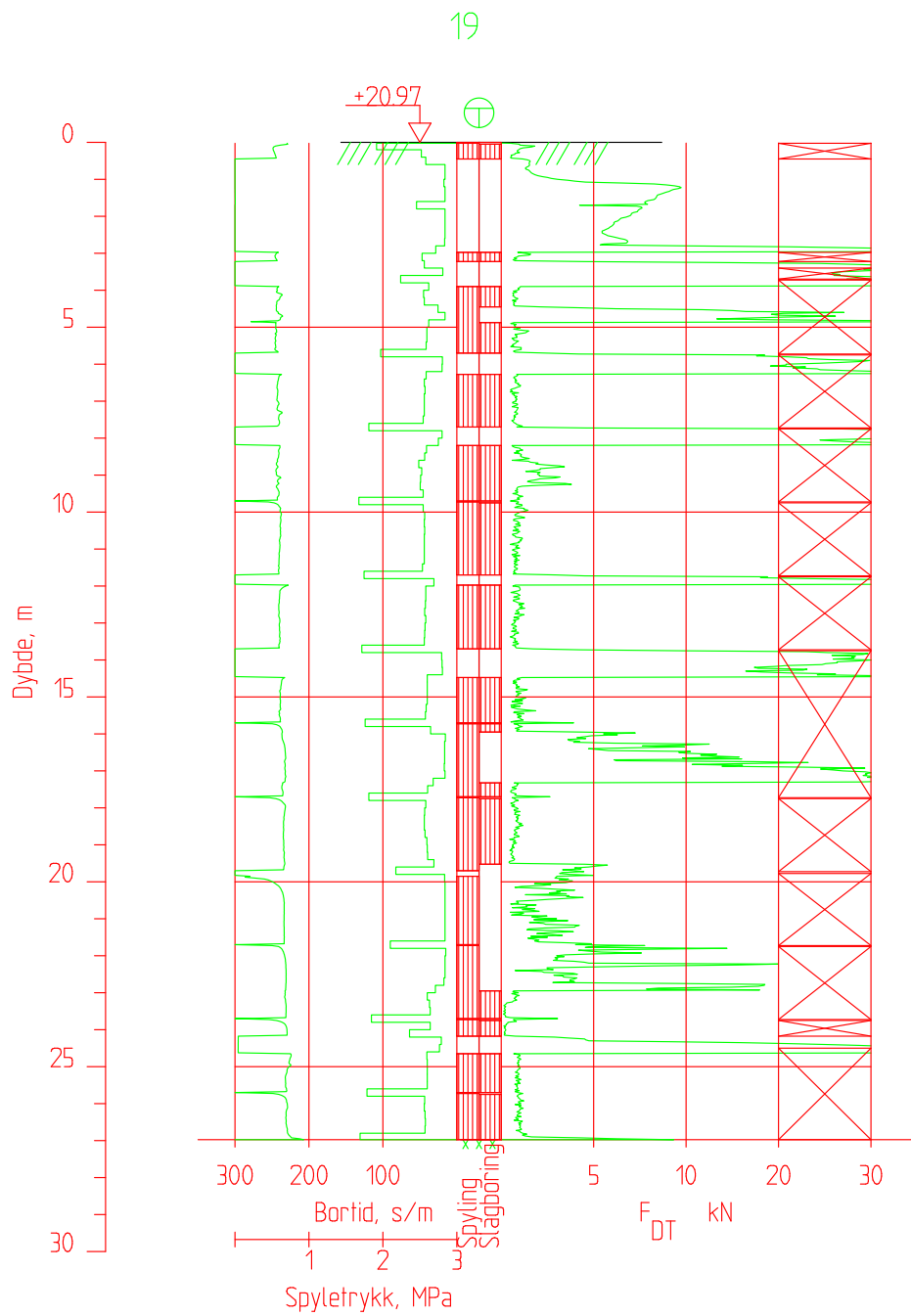
Borhull 18B

Dato boreal :25.01.2017

$M = 1 : 200$

BG

19756



Posisjon: X 1124410.06 Y 112104.64

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

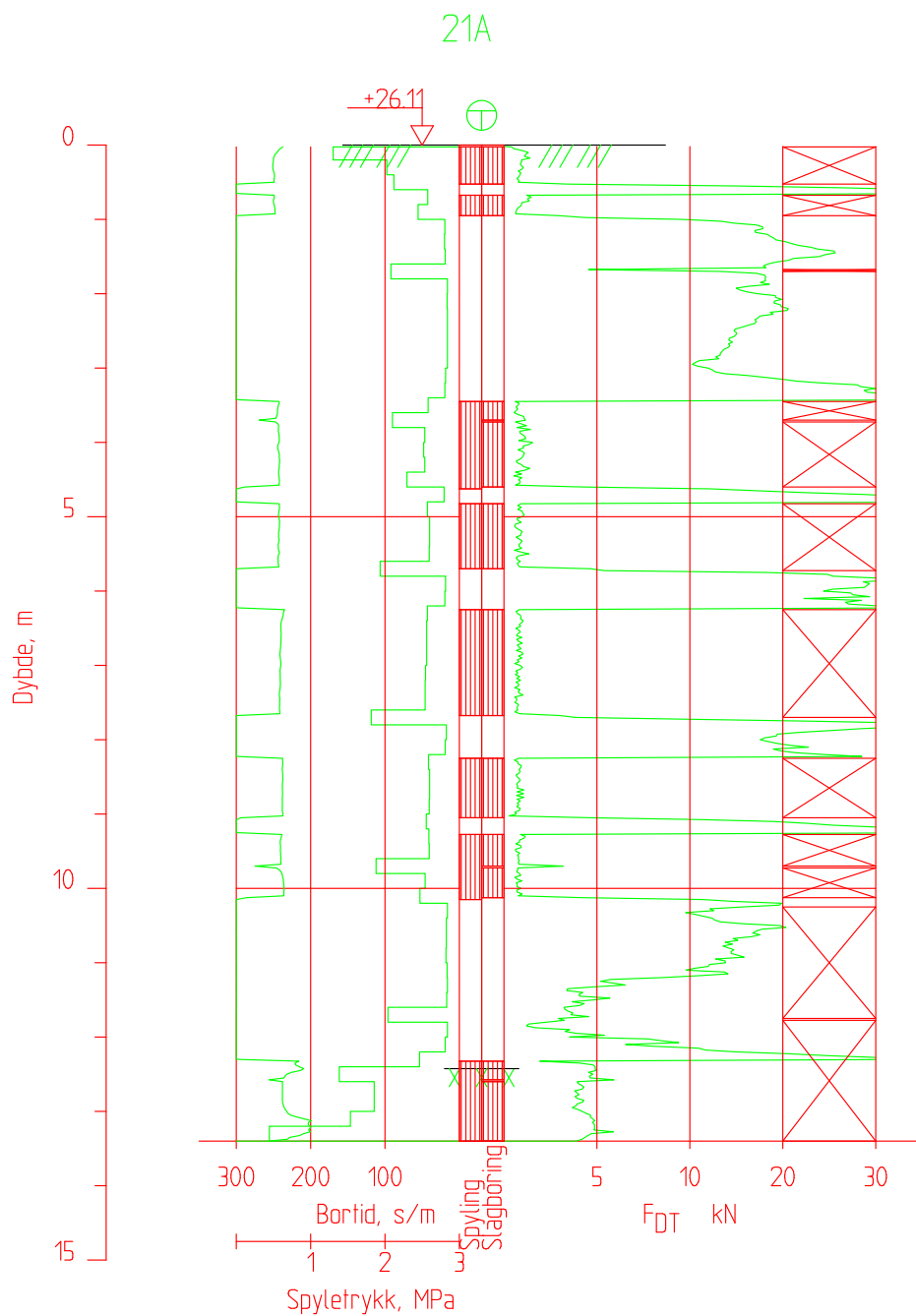
Borhull 19

Dato borete :19.01.2017

M = 1 : 200

BG

19756



Posisjon: X 1124383.25 Y 112098.01

Totalsondering

Borhull 21A

Dato borete :19.01.2017

EIFFAGE

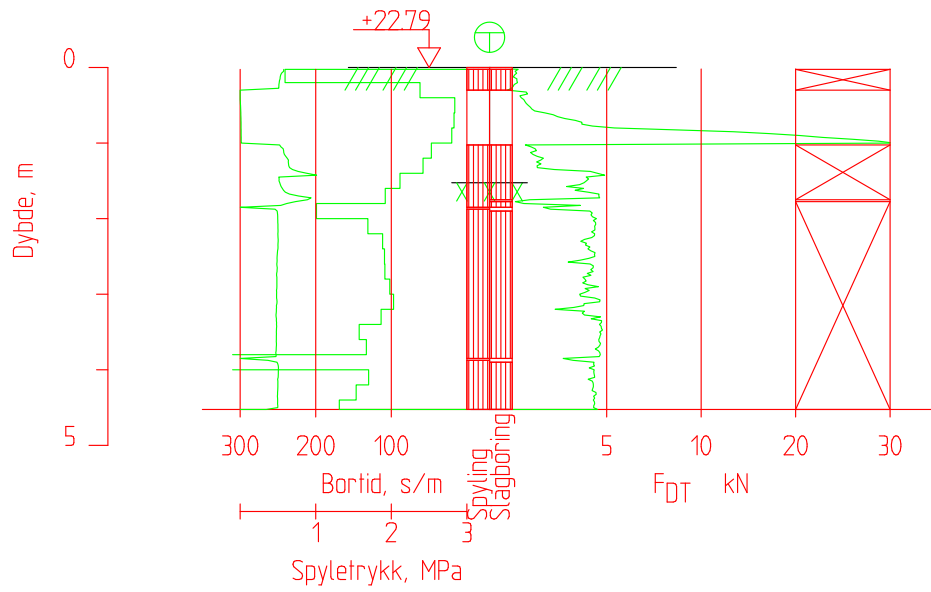
M = 1 : 100

E18 Langangen Rugtvedt

BG

19756

21B



Posisjon: X 1124434.36 Y 112096.78

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

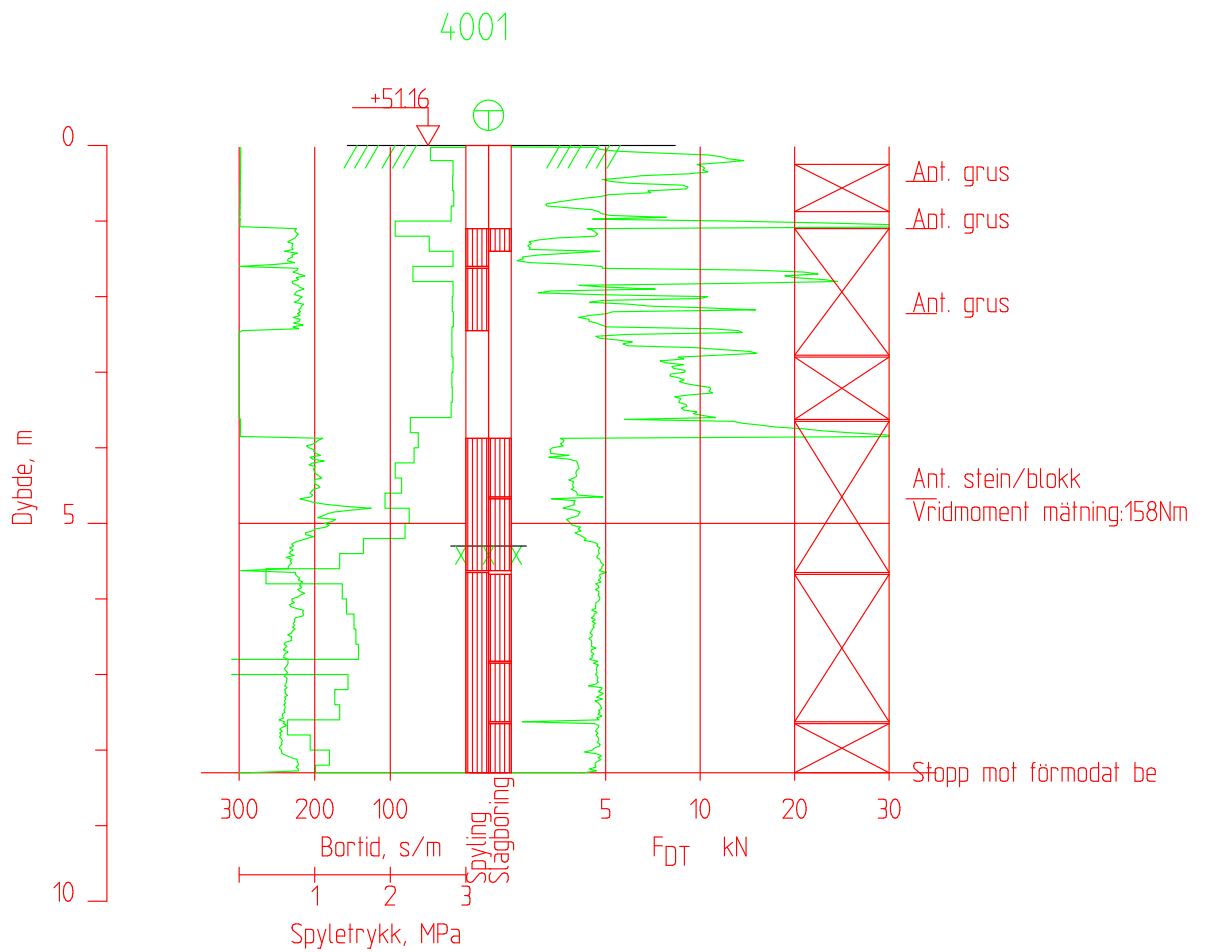
Borhull 21B

Dato boret :19.01.2017

M = 1 : 100

BG

19756



Posisjon: X 1124375.51 Y 112684.84

Totalsondering

Borhull 4001

Dato boret :22.11.2018

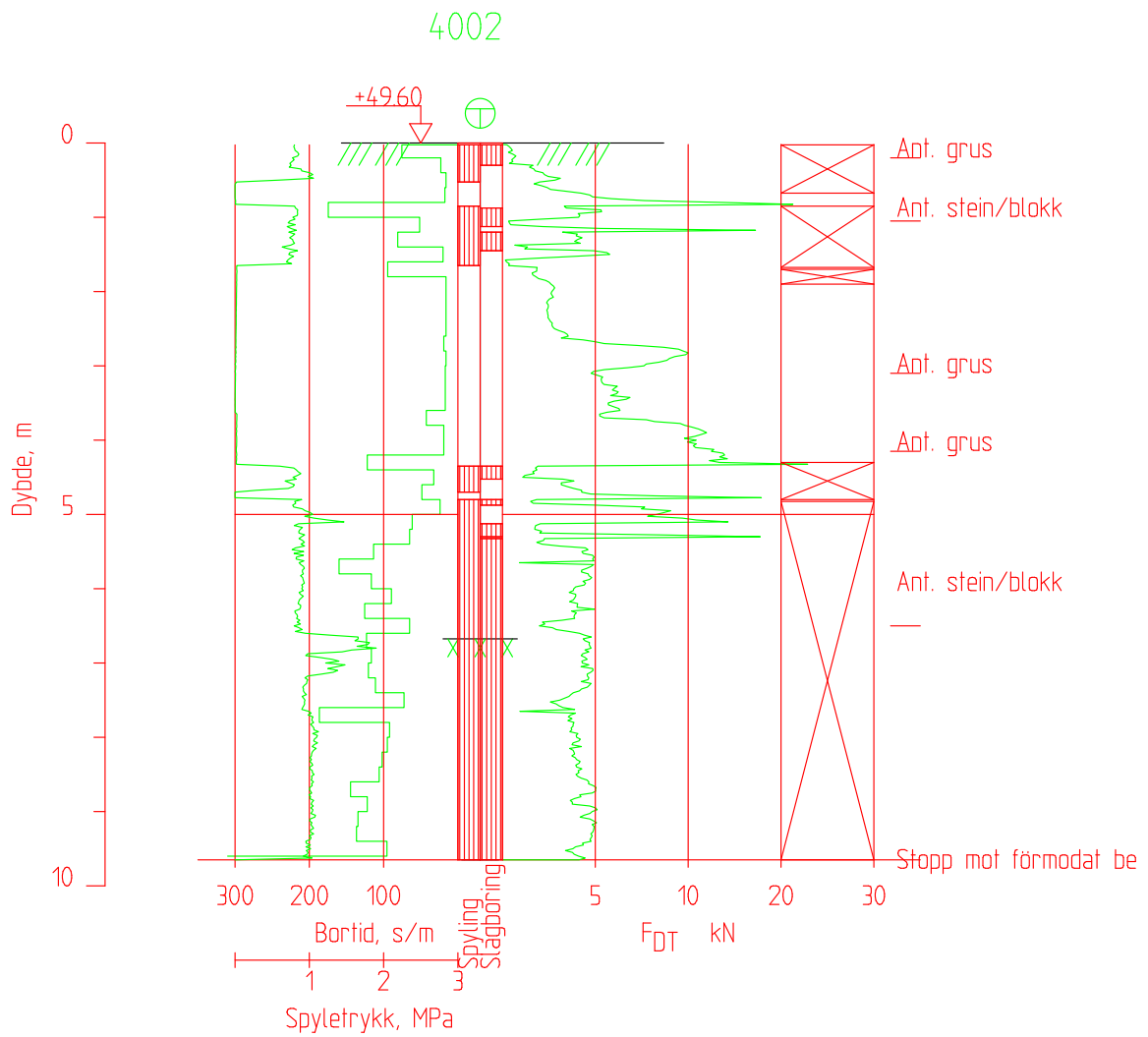
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124390.31 Y 112687.23

Totalsondering

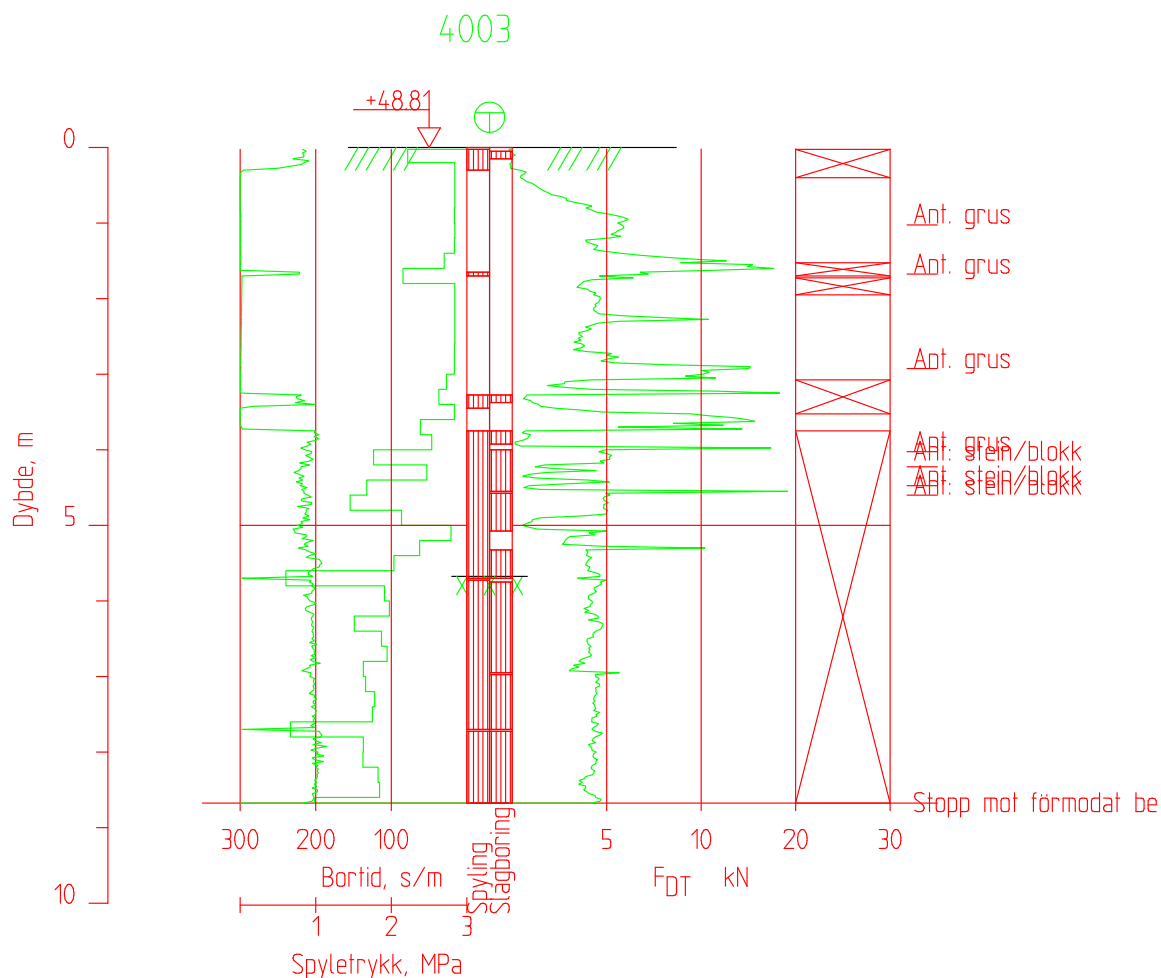
Borhull 4002

Dato boret :22.11.2018

EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt



Posisjon: X 1124404.95 Y 112688.43

Totalsondering

Borhull 4003

Dato boret :22.11.2018

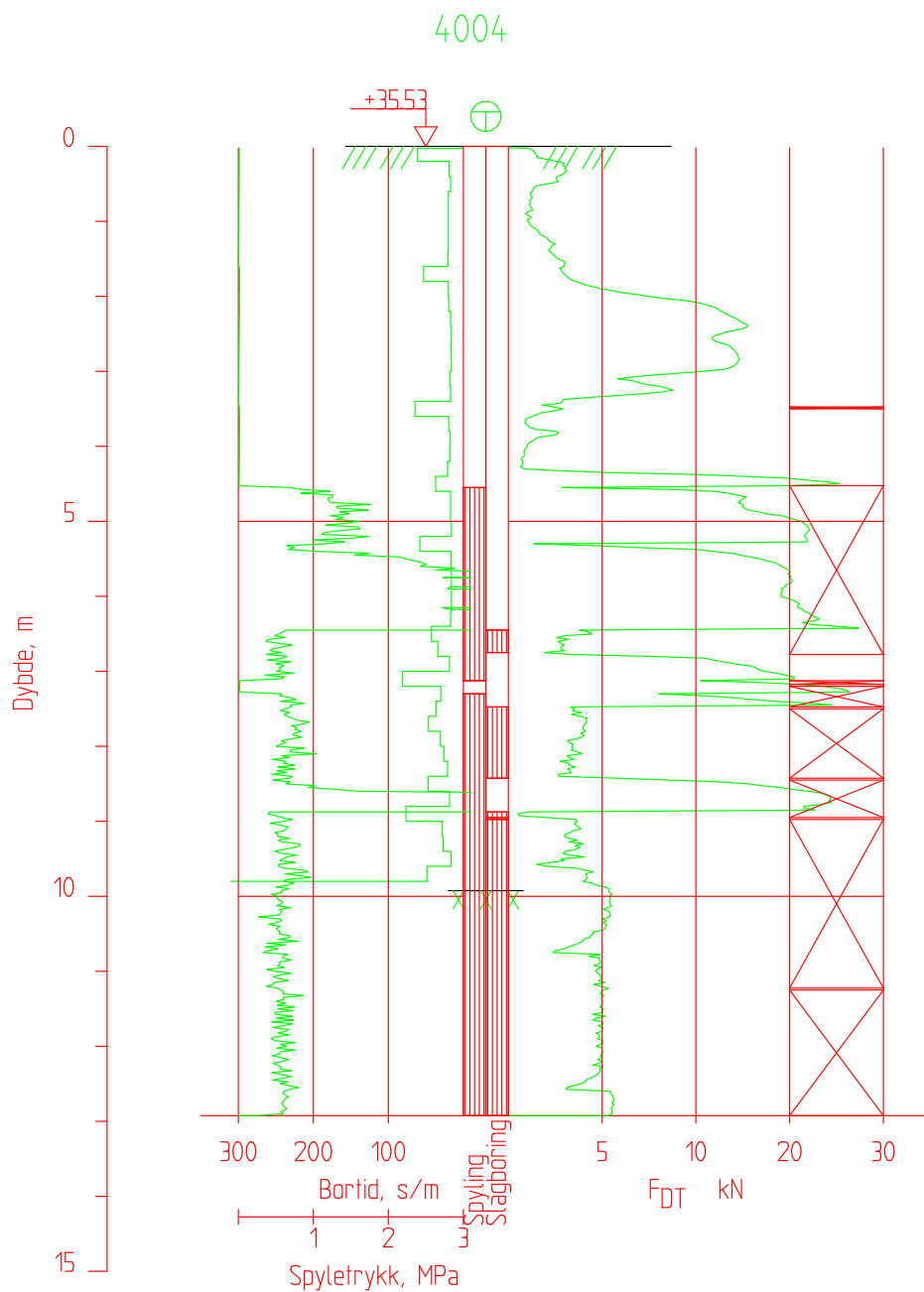
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124366.37 Y 112608.55

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

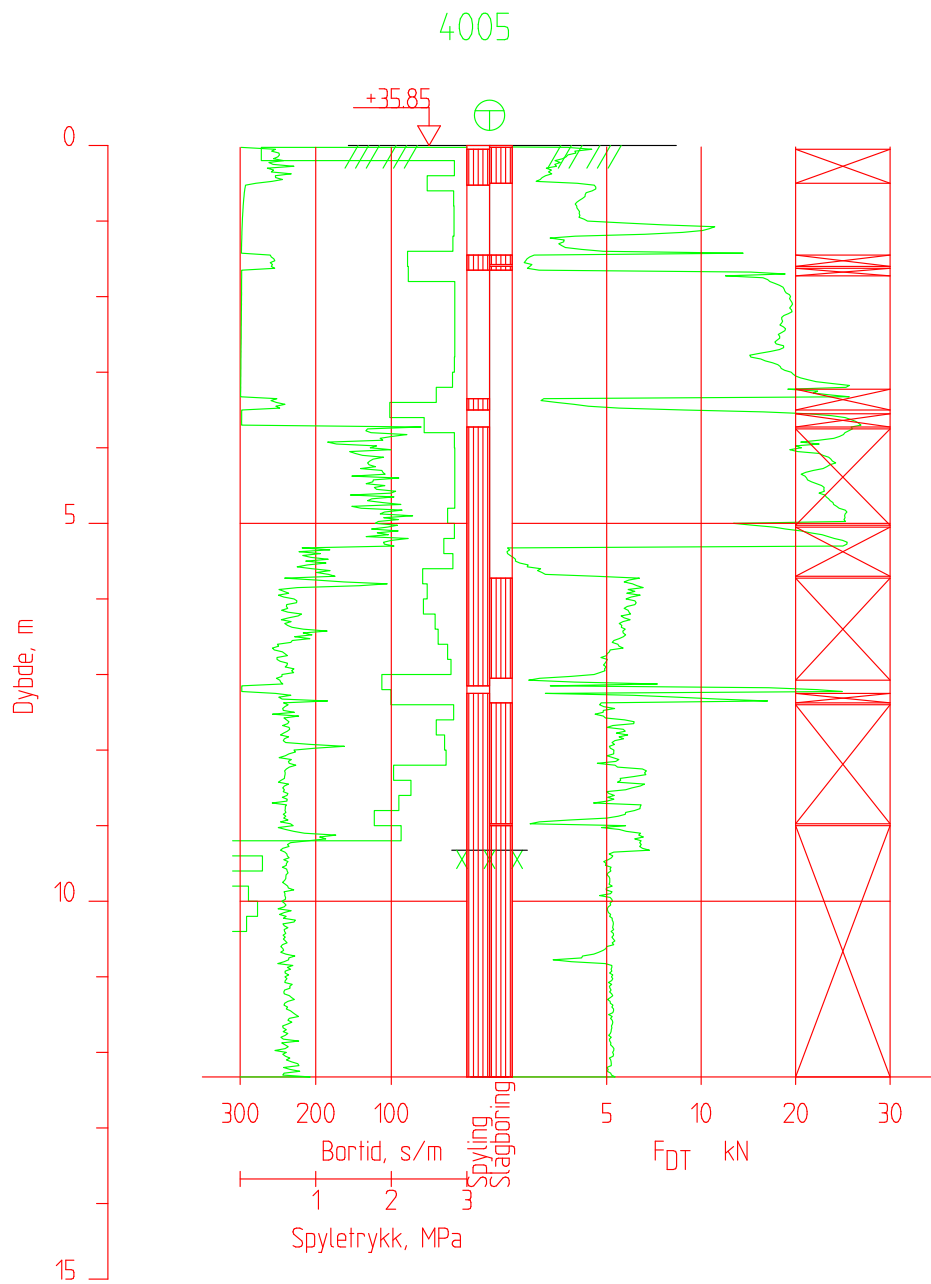
Borhull 4004

Dato boret :29.10.2018

M = 1 : 100

BG

19756



Posisjon: X 1124362.64 Y 112598.17

Totalsondering

Borhull 4005

Dato boret :29.10.2018

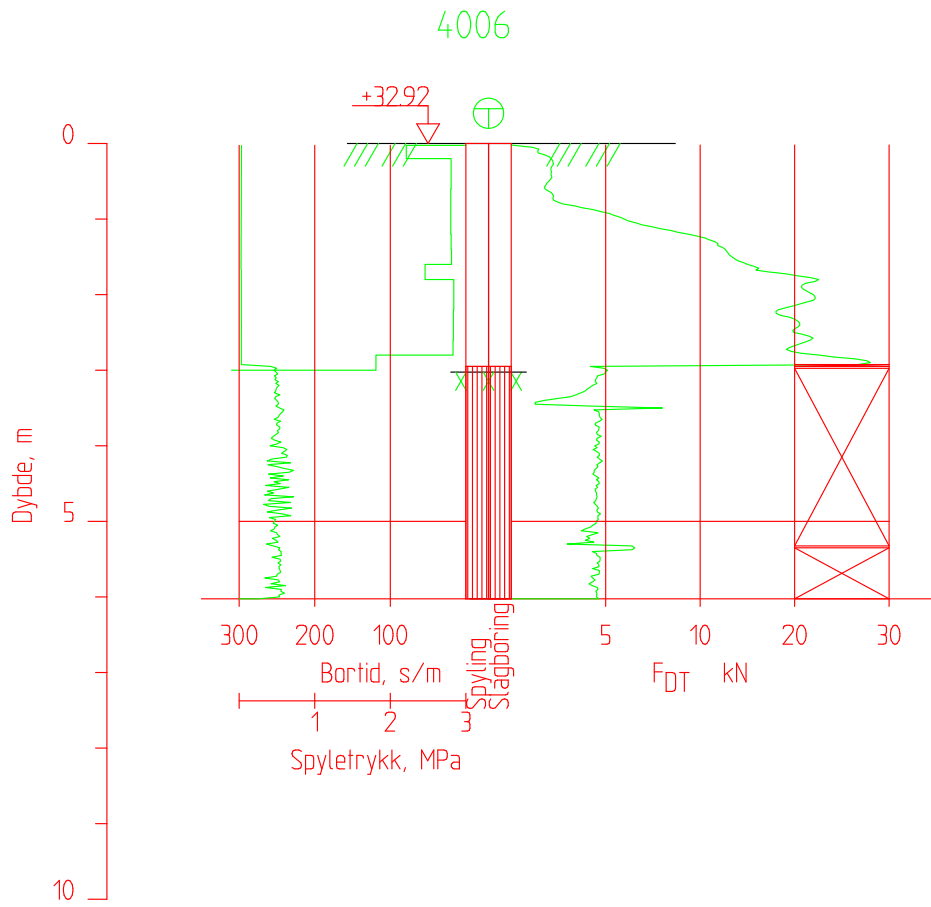
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124380.03 Y 112530.72

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

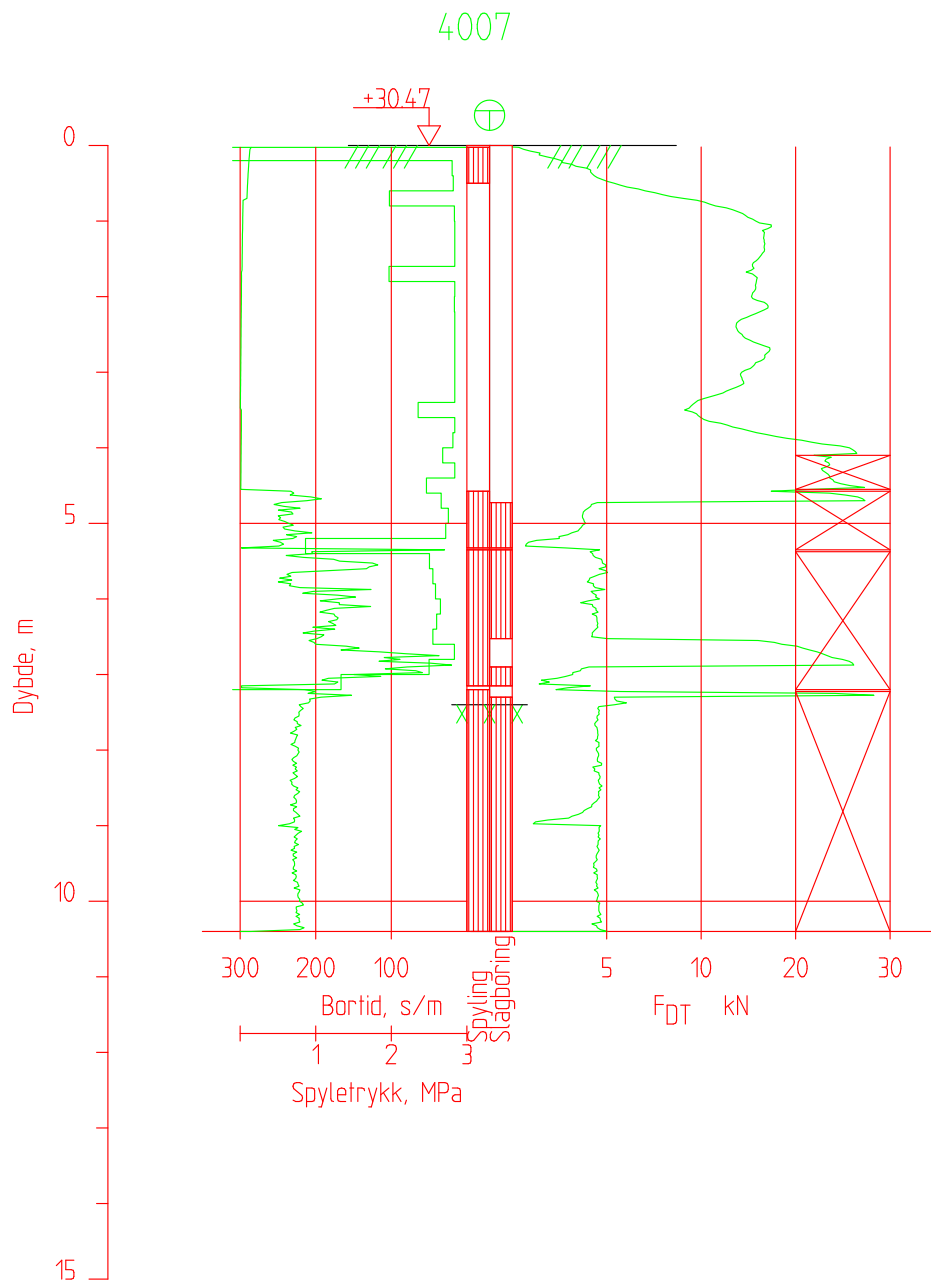
Borhull 4006

Dato boret :29.10.2018

$M = 1 : 100$

BG

19756



Posisjon: X 1124381.78 Y 112511.06

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

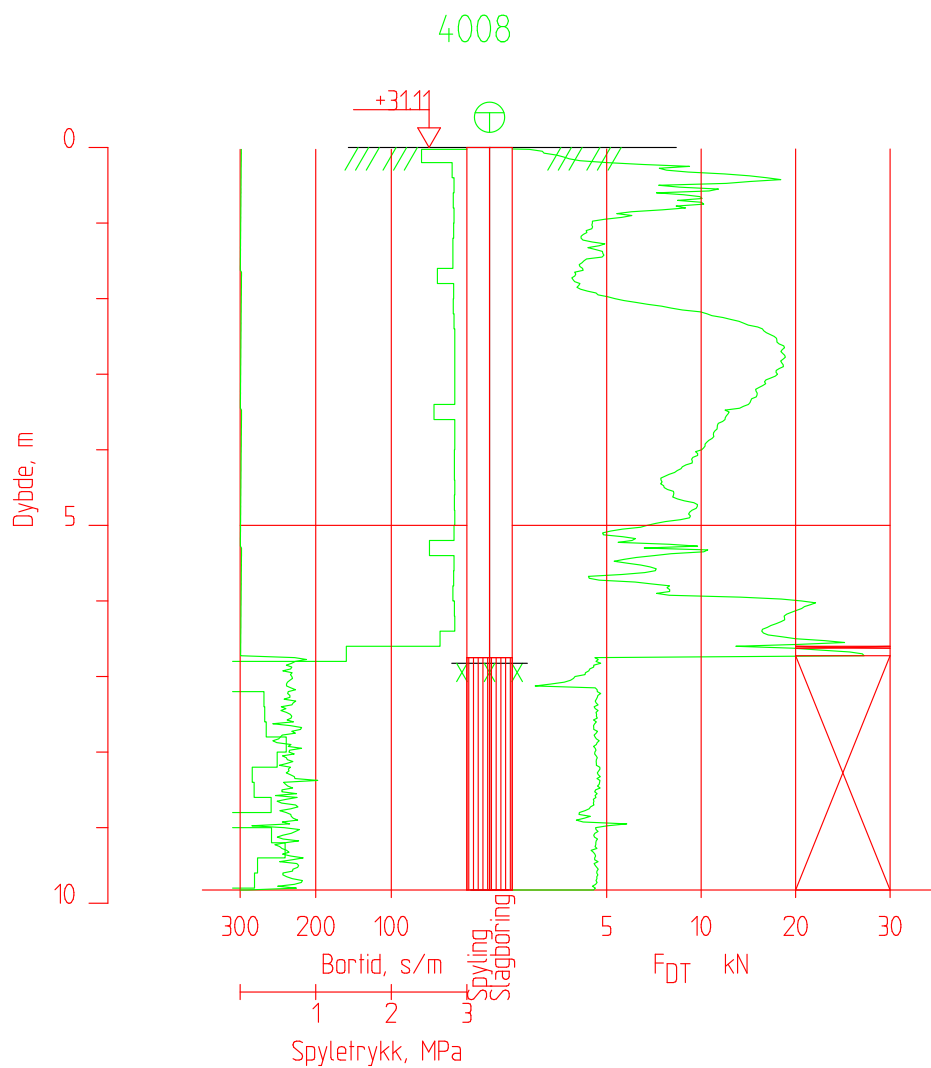
Borhull 4007

Dato boret :29.10.2018

M = 1 : 100

BG

19756



Posisjon: X 1124437.41 Y 112505.62

Totalsondering

Borhull 4008

Dato boret :29.10.2018

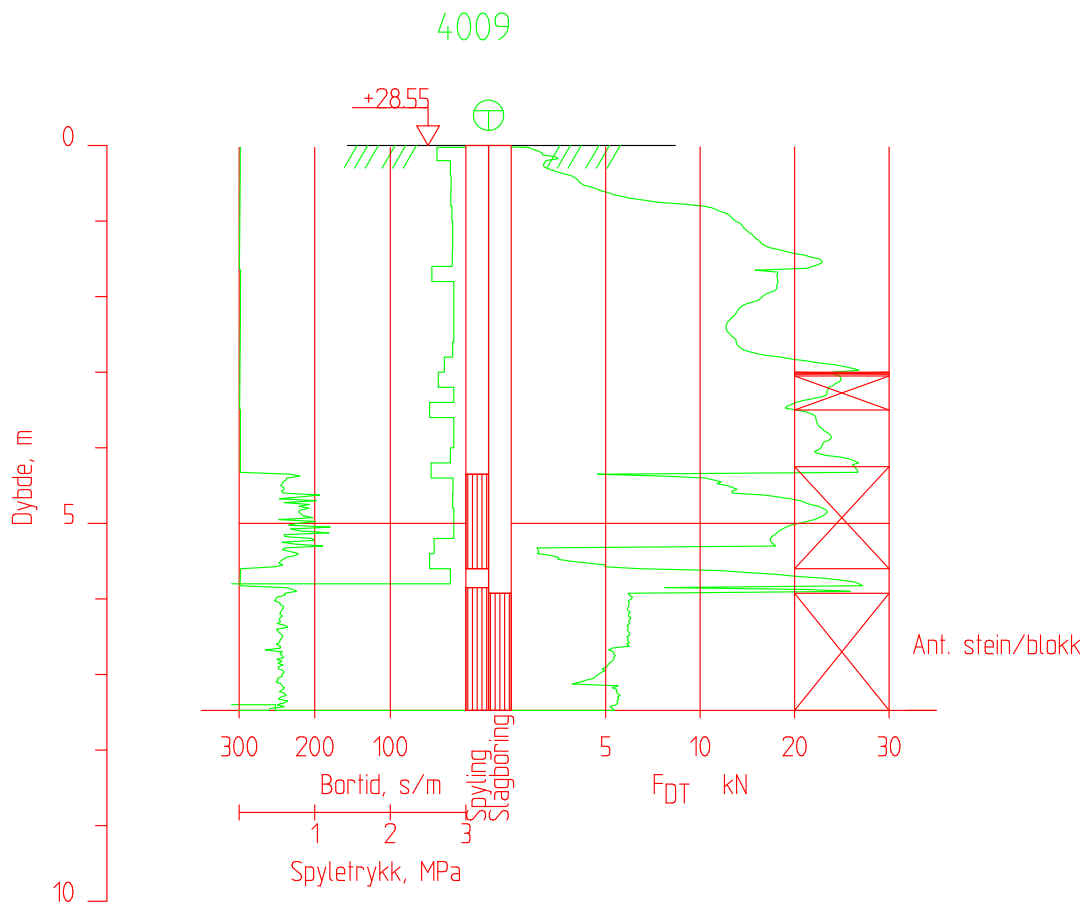
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124383.35 Y 112491.38

Totalsondering

Borhull 4009

Dato boret :25.10.2018

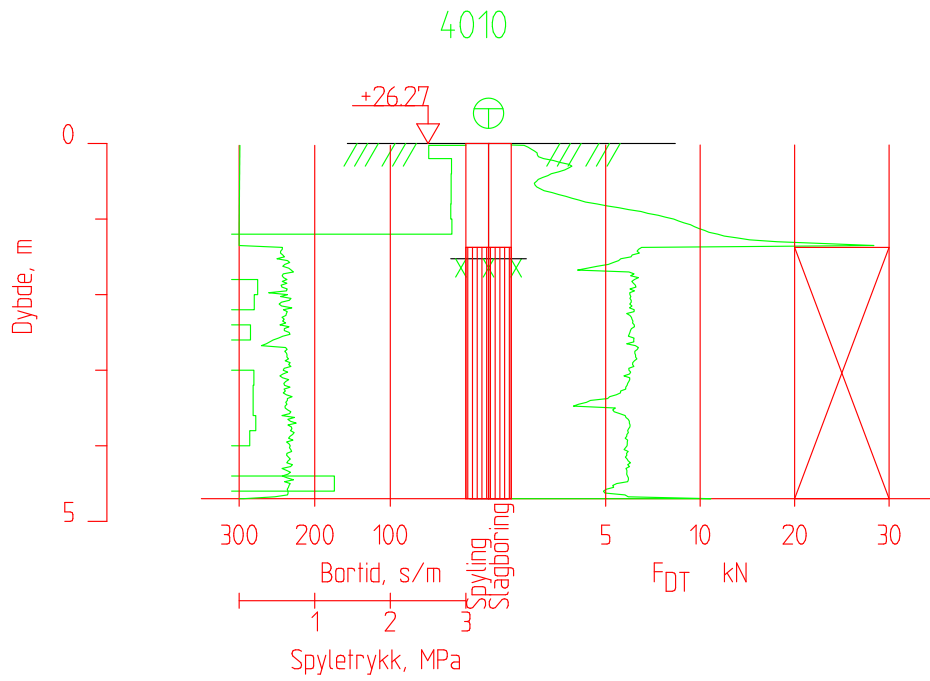
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124384.76 Y 112471.69

Totalsondering

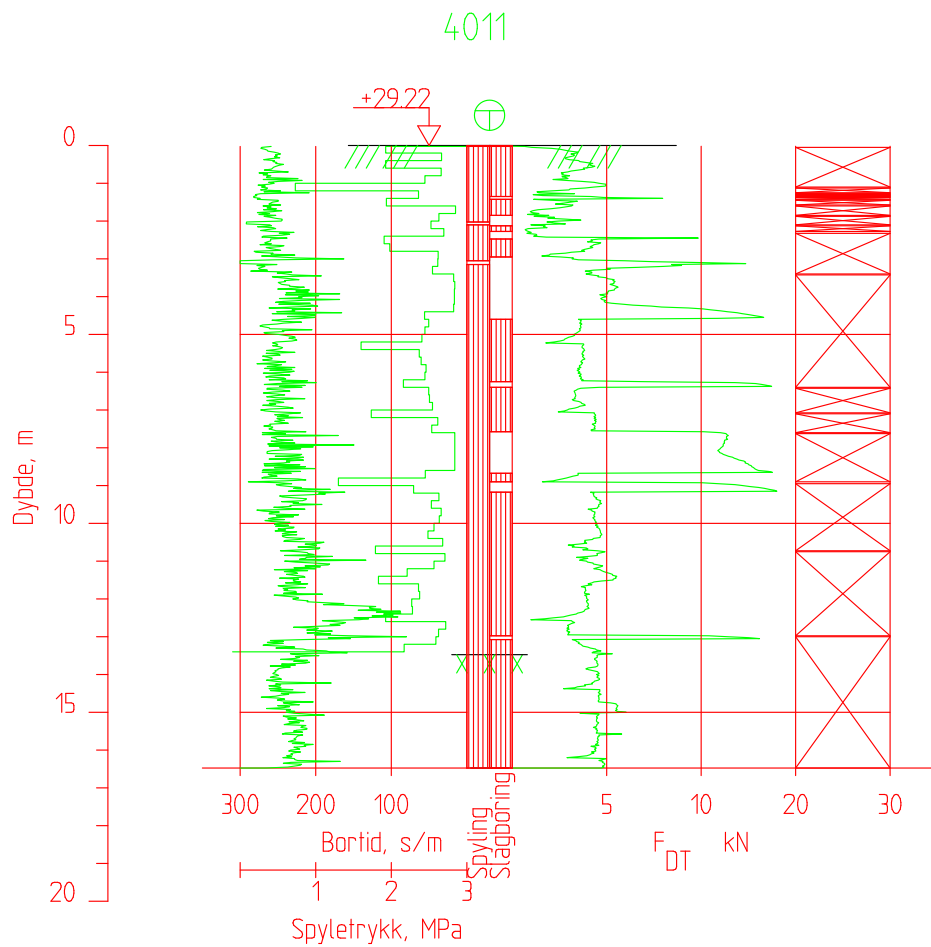
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E18 Langangen Rugtvedt

Borhull 4010

Dato borete :25.10.2018

M = 1 : 100



Posisjon: X 1124437.59 Y 112471.80

Totalsondering

Borhull 4011

Dato boret :07.11.2018

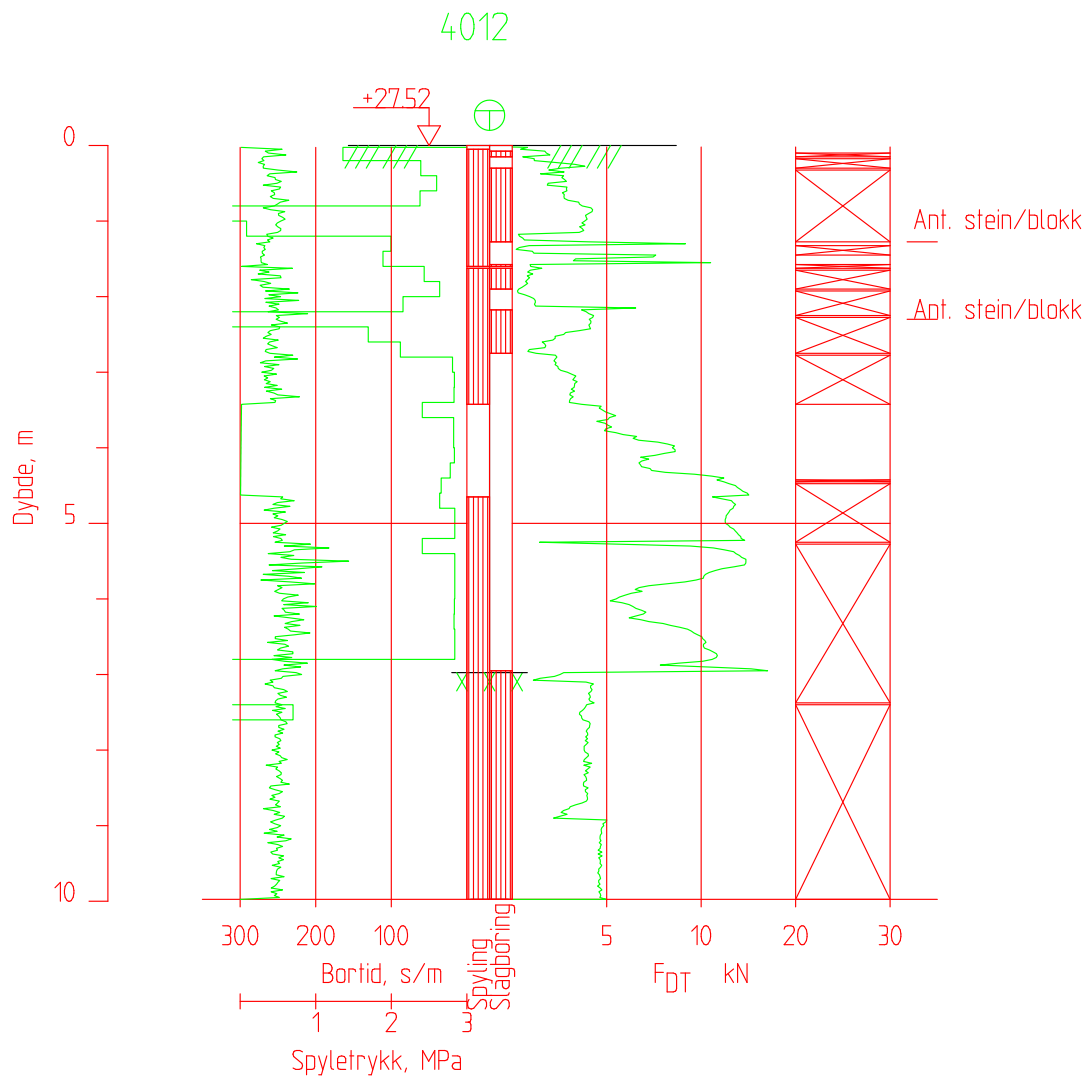
EIFFAGE

M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124422.78 Y 112461.43

Totalsondering

Borhull 4012

Dato boret :07.11.2018

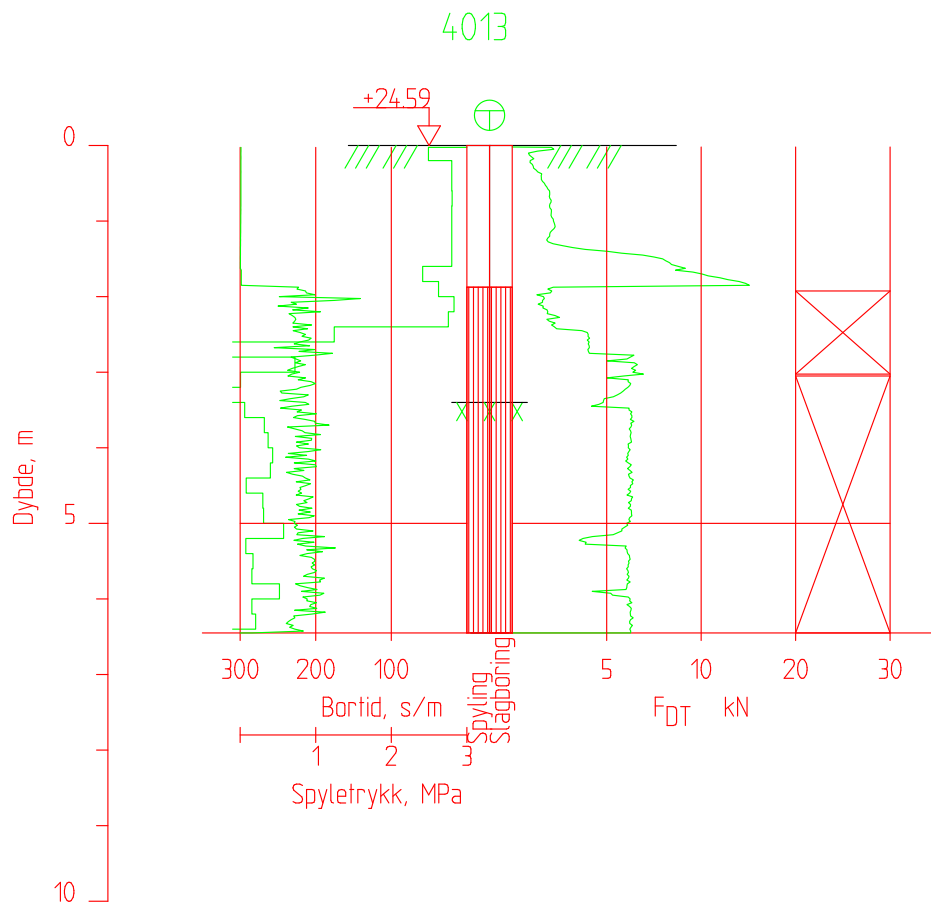
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124381.01 Y 112451.70

Totalsondering

Borhull 4013

Dato boret :25.10.2018

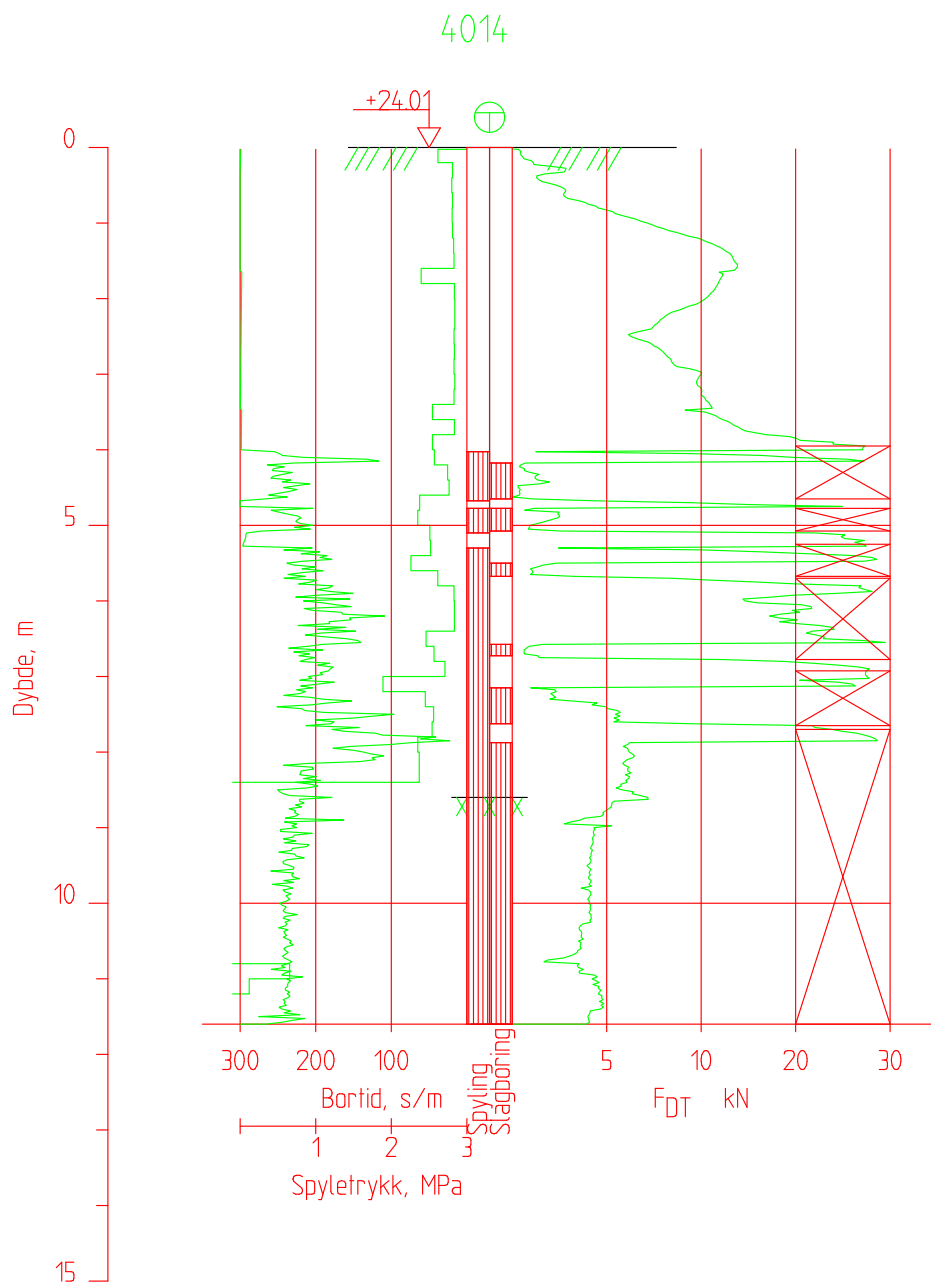
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124441.92 Y 112456.67

Totalsondering

Borhull 4014

Dato boret :06.11.2018

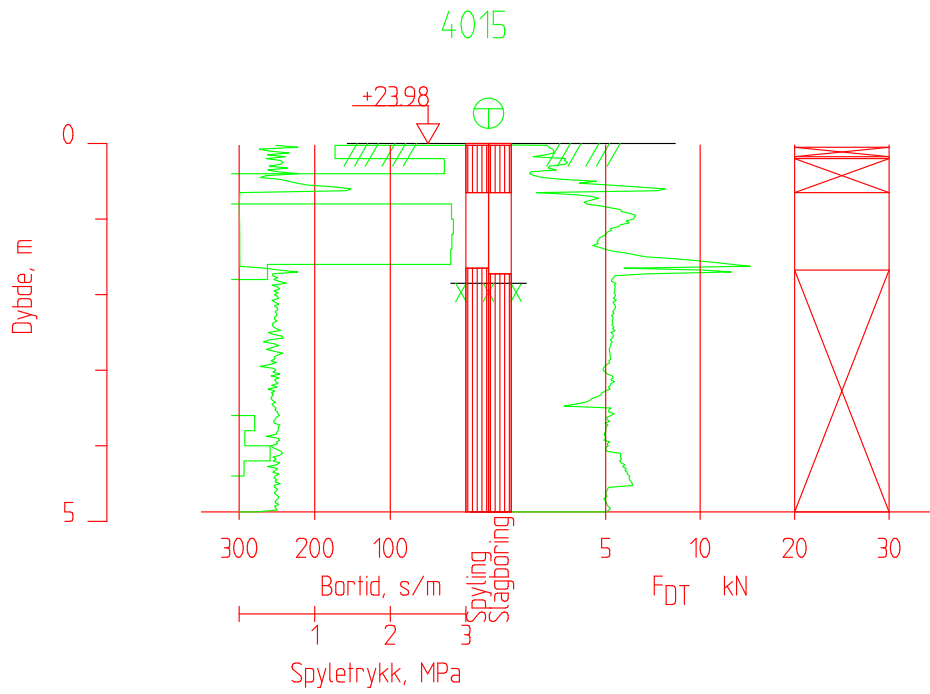
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124416.90 Y 112441.62

Totalsondering

Borhull 4015

Dato boret :06.11.2018

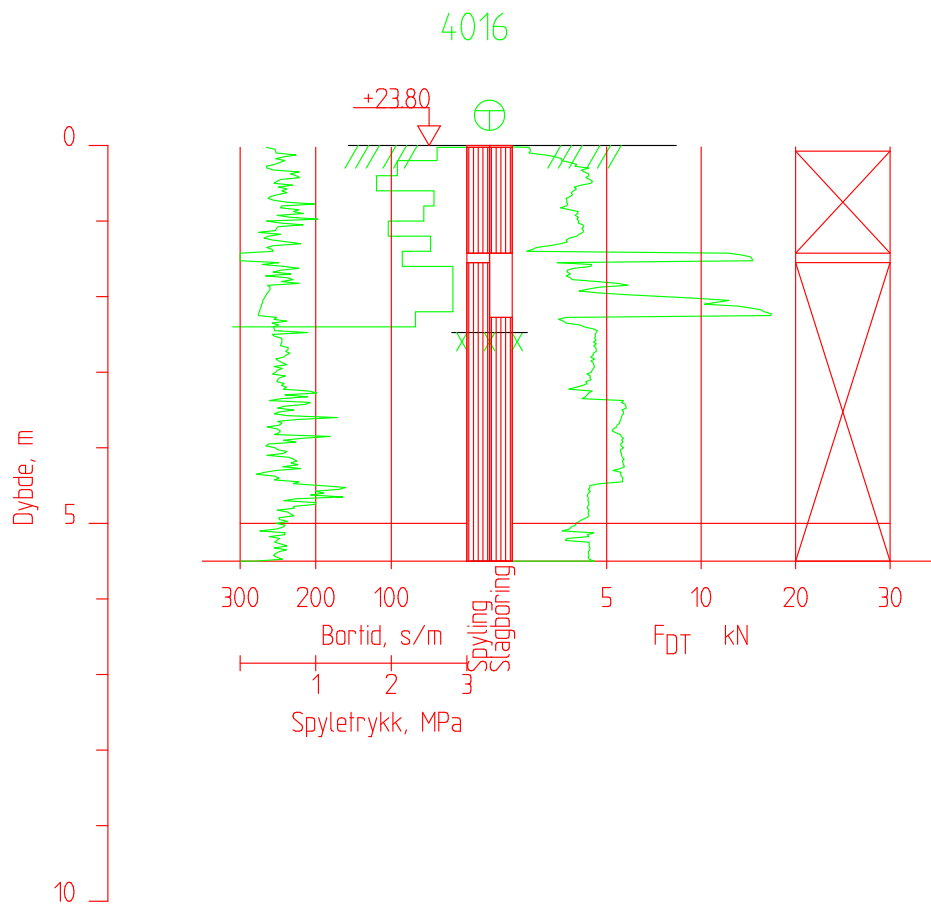
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124382.81 Y 112431.03

Totalsondering

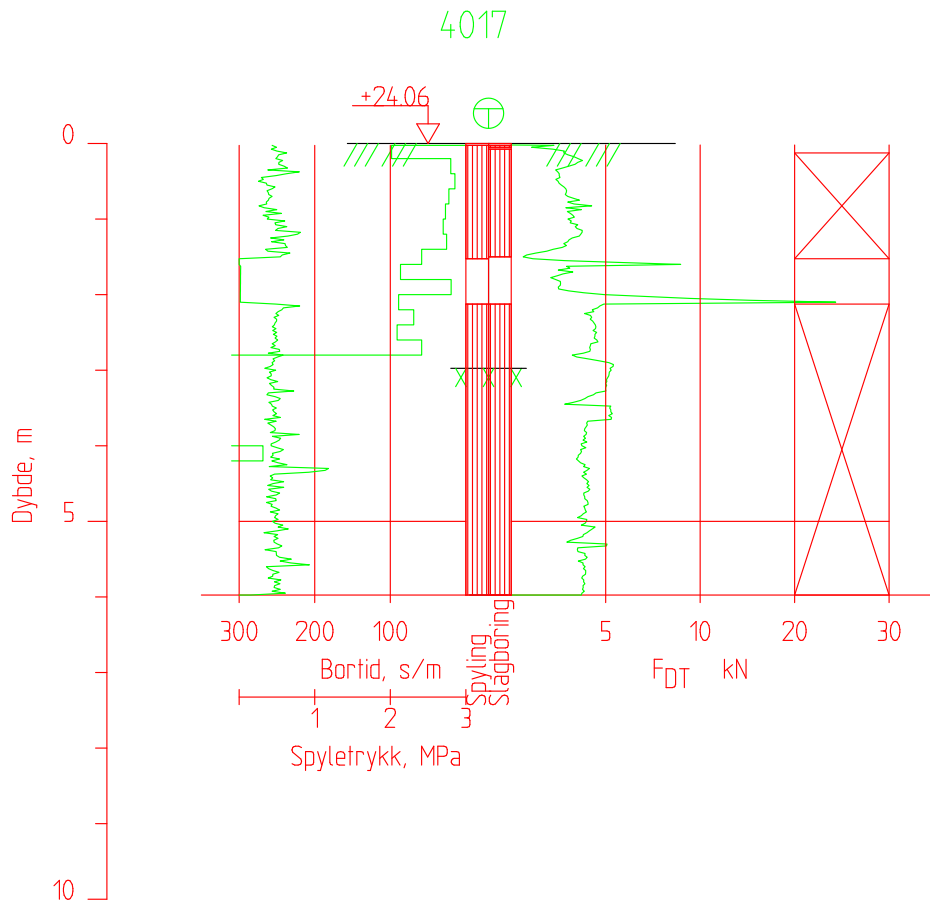
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E18 Langangen Rugtvedt

Borhull 4016

Dato boret :07.11.2018

M = 1 : 100



Posisjon: X 1124417.02 Y 112433.77

Totalsondering

Borhull 4017

Dato boret :06.11.2018

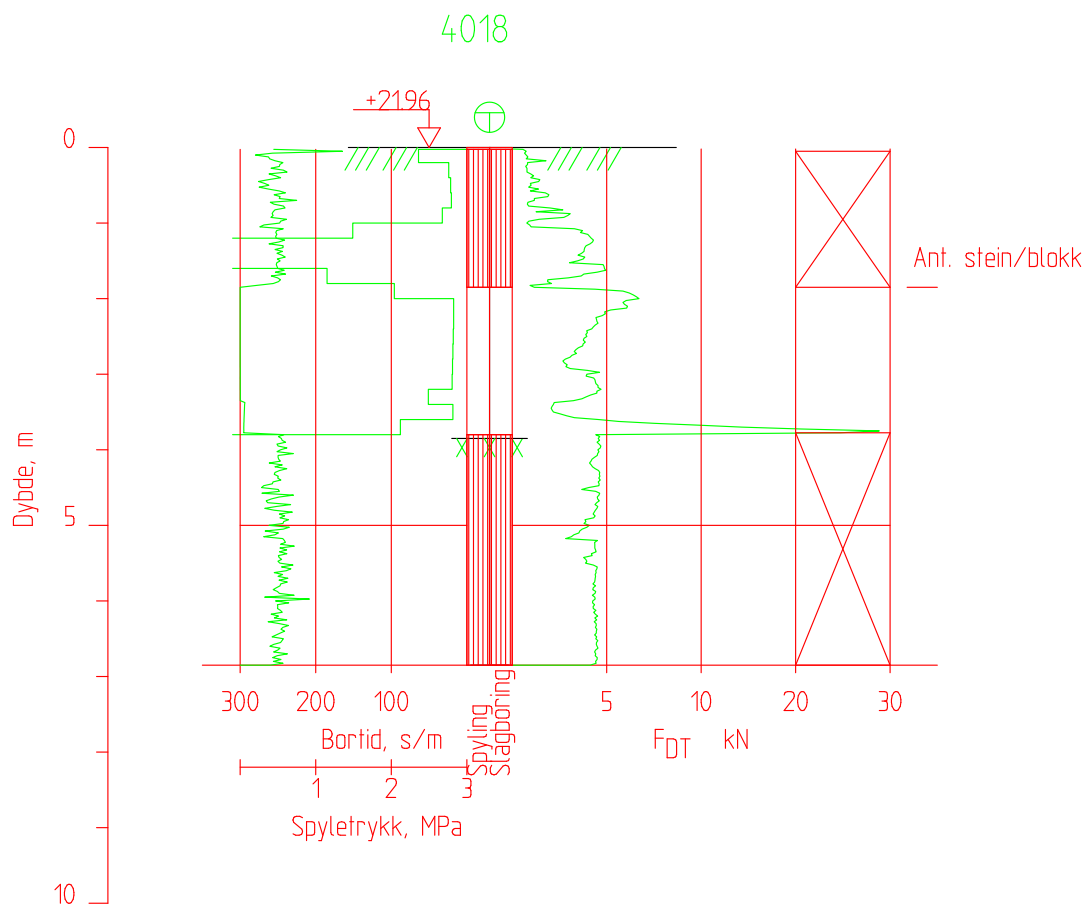
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124441.56 Y 112422.83

Totalsondering

Borhull 4018

Dato boret :07.11.2018

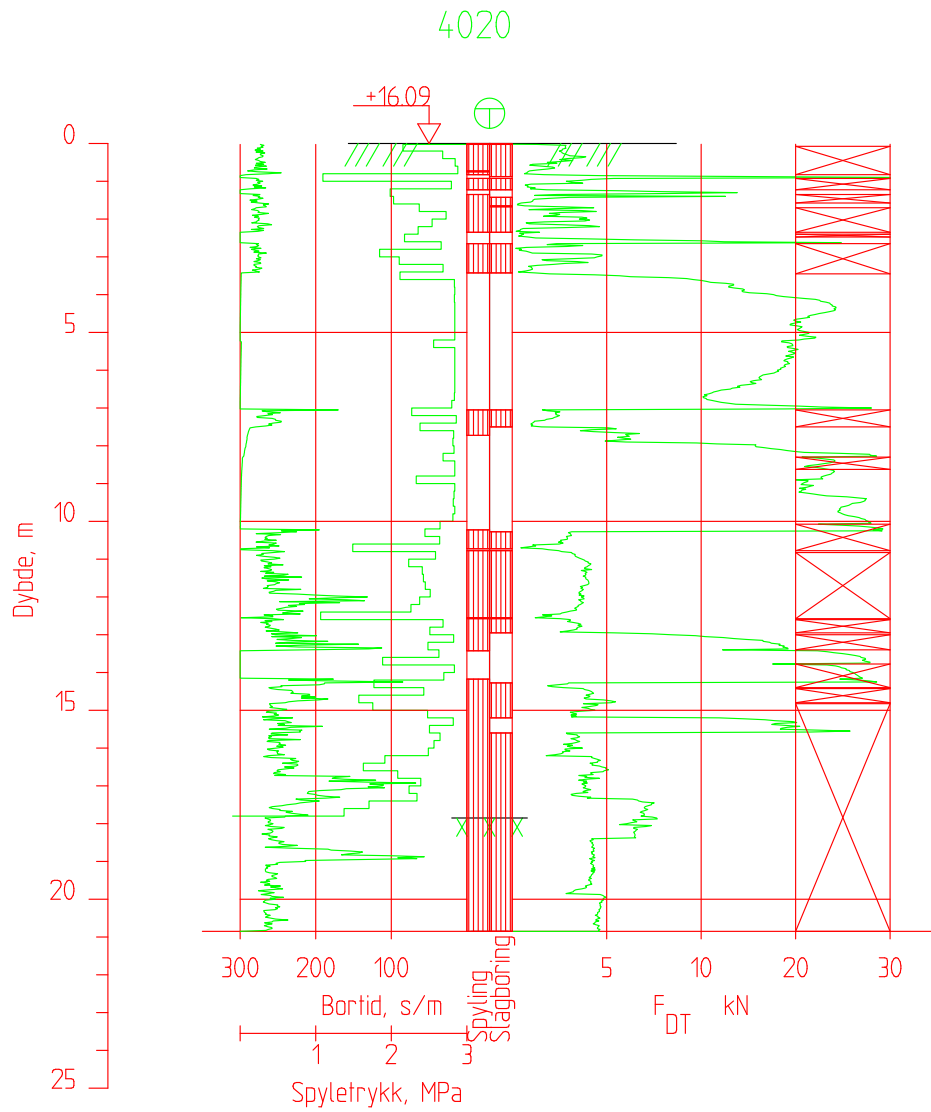
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124388.35 Y 112394.68

Totalsondering

Borhull 4020

Dato boret :25.10.2018

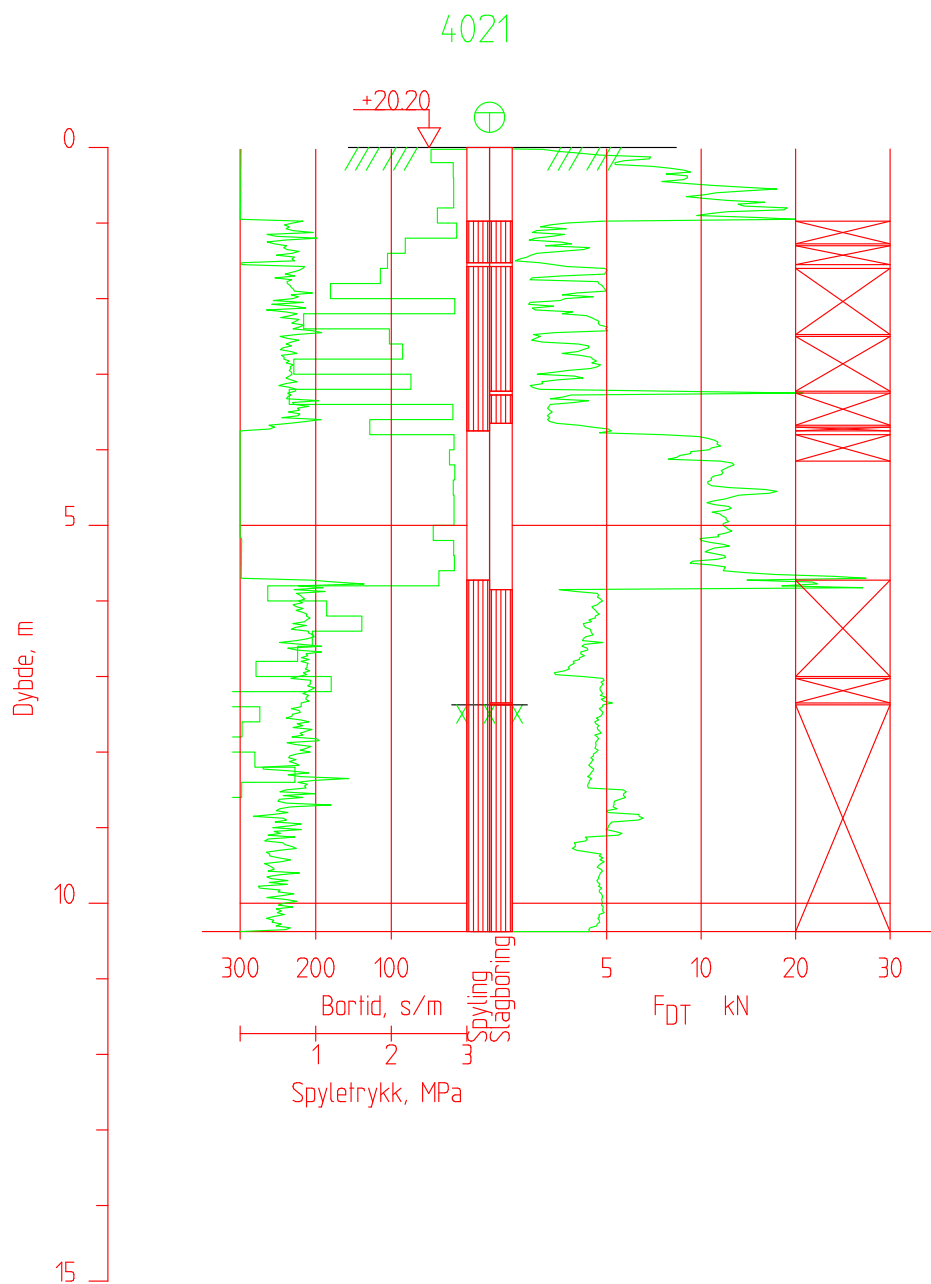
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124443.64 Y 112394.61

Totalsondering

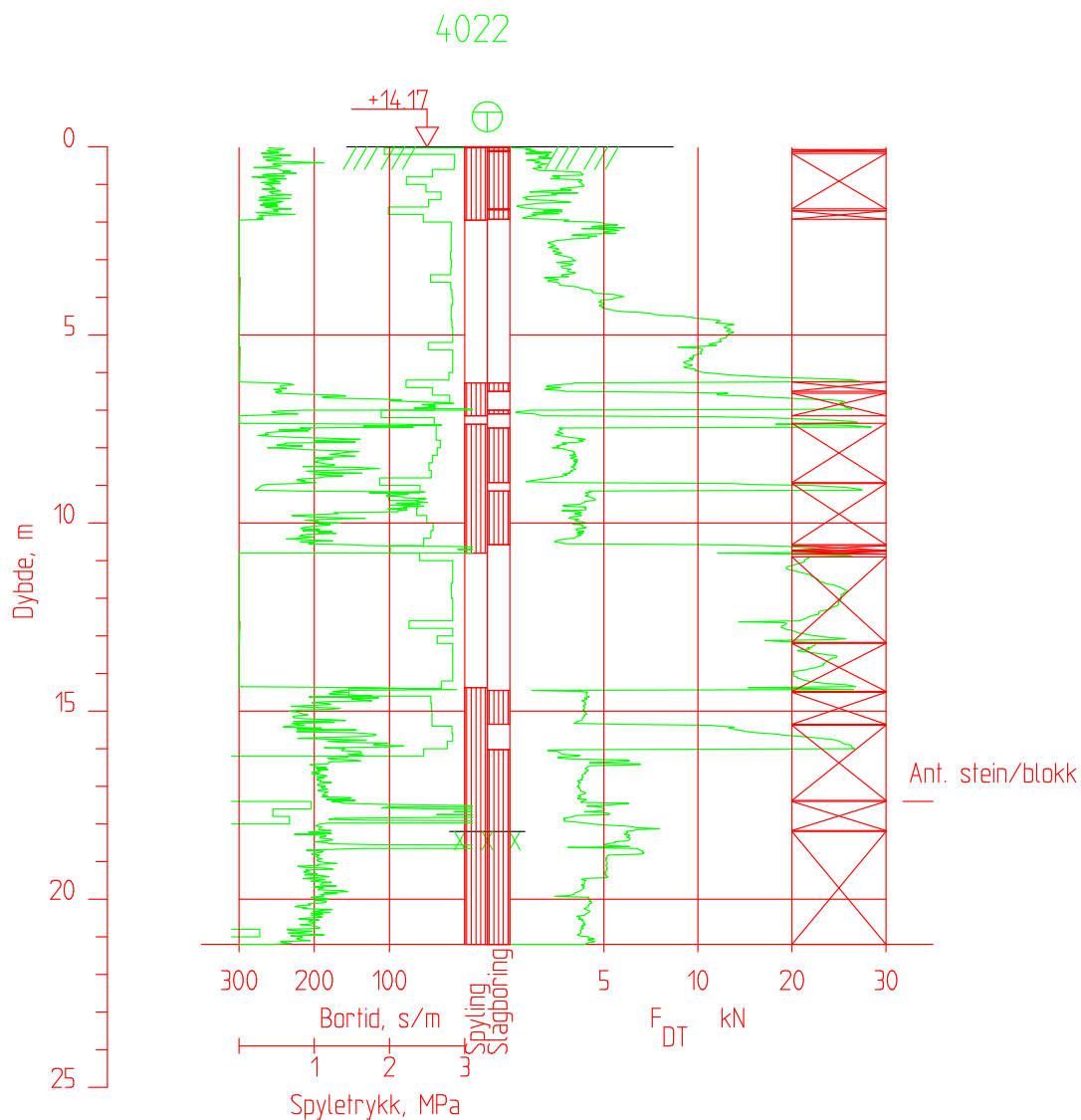
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E18 Langangen Rugtvedt

Borhull 4021

Dato boret :24.10.2018

M = 1 : 100



Posisjon: X 1124389.22 Y 112373.11

Totalsondering

Borhull 4022

Dato boret :25.10.2018

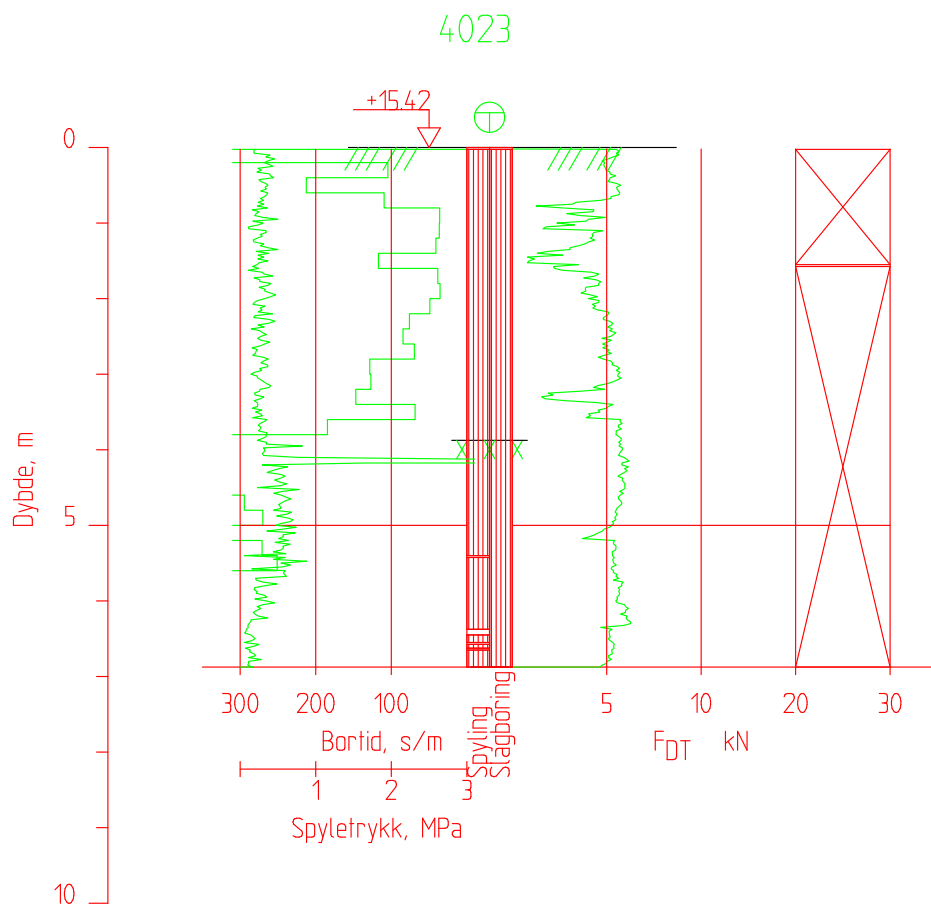
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124444.21 Y 112374.40

Totalsondering

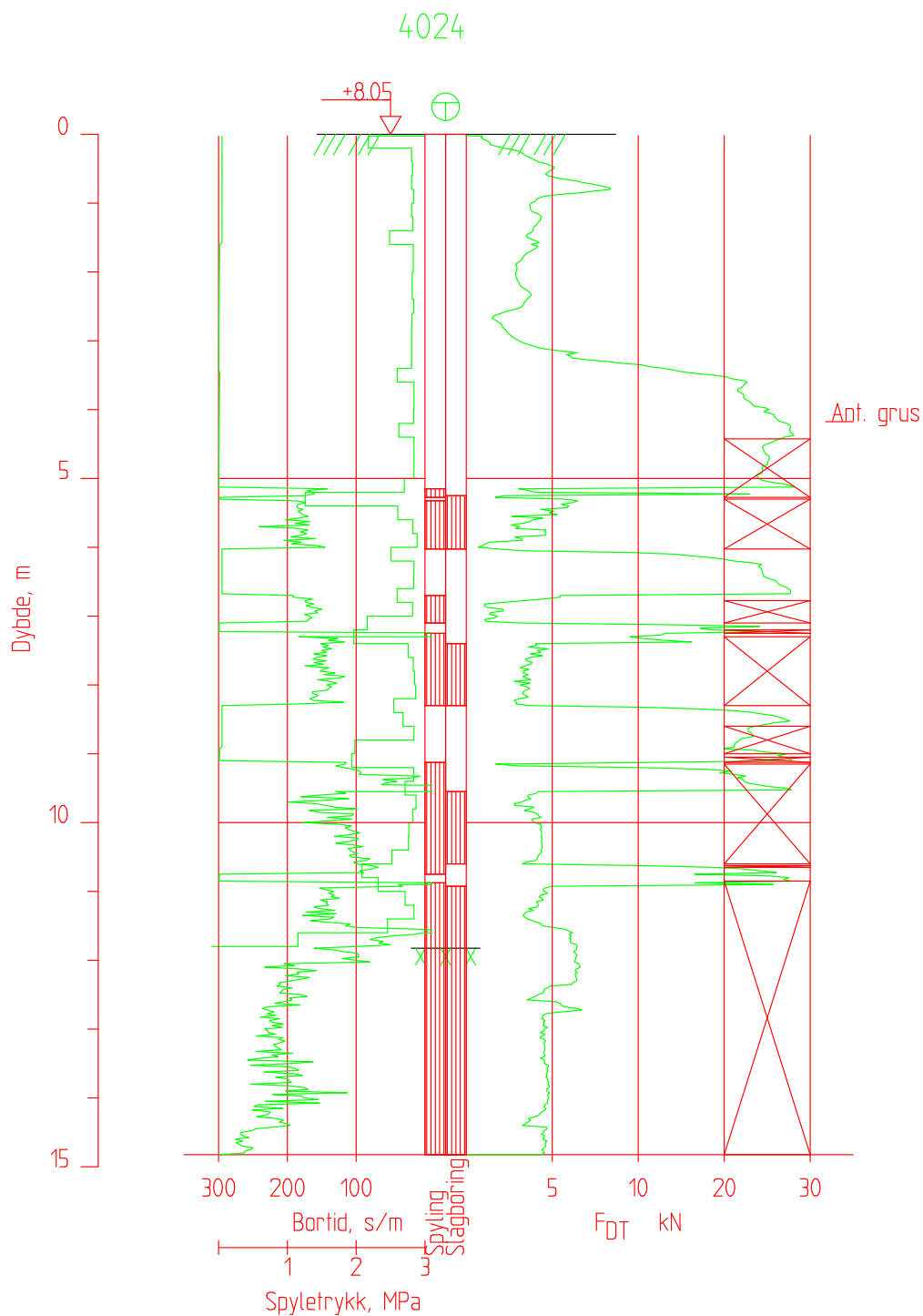
Borhull 4023

Dato boret :24.10.2018

EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt



Posisjon: X 1124389.60 Y 112353.37

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

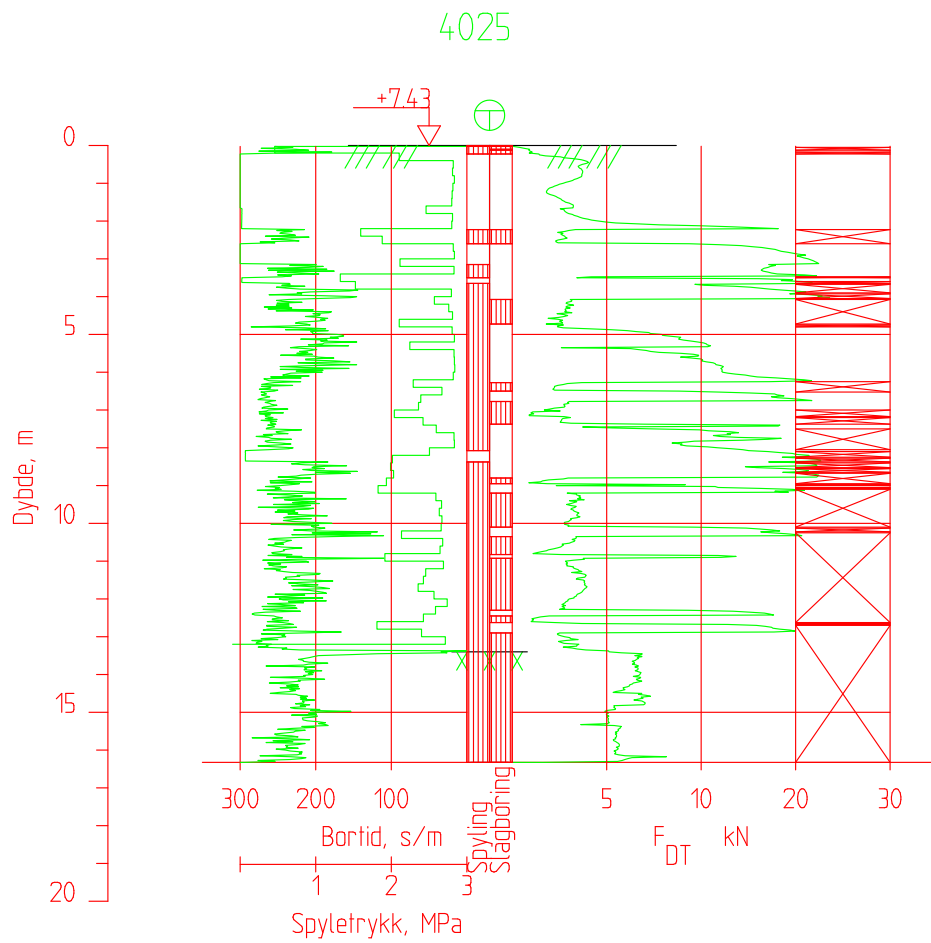
Borhull 4024

Dato boret :24.10.2018

M = 1 : 100

BG

19756



Posisjon: X 1124419.60 Y 112353.82

Totalsondering

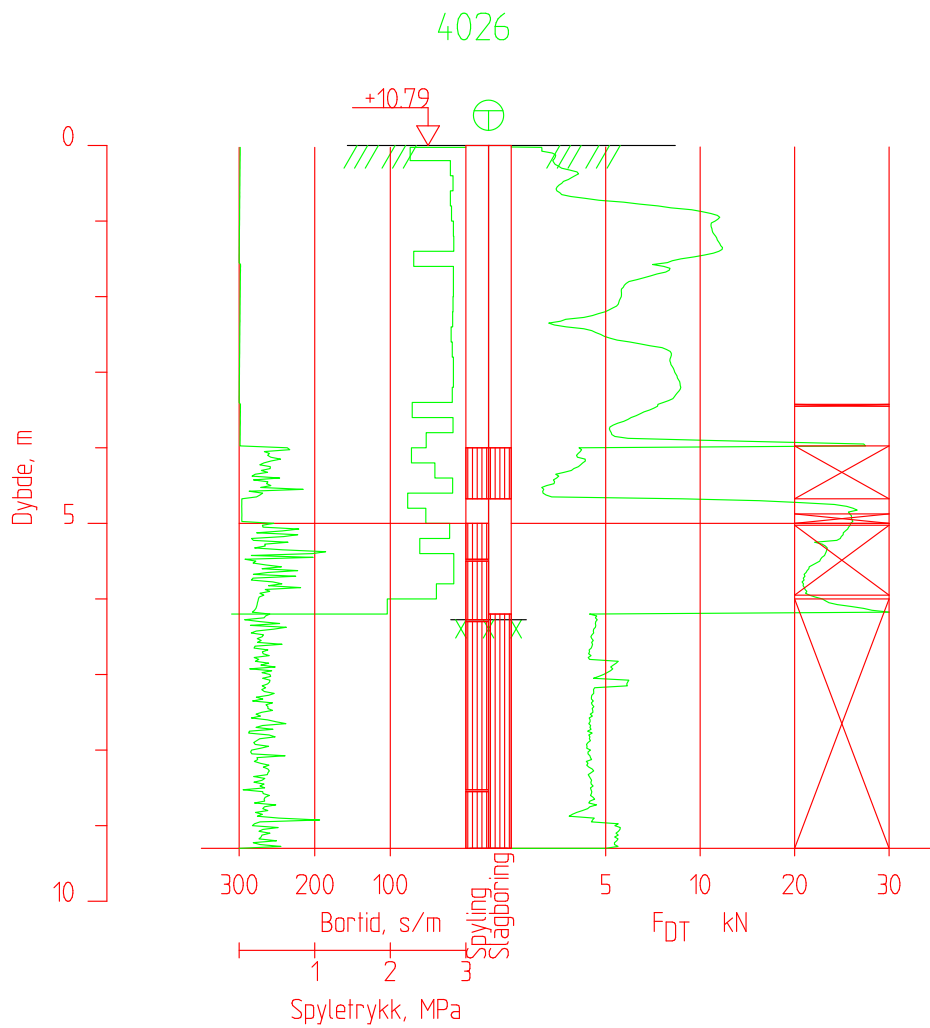
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E18 Langangen Rugtvedt

Borhull 4025

Dato boret :23.10.2018

M = 1 : 200



Posisjon: X 1124442.67 Y 112354.18

Totalsondering

Borhull 4026

Dato boret :24.10.2018

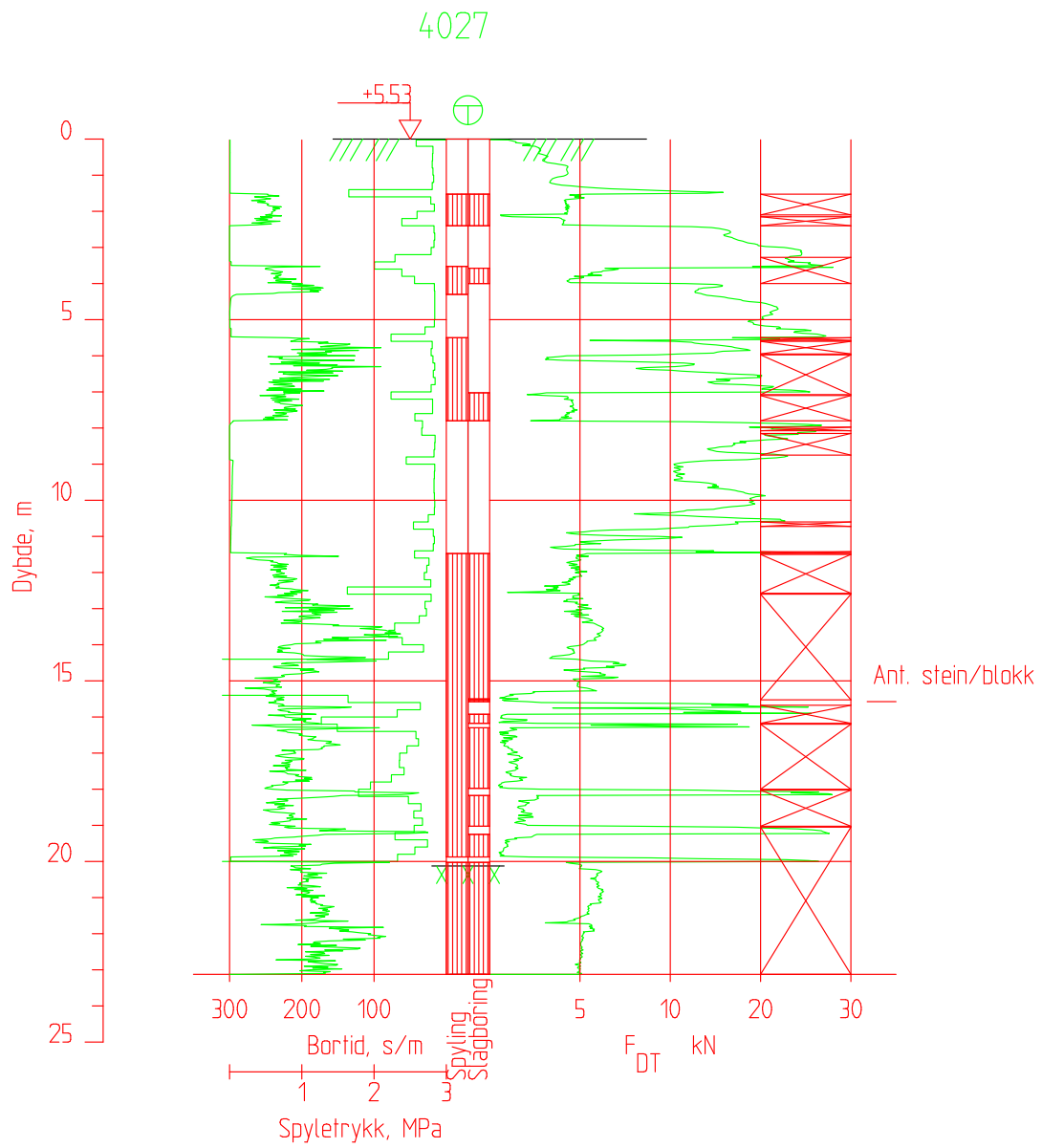
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124419.72 Y 112343.82

Totalsondering

Borhull 4027

Dato boret :23.10.2018

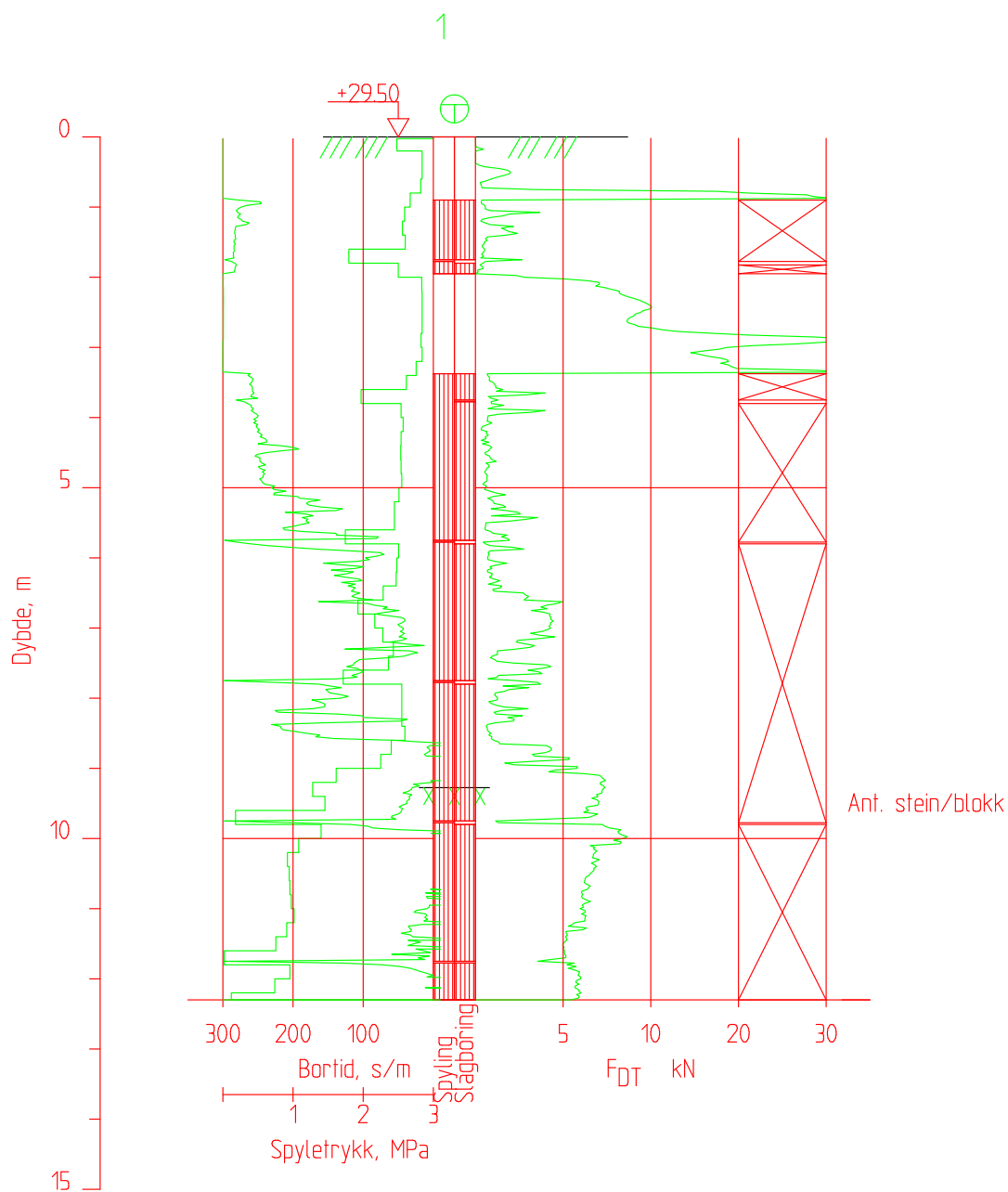
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124399.02 Y 112629.97

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

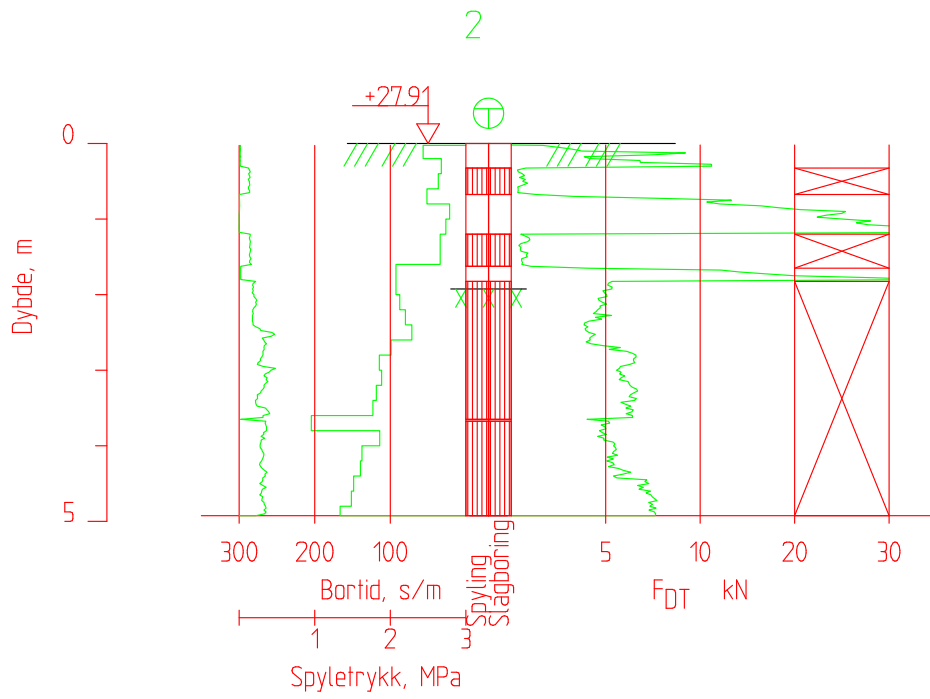
Borhull 1

Dato boret :07.11.2016

M = 1 : 100

BG

19756



Posisjon: X 1124377.36 Y 112629.23

Totalsondering

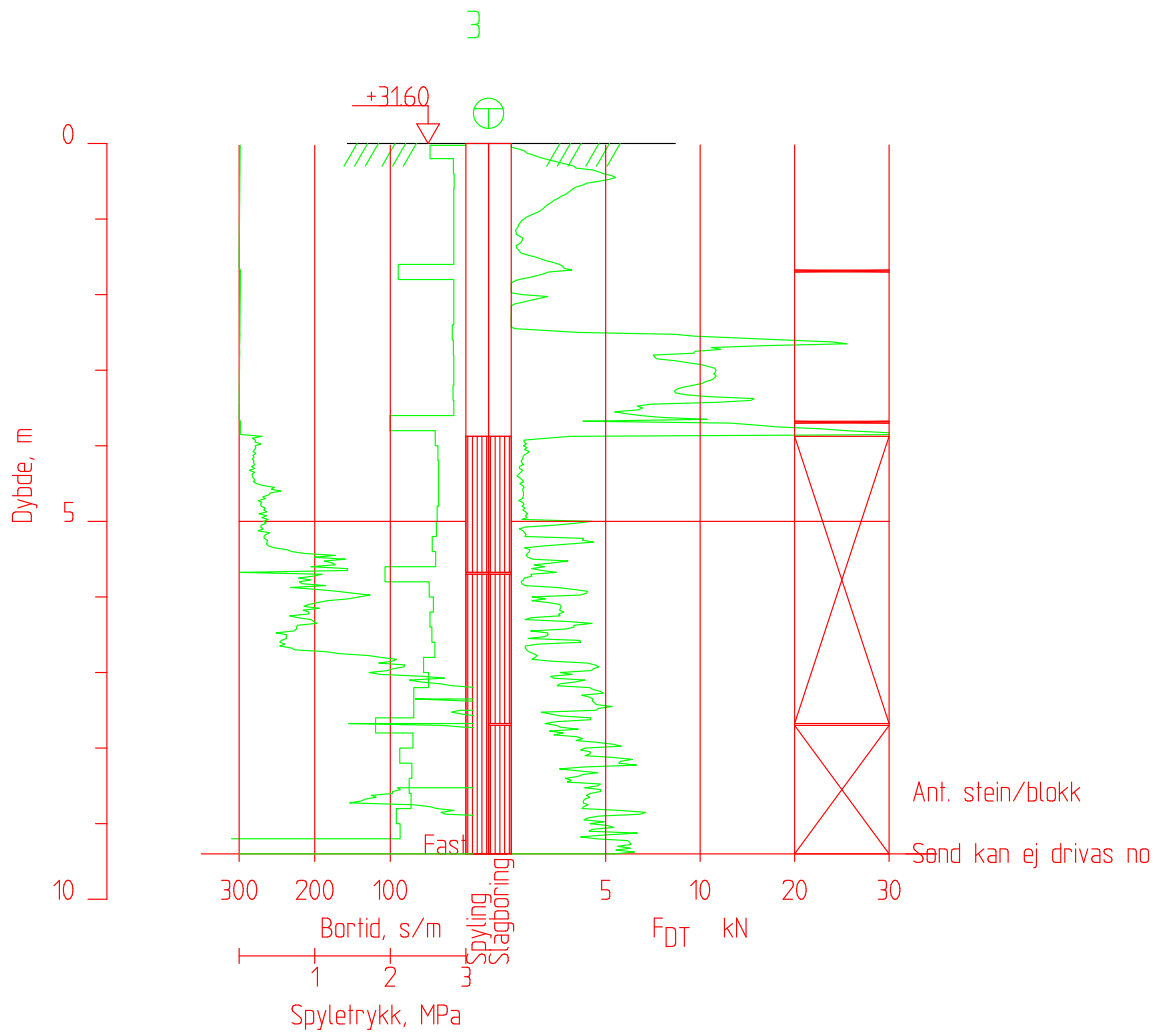
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E18 Langangen Rugtvedt

Borhull 2

Dato boref :07.11.2016

M = 1 : 100



Posisjon: X 1124414.50 Y 112631.93

Totalsondering

Borhull 3

Dato boret :03.11.2016

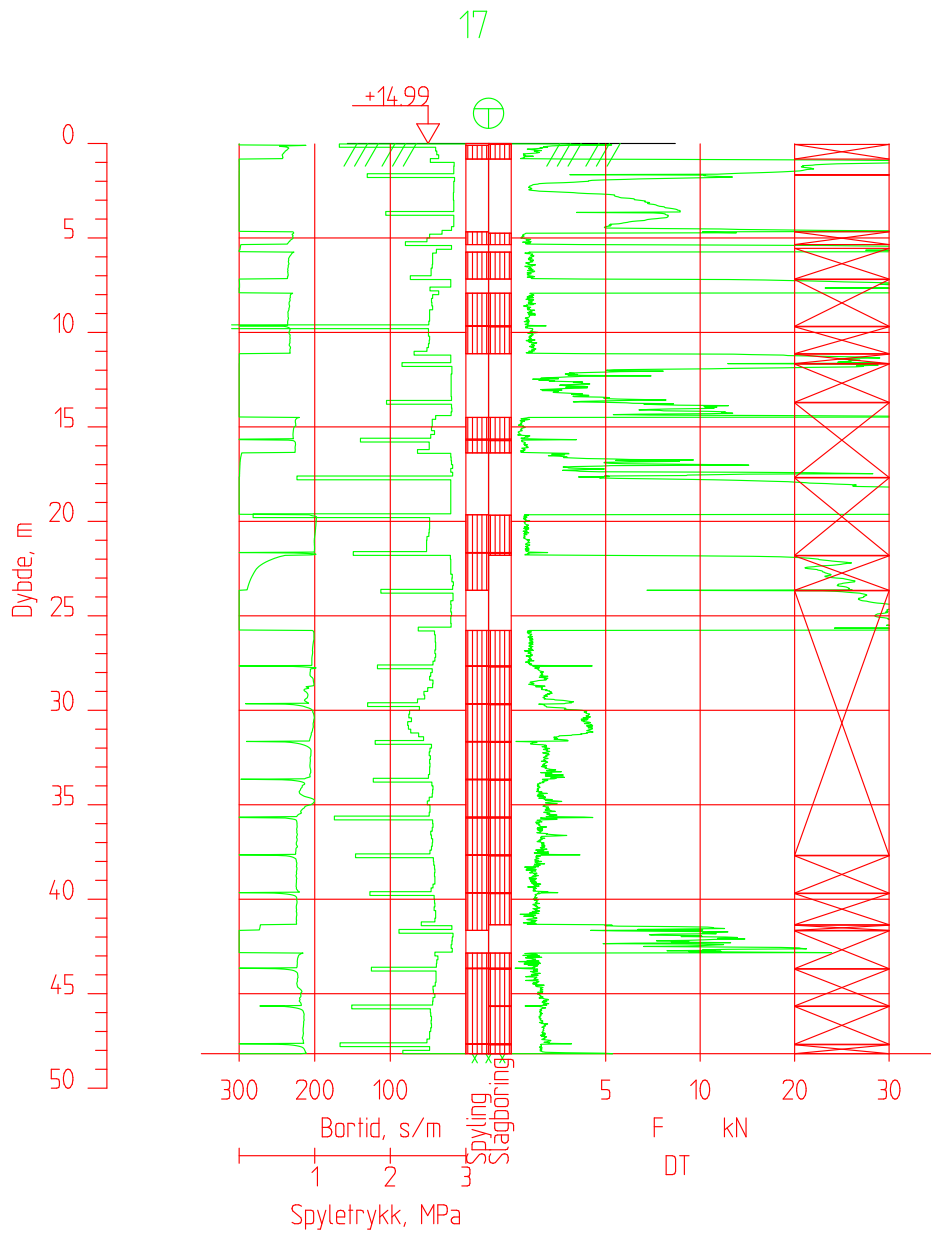
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1124413.27 Y 112155.75

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

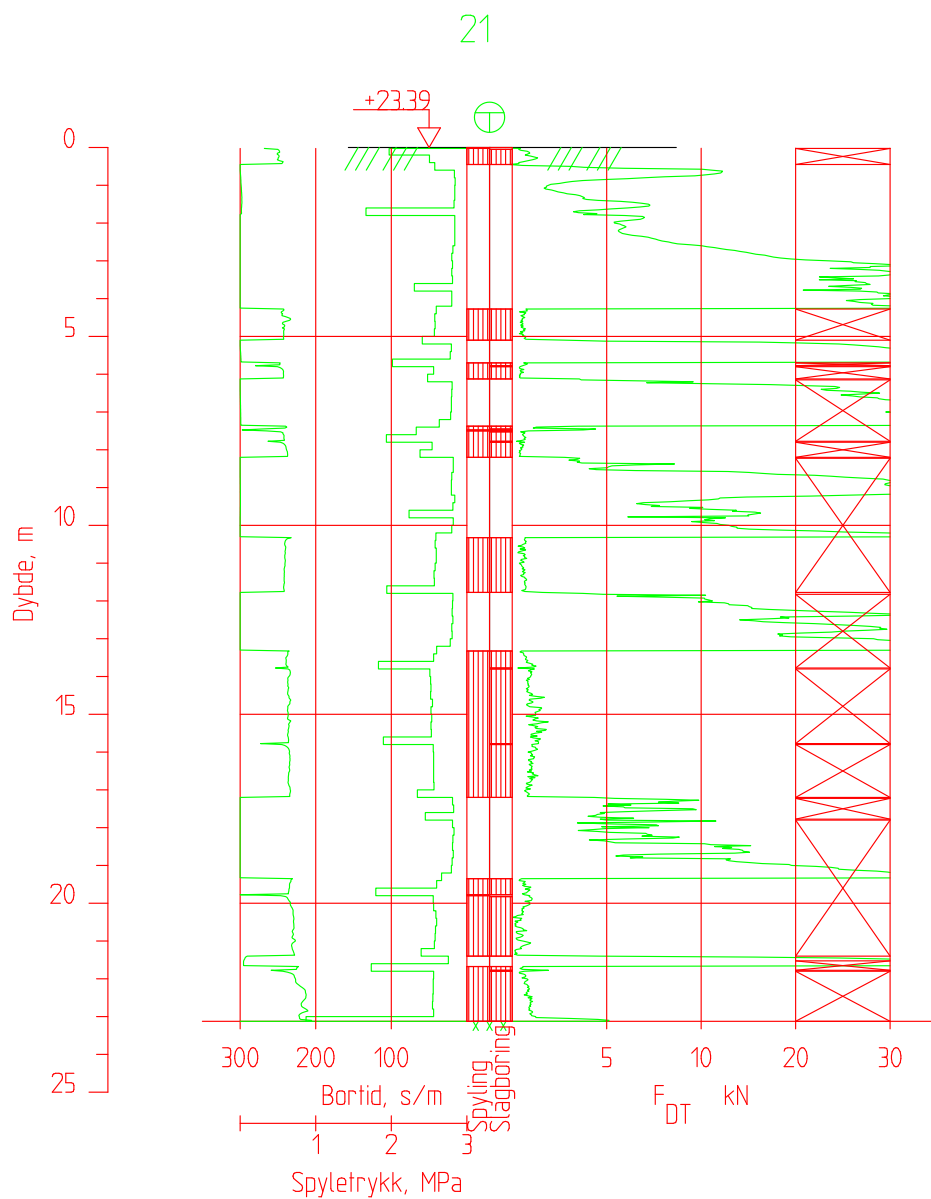
Borhull 17

Dato boret :23.01.2017

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BG

19756



Posisjon: X 1124408.54 Y 112091.17

Totalsondering

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E18 Langangen Rugtvedt

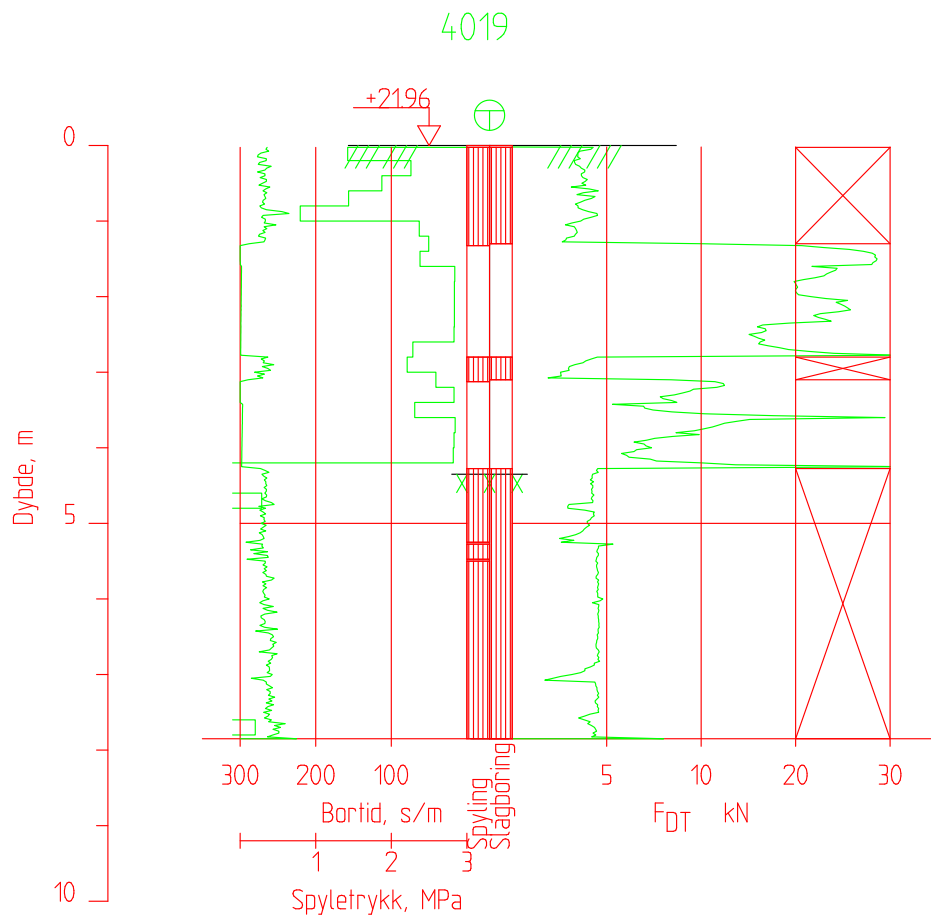
Borhull 21

Dato borete :19.01.2017

M = 1 : 200

BG

19756



Posisjon: X 1124387.95 Y 112412.57

Totalsondering

Borhull 4019

Dato boret :07.11.2018

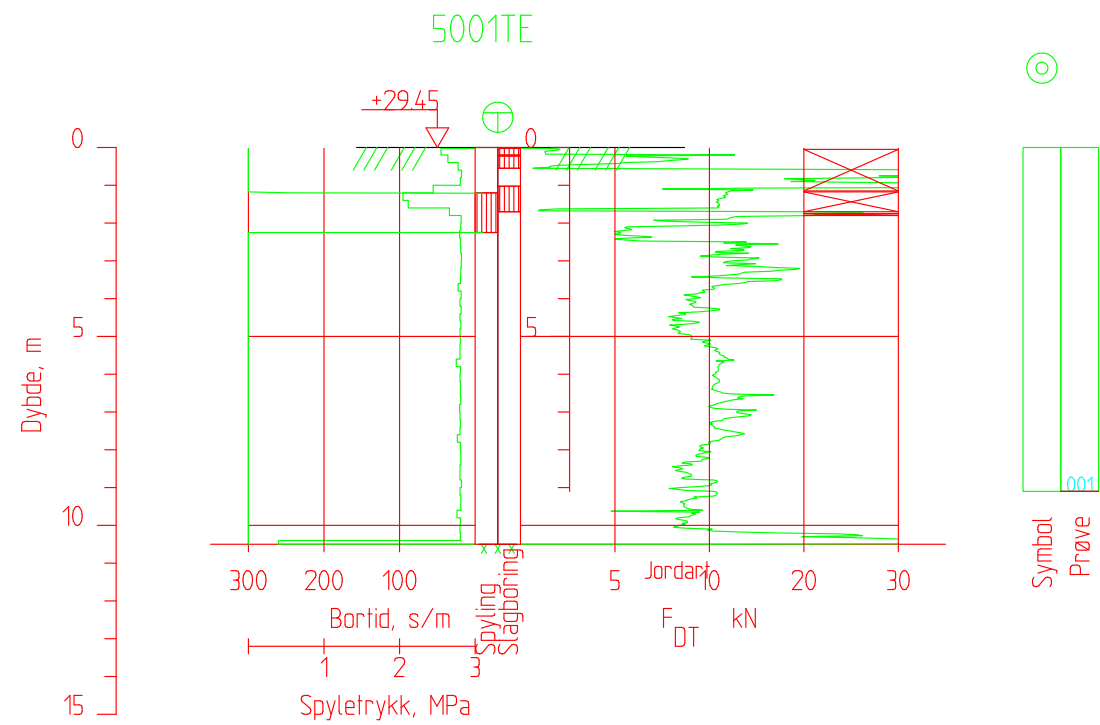
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



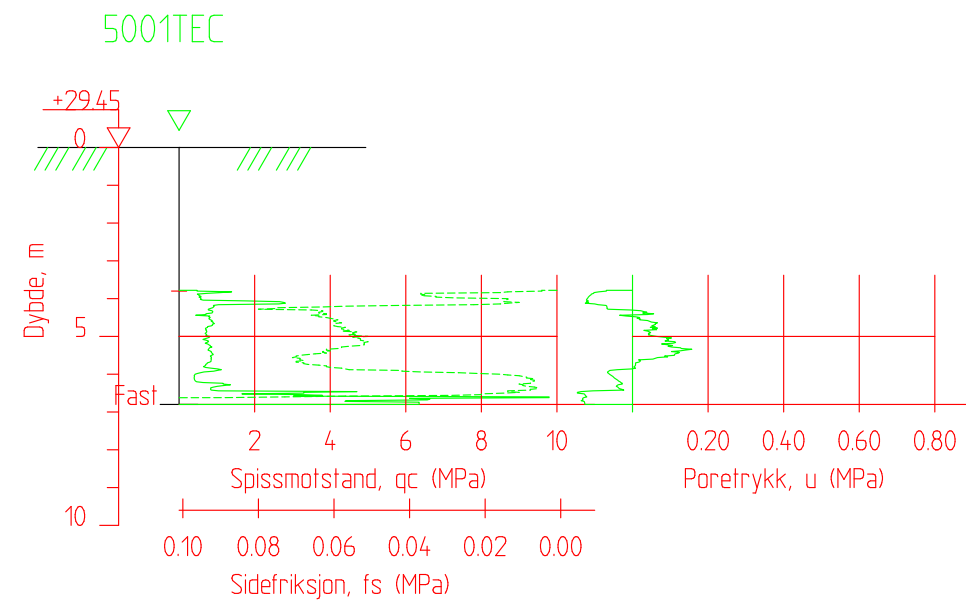
Posisjon: X 1122686.87 Y 109742.64

Totalsondering Borprofil
EIFFAGE
E18 Langangen Rugtvedt

Borhull 5001TE

Dato borete :30.06.2020

M = 1 : 200



Posisjon: X 1122686.87 Y 109742.64

CPT-sondering

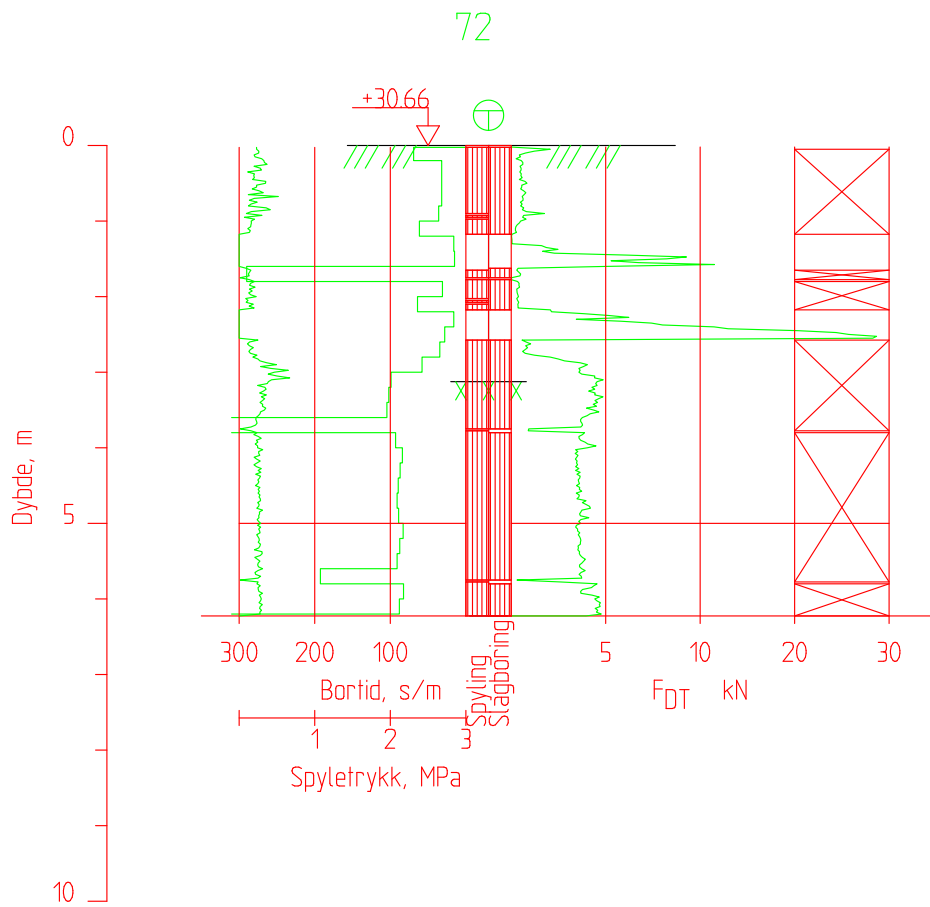
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E18 Langangen Rugtvedt

Borhull 5001TEC

Dato borete :02.07.2020

M = 1 : 200



Posisjon: X 1122724.57 Y 109798.17

Totalsondering

Borhull 72

Dato borete :16.11.2016

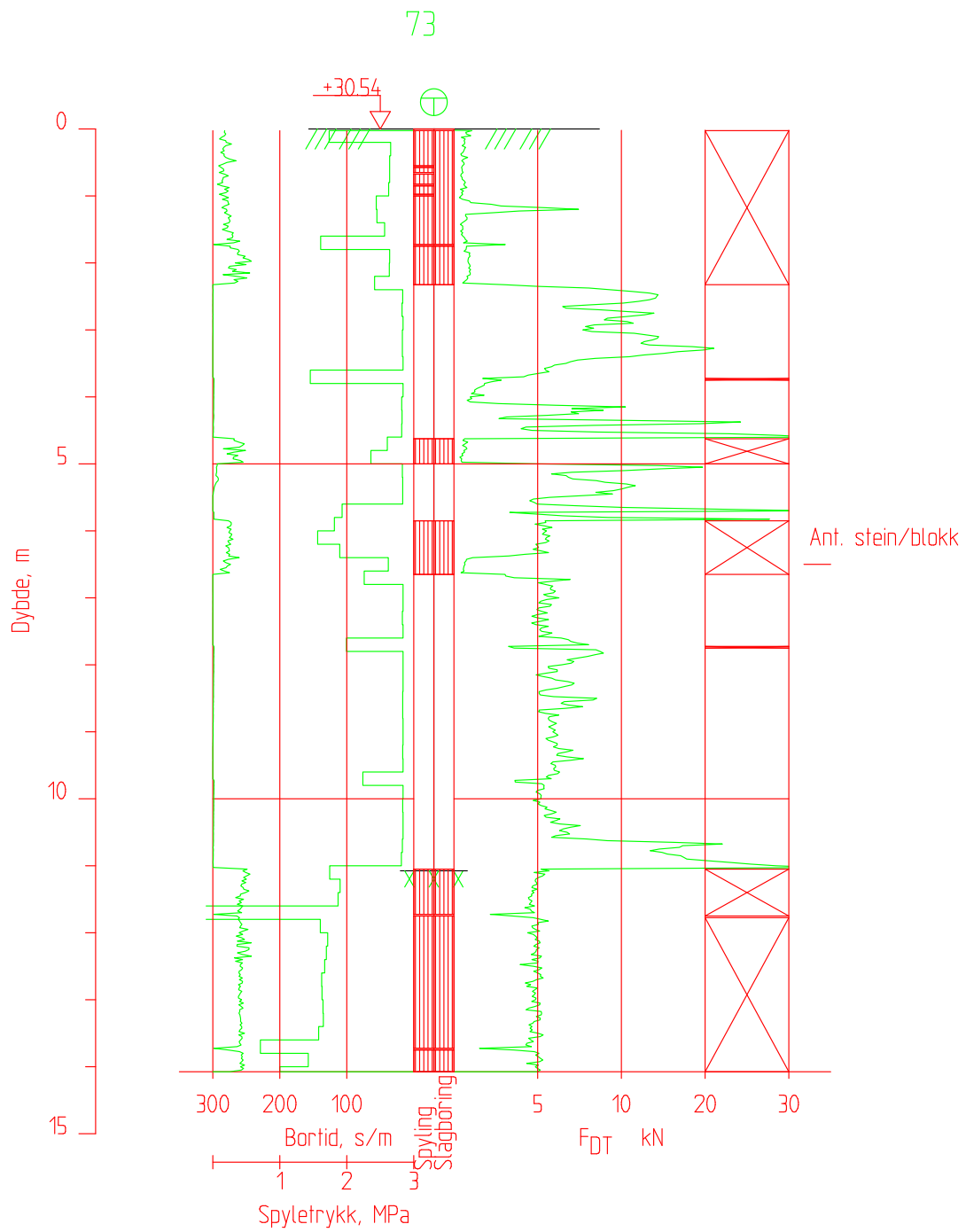
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122685.44 Y 109771.07

Totalsondering

Borhull 73

Dato boret :16.11.2016

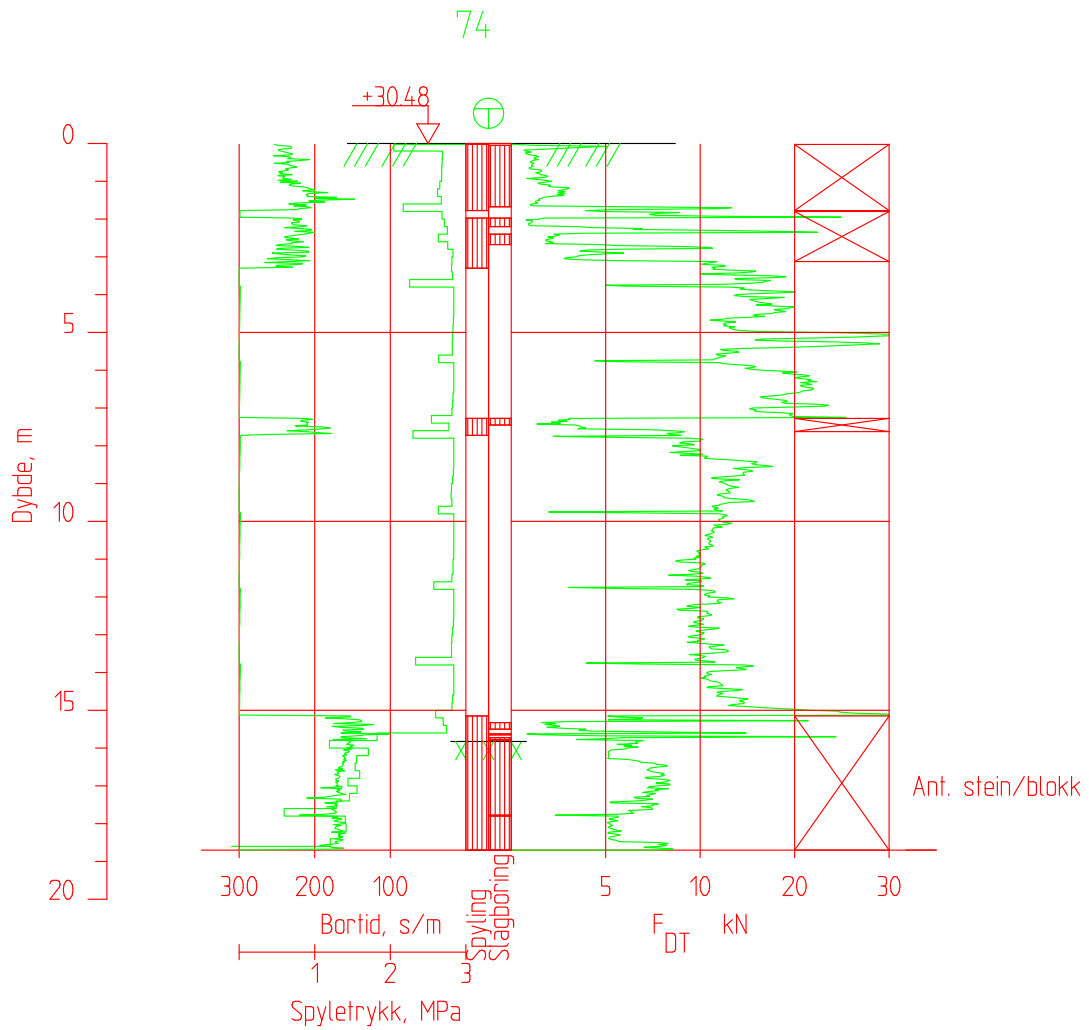
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122642.65 Y 109756.24

Totalsondering

Borhull 74

Dato boret :16.11.2016

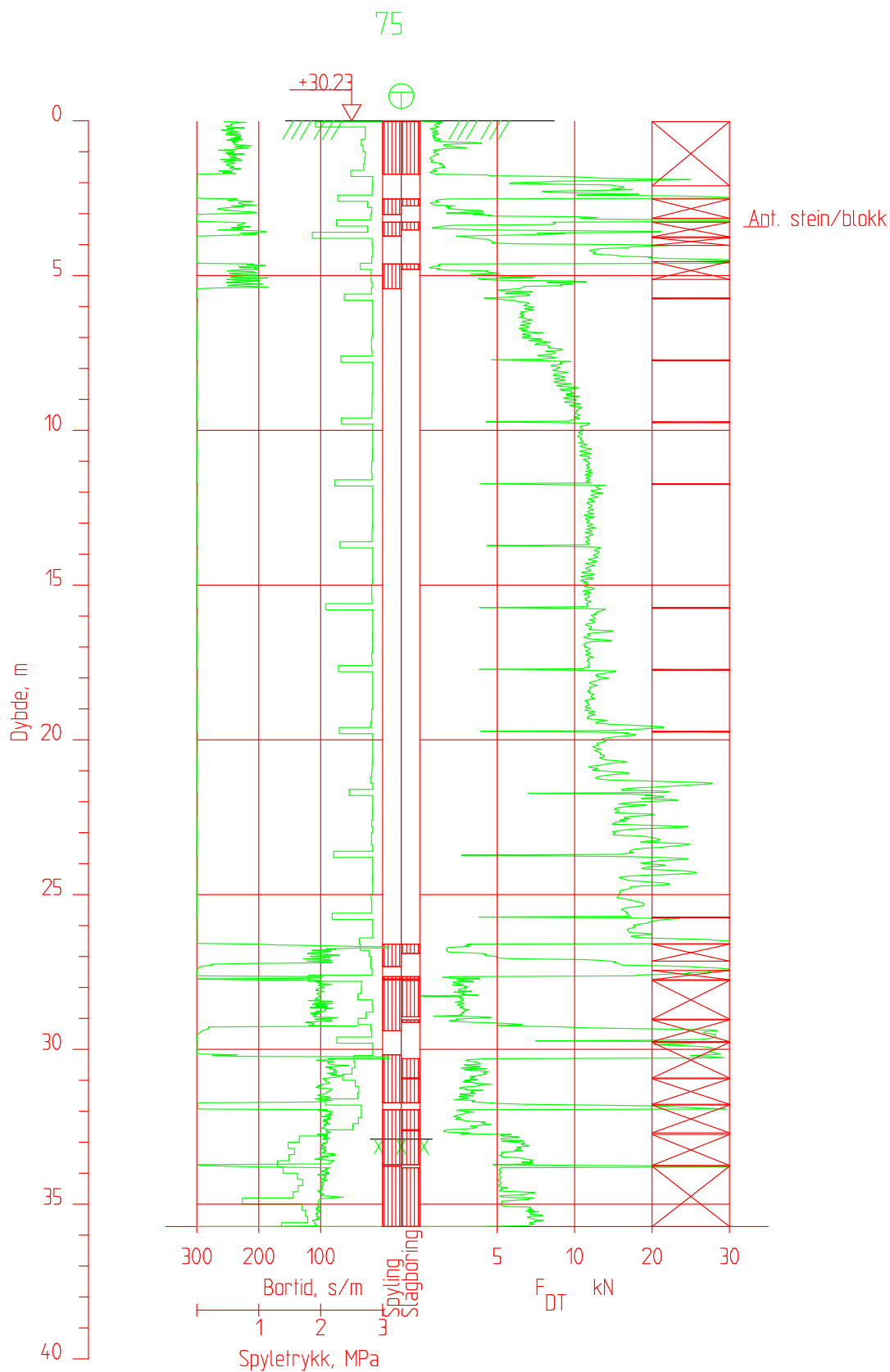
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122627.10 Y 109742.25

Totalsondering

Borhull 75

Dato boret :16.11.2016

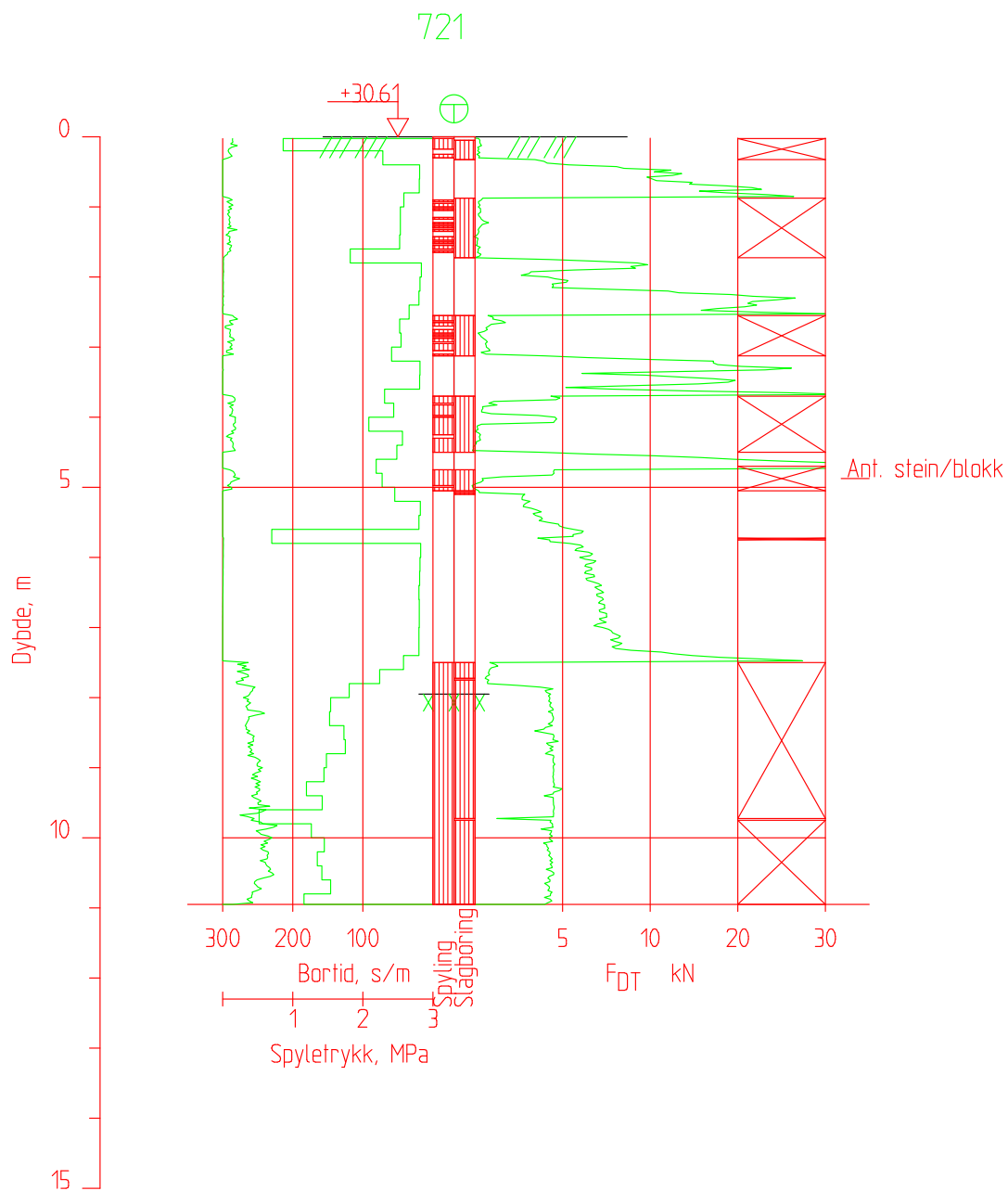
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E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122747.19 Y 109766.10

Totalsondering

Borhull 721

Dato boret :11.01.2017

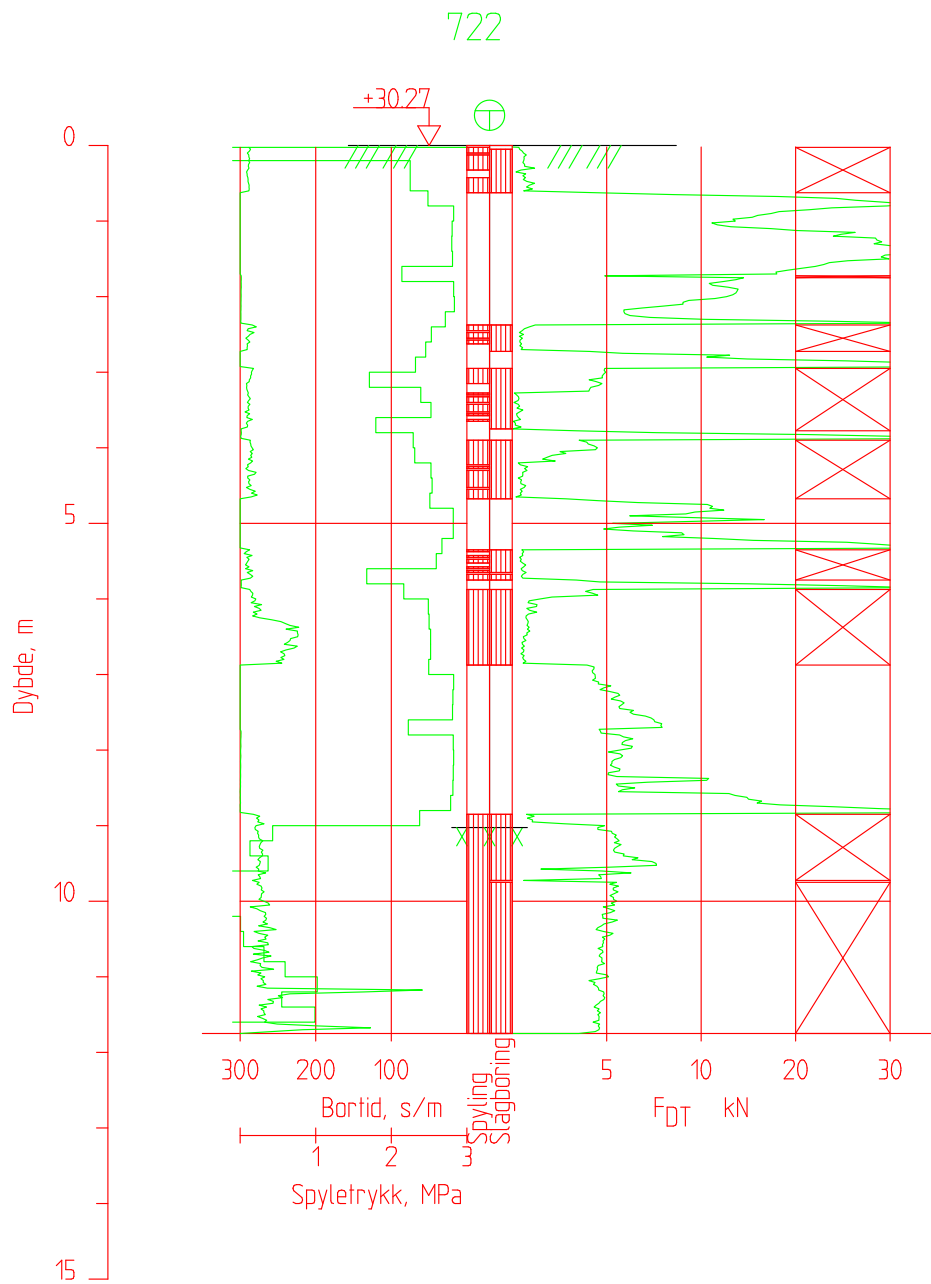
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122719.18 Y 109745.63

Totalsondering

Borhull 722

Dato boret :11.01.2017

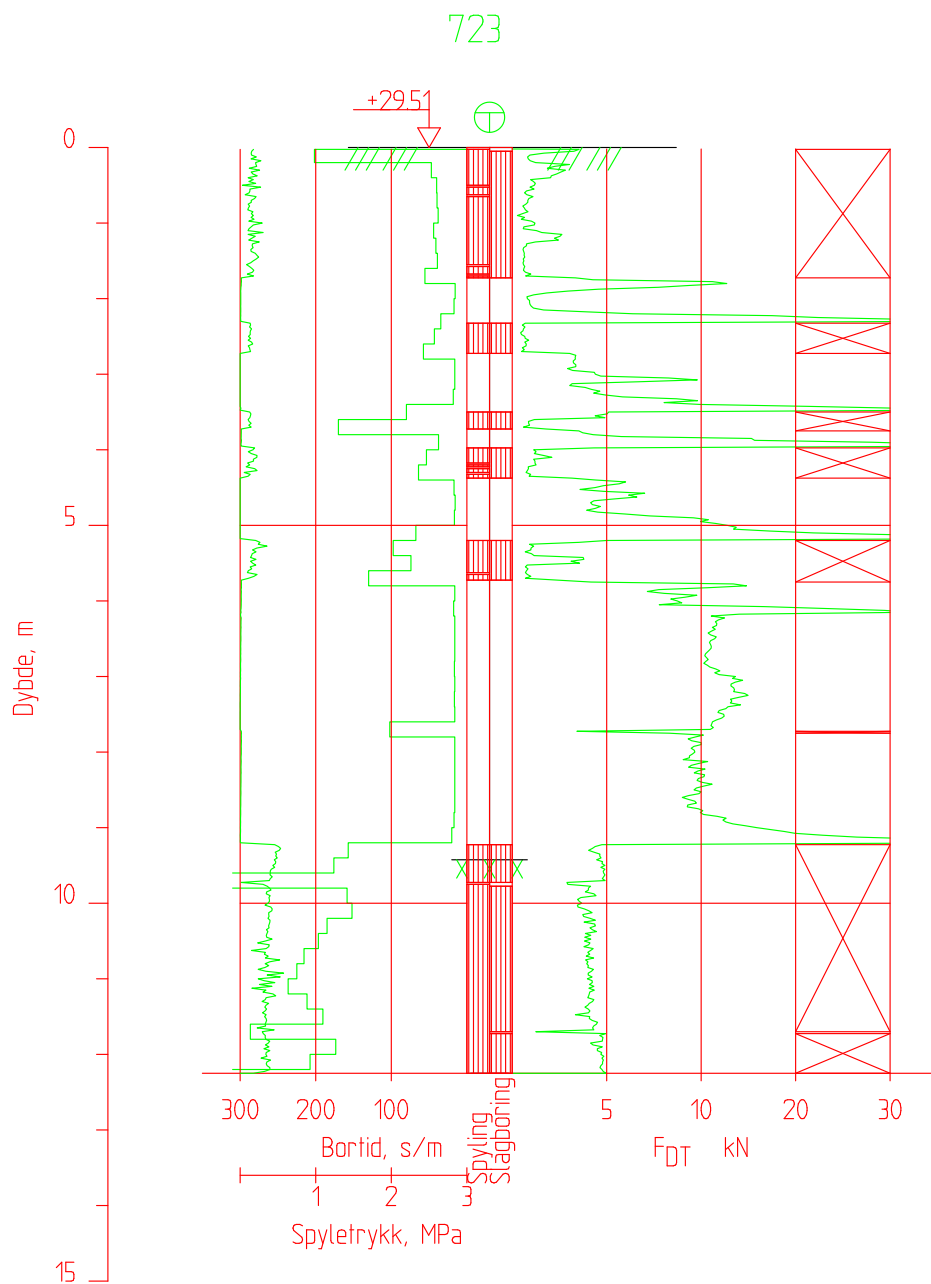
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122694.22 Y 109733.96

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

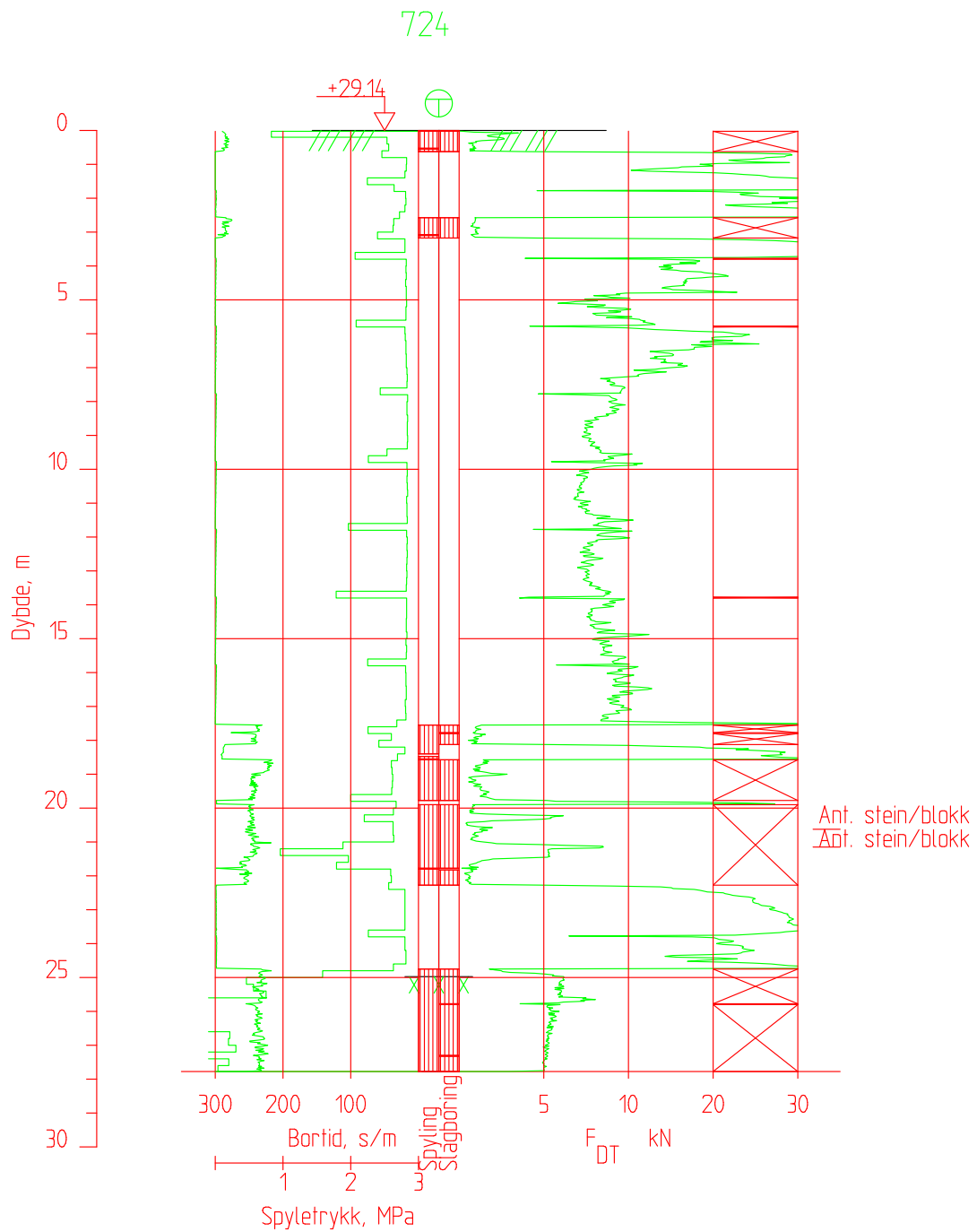
Borhull 723

Dato boret :11.01.2017

M = 1 : 100

BG

19756



Posisjon: X 1122664.86 Y 109718.22

Totalsondering

Borhull 724

Dato boret :10.01.2017

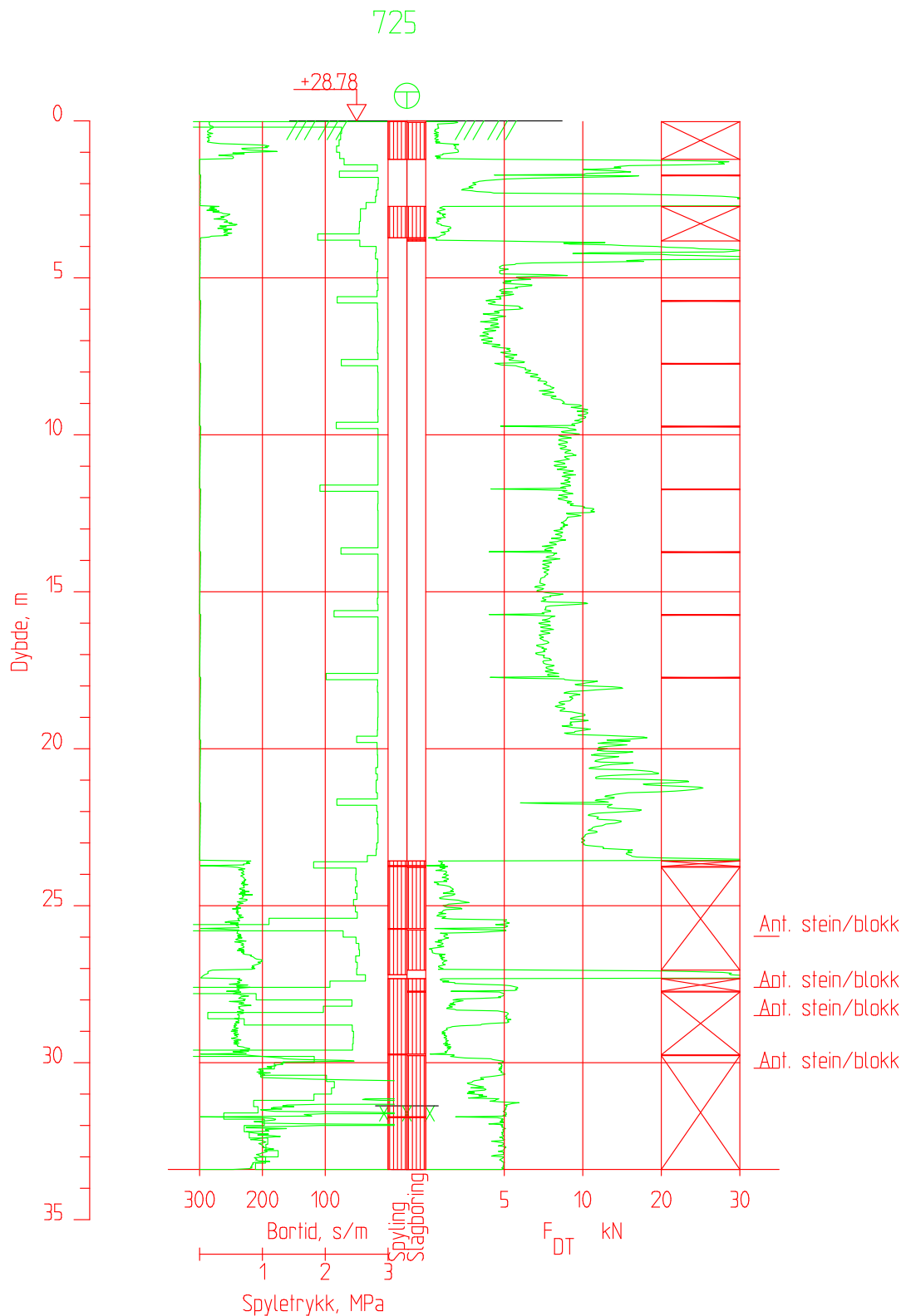
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E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122636.46 Y 109705.64

Totalsondering

Borhull 725

Dato boret :10.01.2017

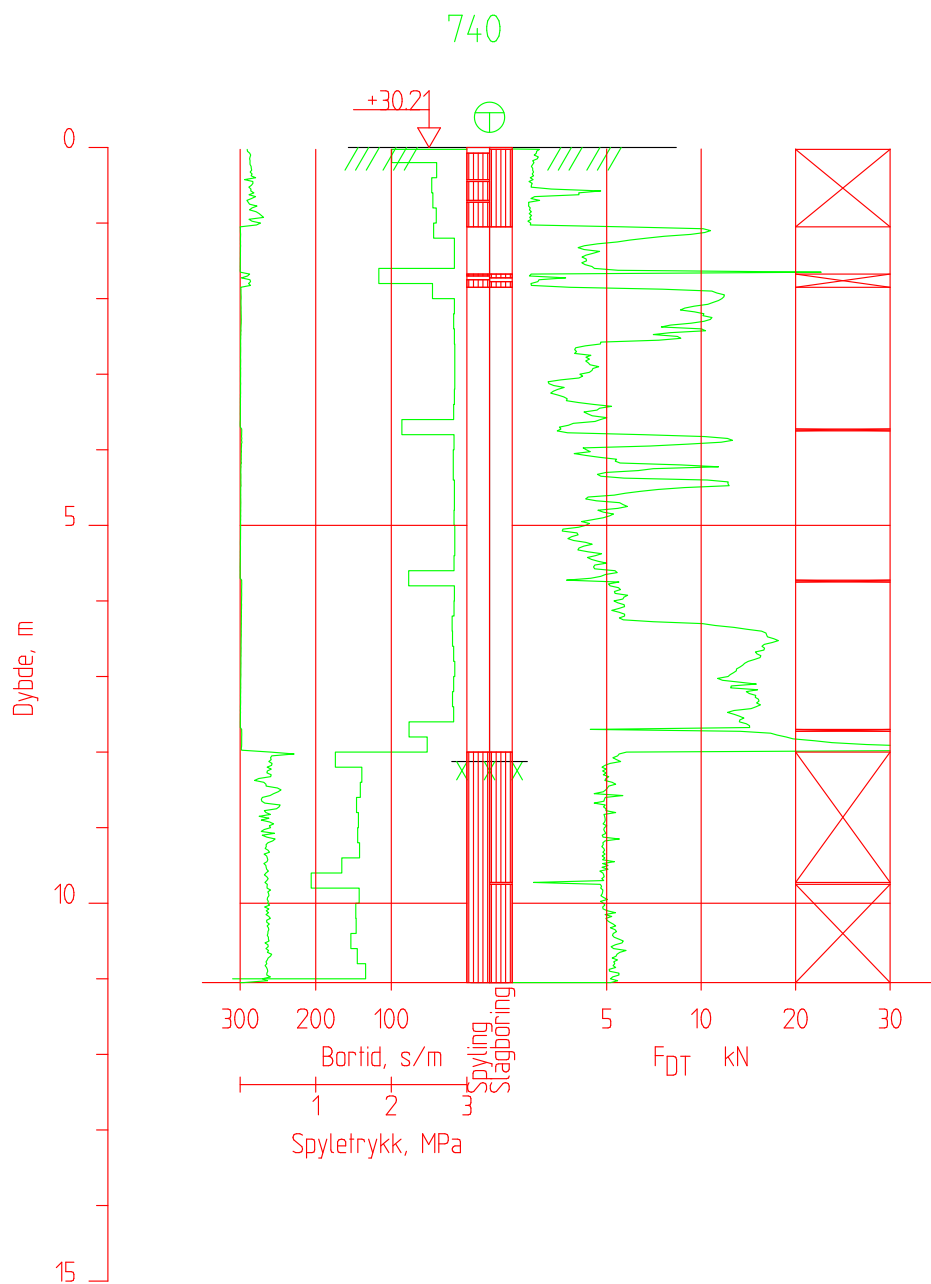
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122756.44 Y 109742.31

Totalsondering

Borhull 740

Dato boret :28.03.2017

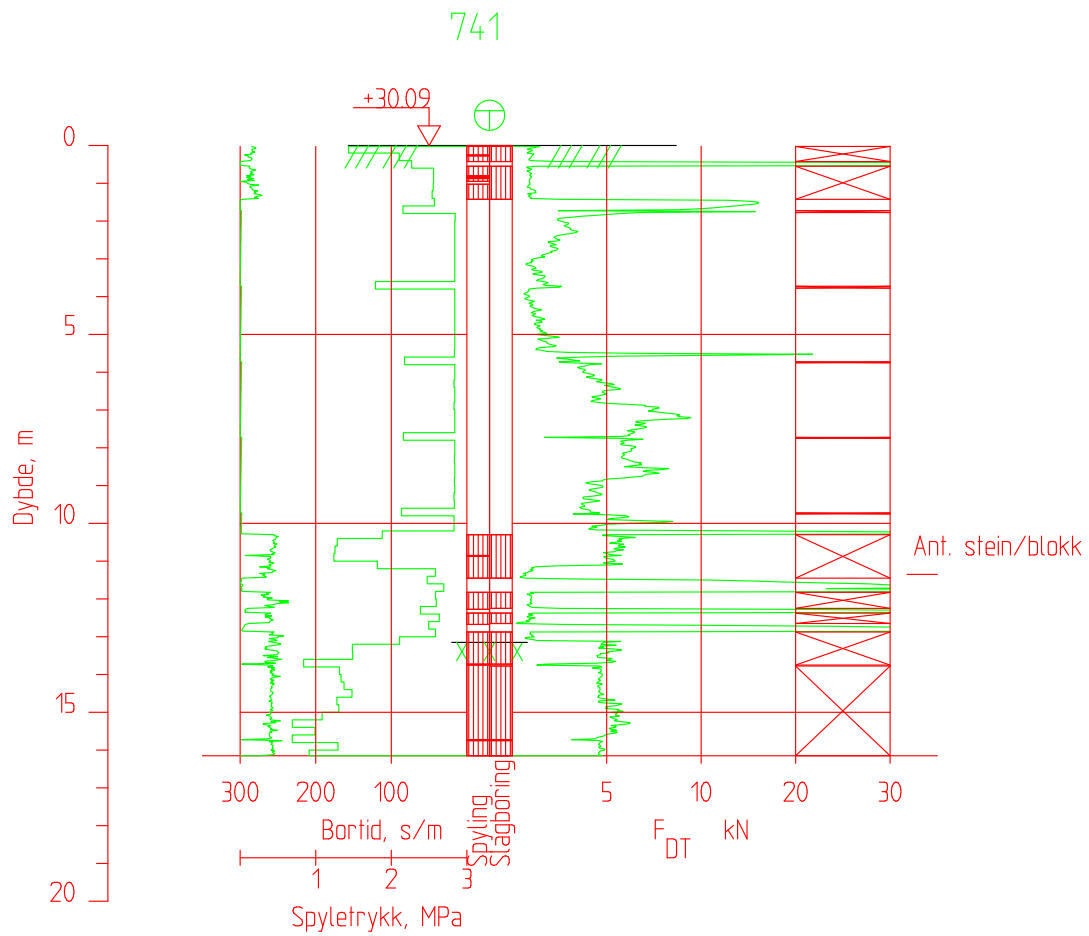
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122749.16 Y 109739.41

Totalsondering

Borhull 741

Dato boret :28.03.2017

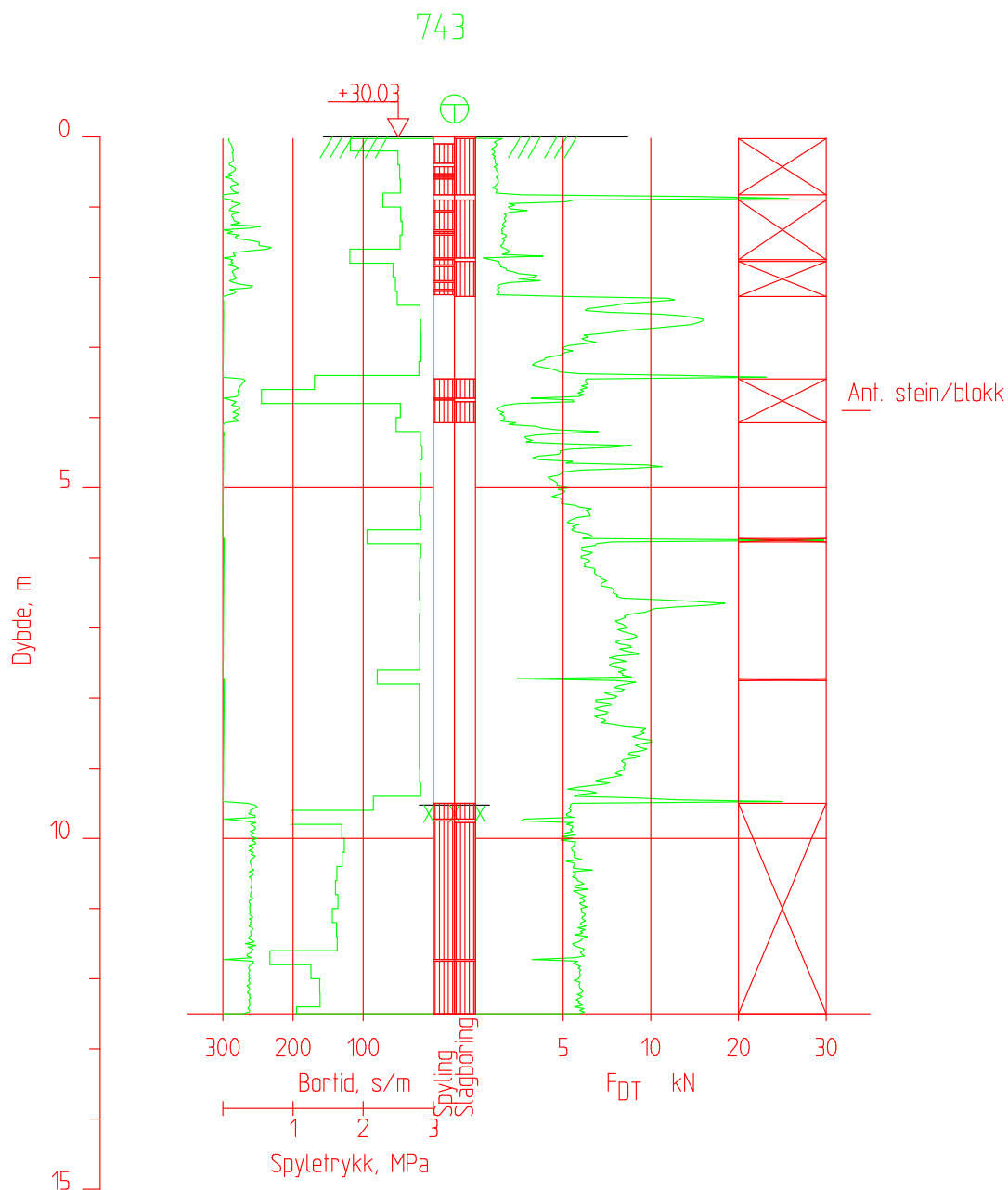
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122733.29 Y 109729.93

Totalsondering

Borhull 743

Dato boret :28.03.2017

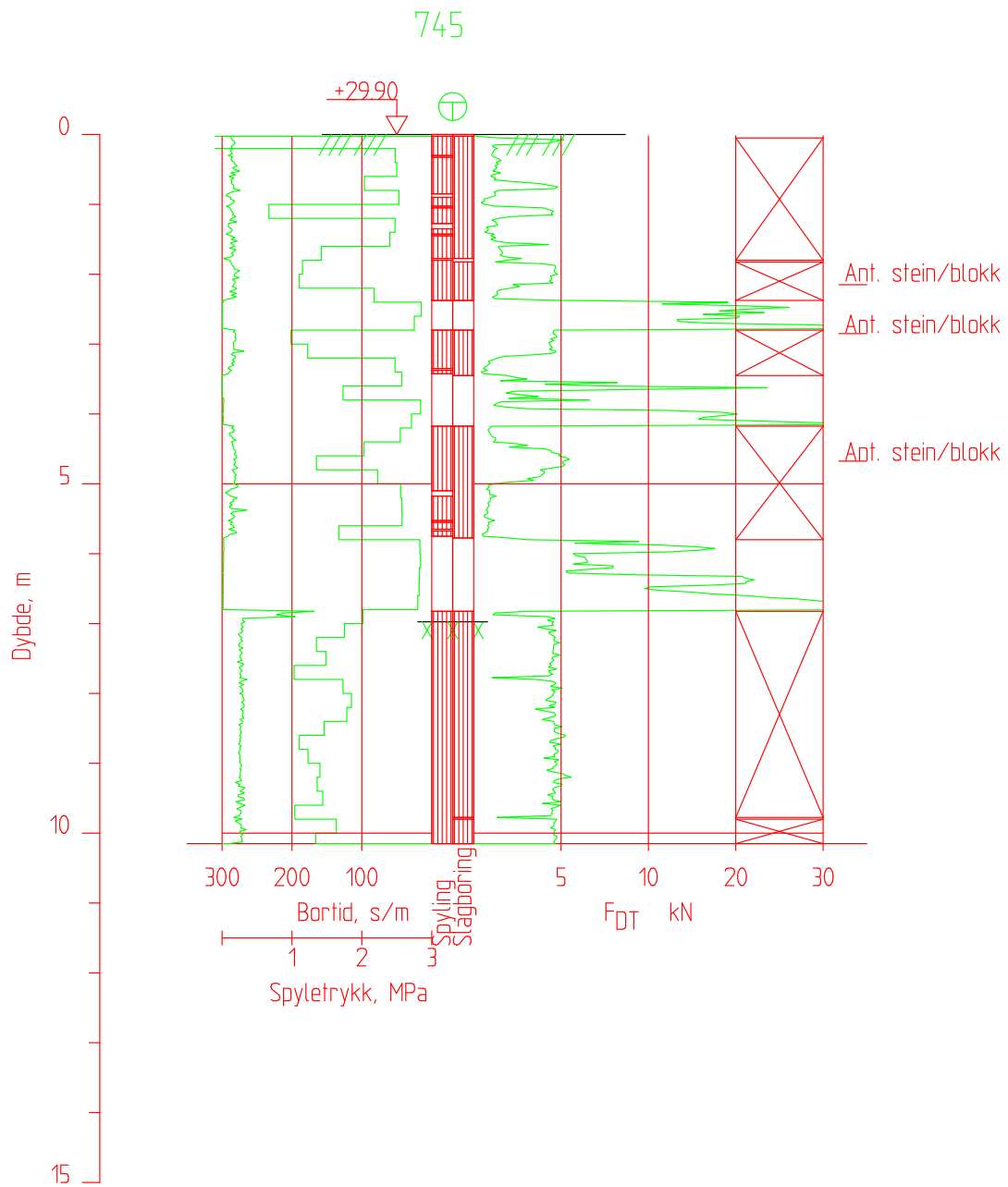
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122711.86 Y 109719.82

Totalsondering

Borhull 745

Dato boret :28.03.2017

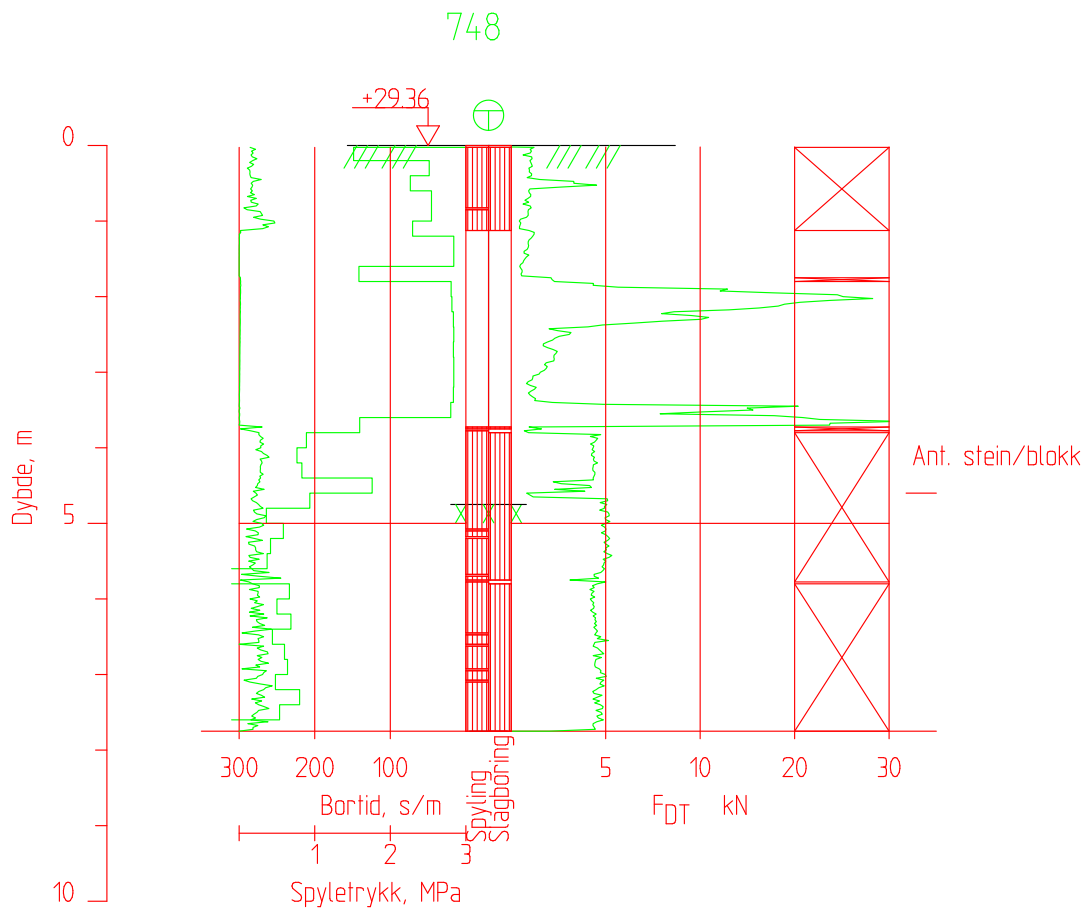
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E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122687.18 Y 109705.74

Totalsondering

EIFFAGE

E18 Langangen Røgtvedt

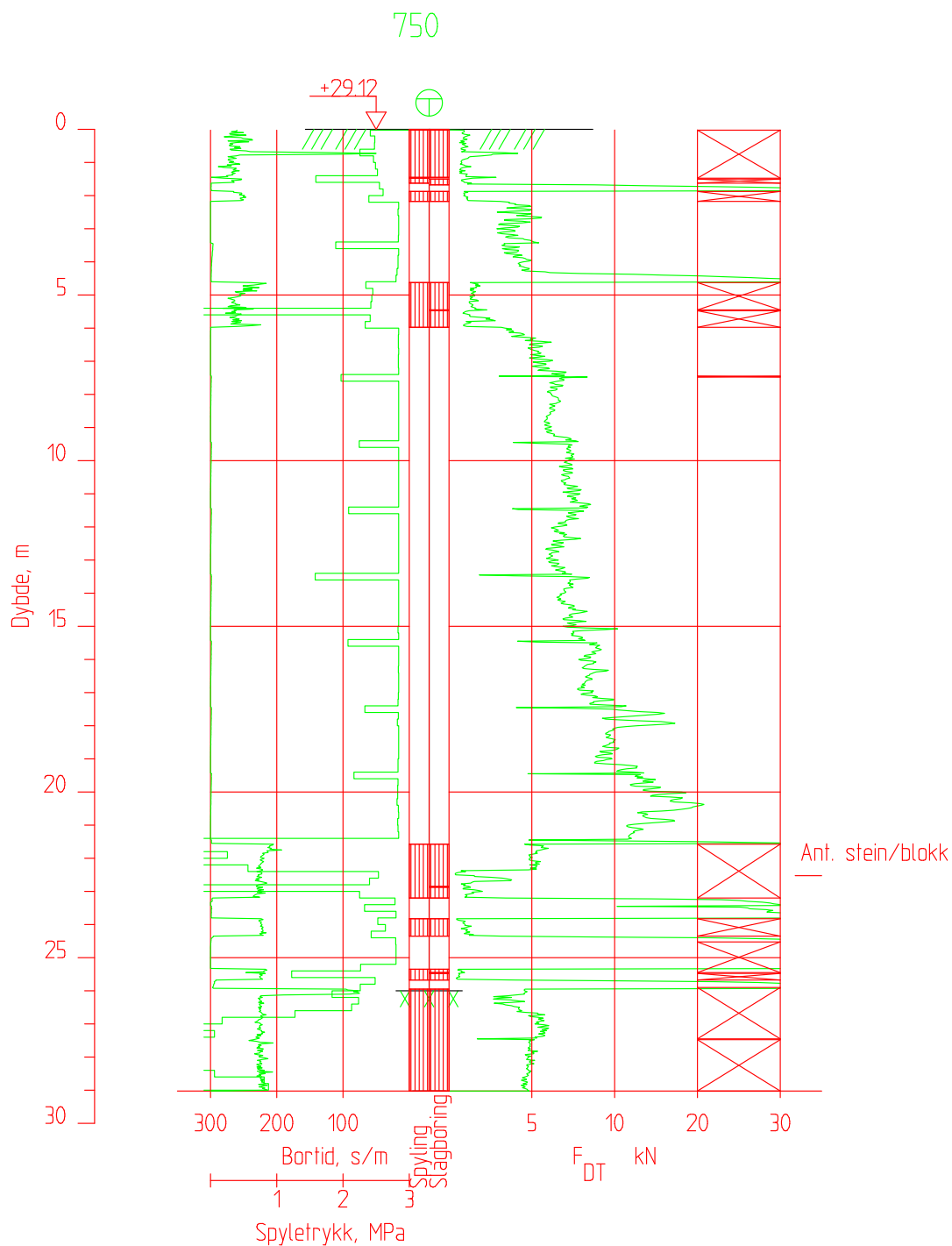
Borhull 748

Dato boreal :28.03.2017

M = 1 : 100

BG

19756



Posisjon: X 1122671.54 Y 109697.00

Totalsondering

Borhull 750

Dato boret :21.03.2017

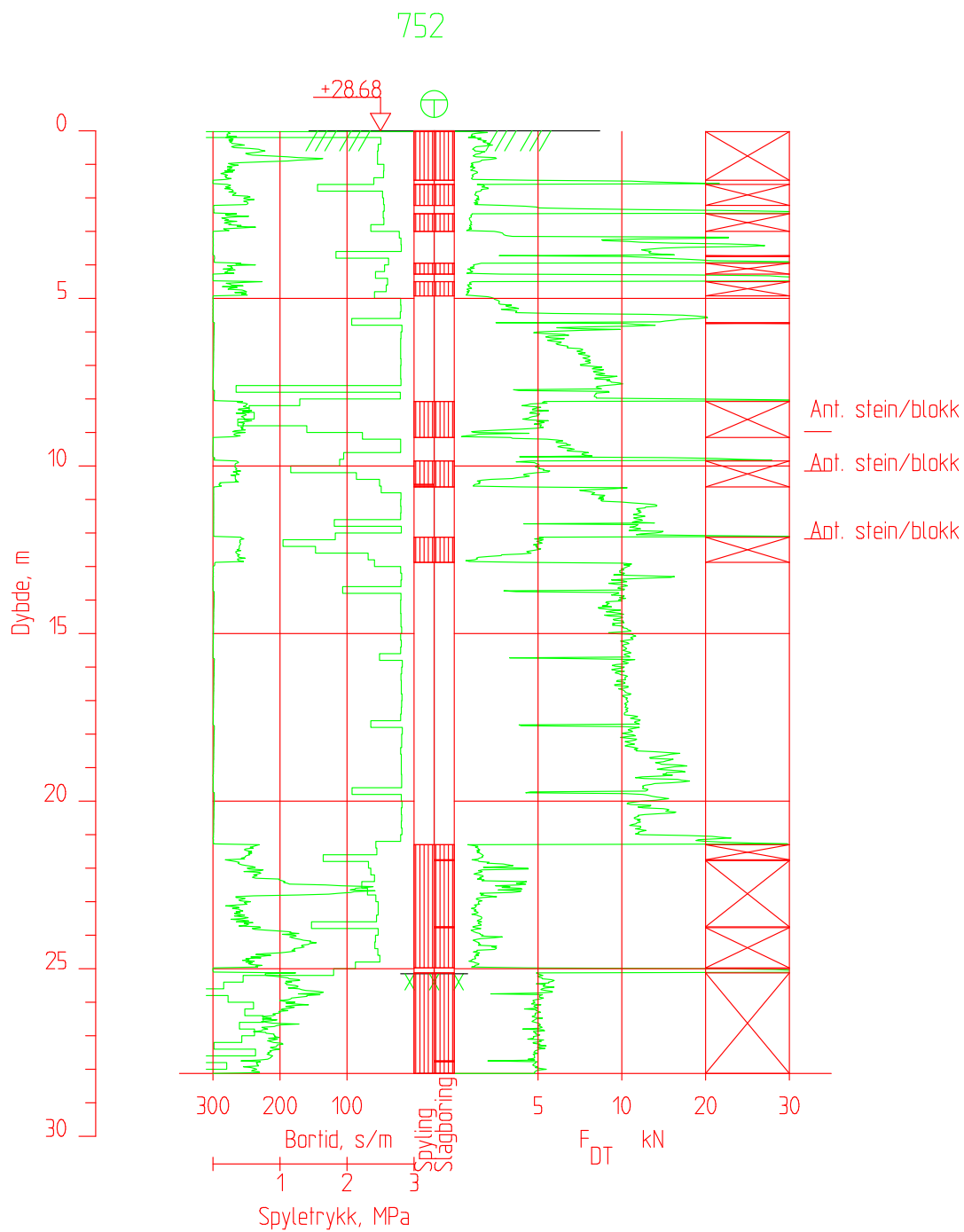
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122632.62 Y 109677.92

Totalsondering

Borhull 752

Dato boret :28.03.2017

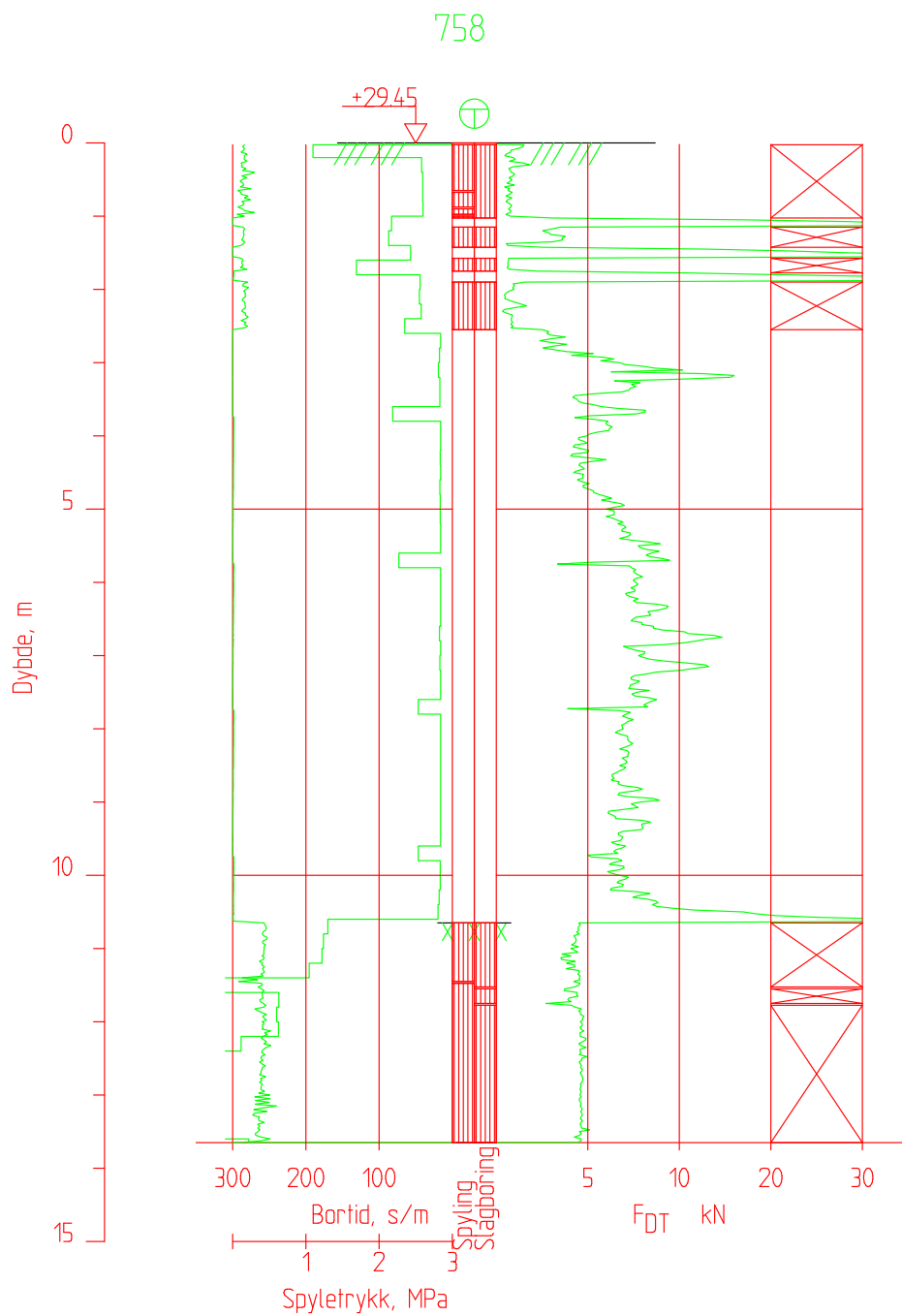
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122687.65 Y 109743.03

Totalsondering

Borhull 758

Dato boret :21.03.2017

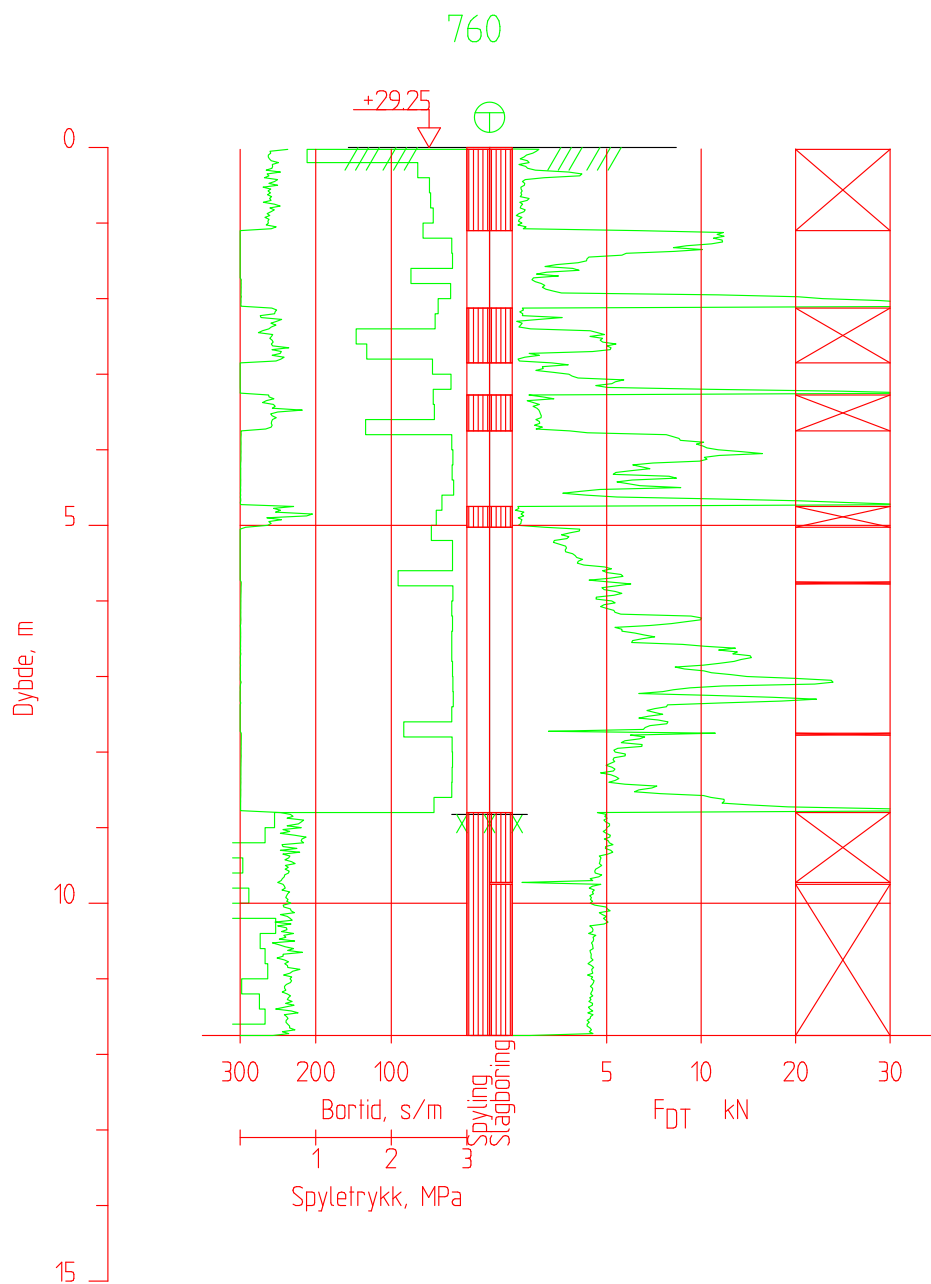
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122675.11 Y 109735.77

Totalsondering

Borhull 760

Dato borete :21.03.2017

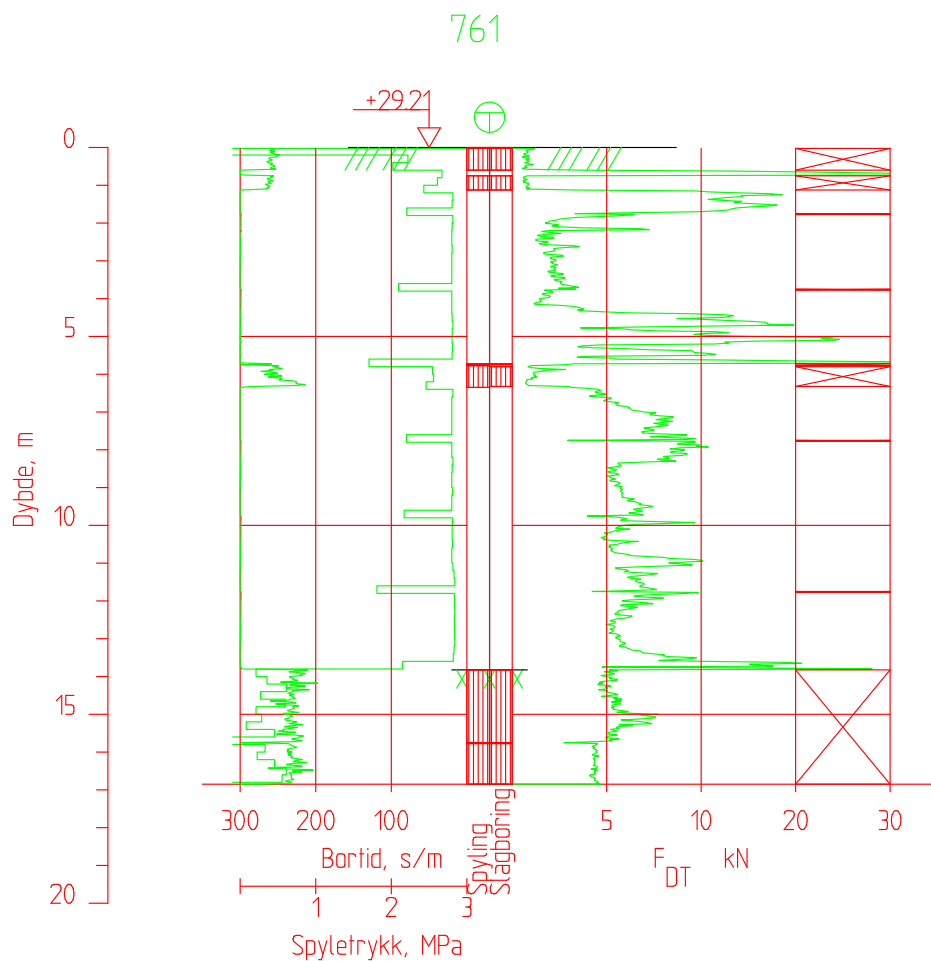
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122668.54 Y 109731.77

Totalsondering

Borhull 761

Dato borete :21.03.2017

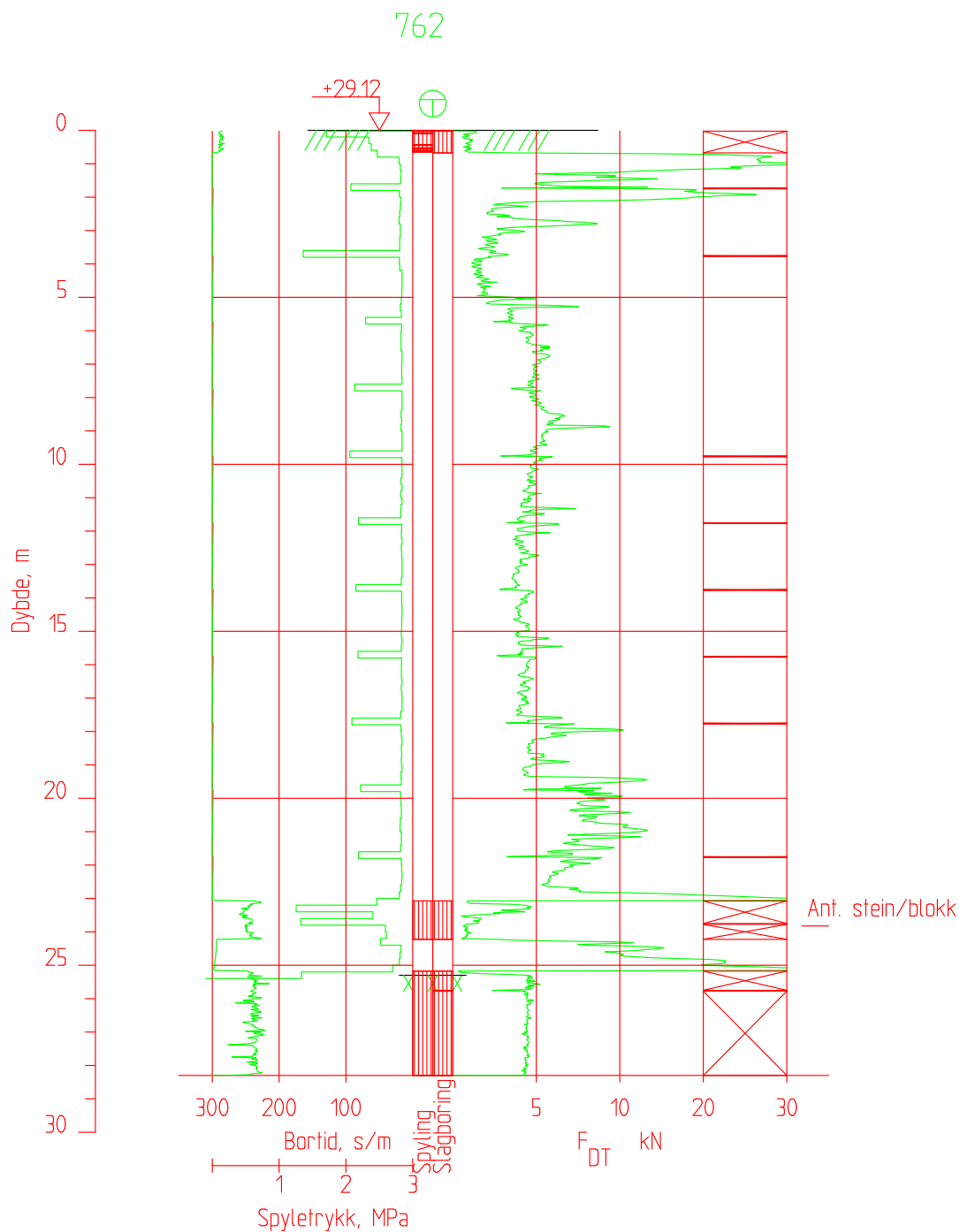
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122661.96 Y 109727.98

Totalsondering

Borhull 762

Dato boret :20.03.2017

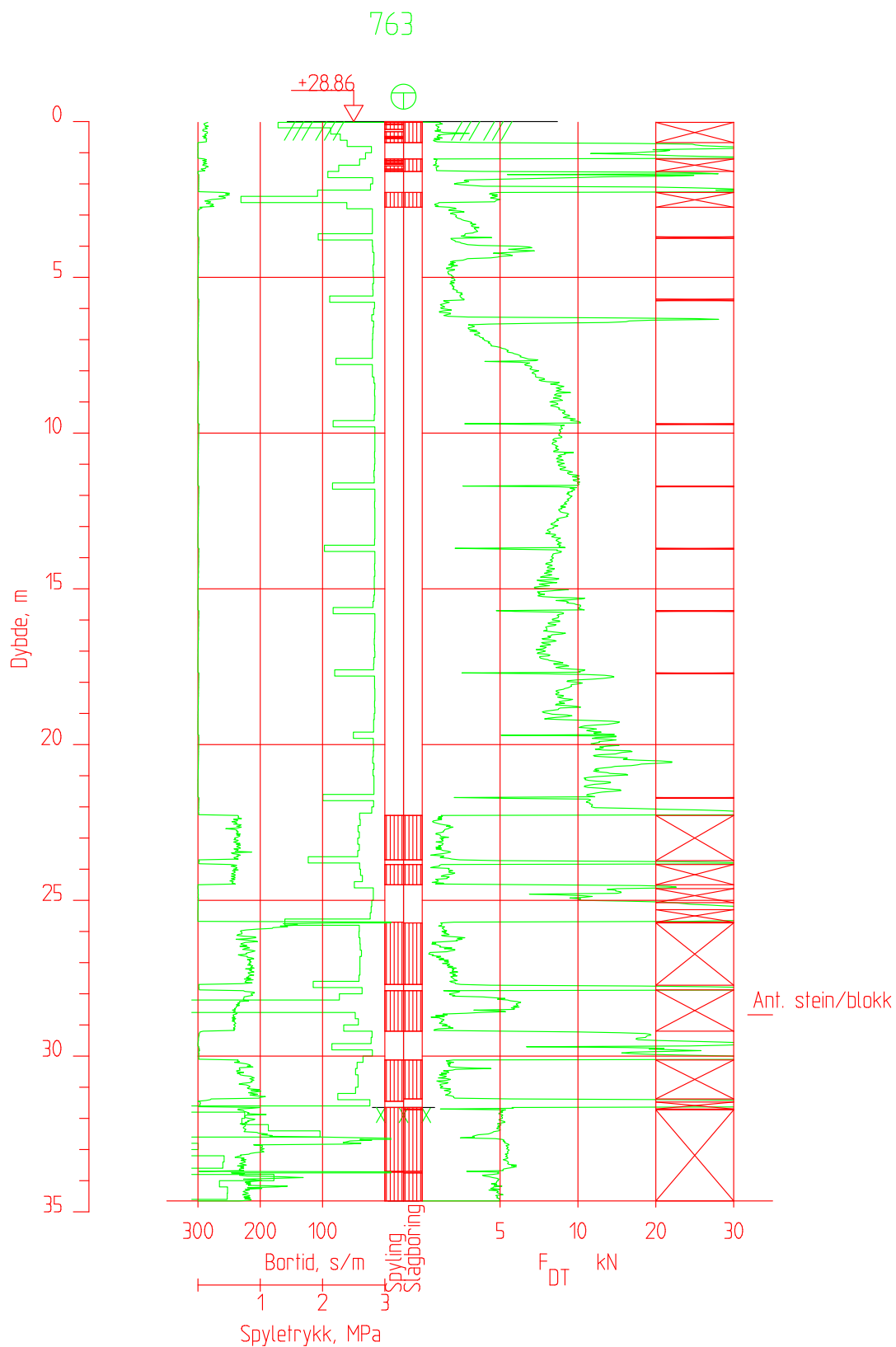
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122642.40 Y 109716.52

Totalsondering

Borhull 763

Dato boret :20.03.2017

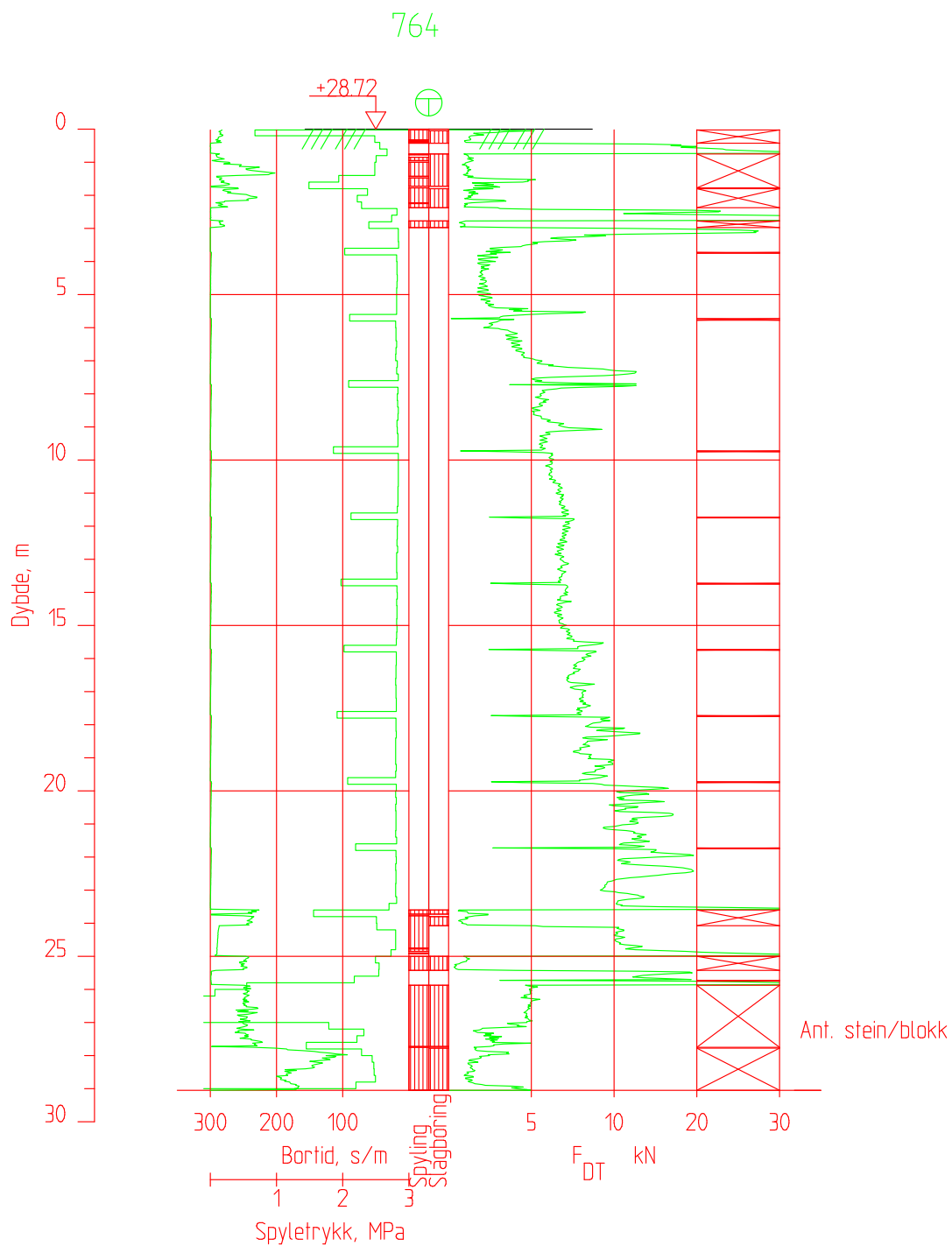
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122628.73 Y 109708.58

Totalsondering

Borhull 764

Dato boret :20.03.2017

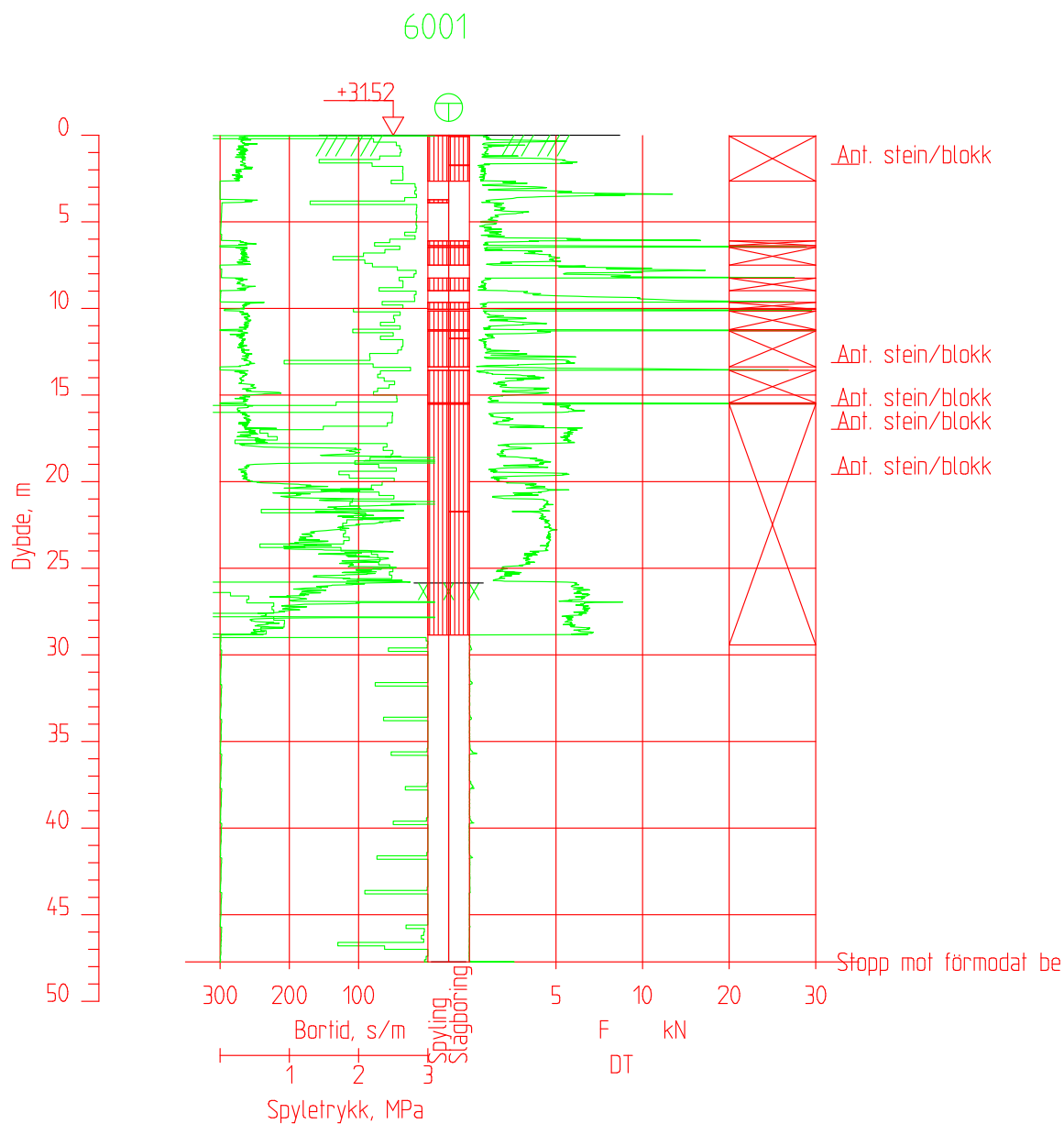
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122581.86 Y 109828.29

Totalsondering

Borhull 6001

Dato boret :10.04.2019

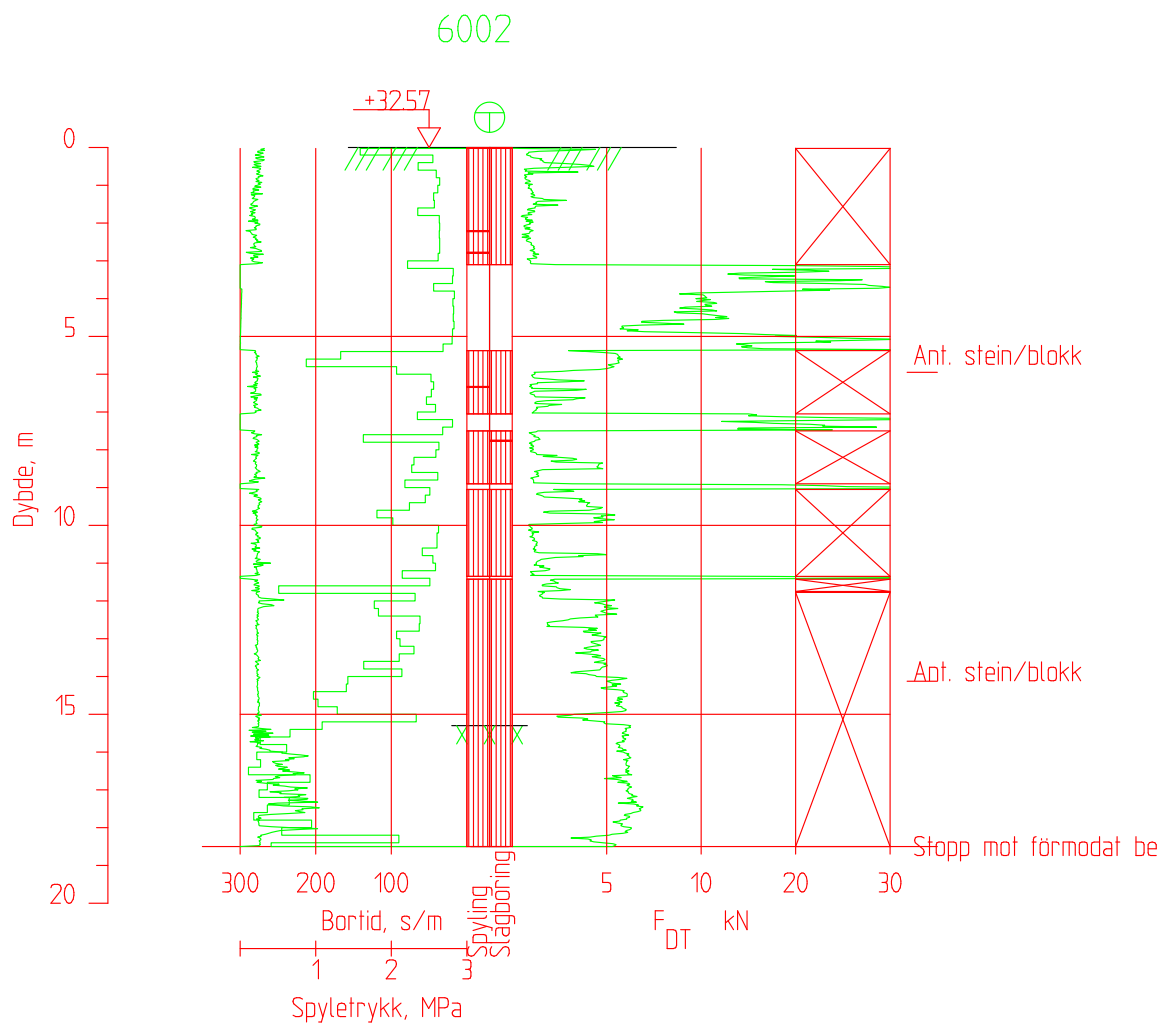
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E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122584.47 Y 109867.49

Totalsondering

Borhull 6002

Dato boret :09.04.2019

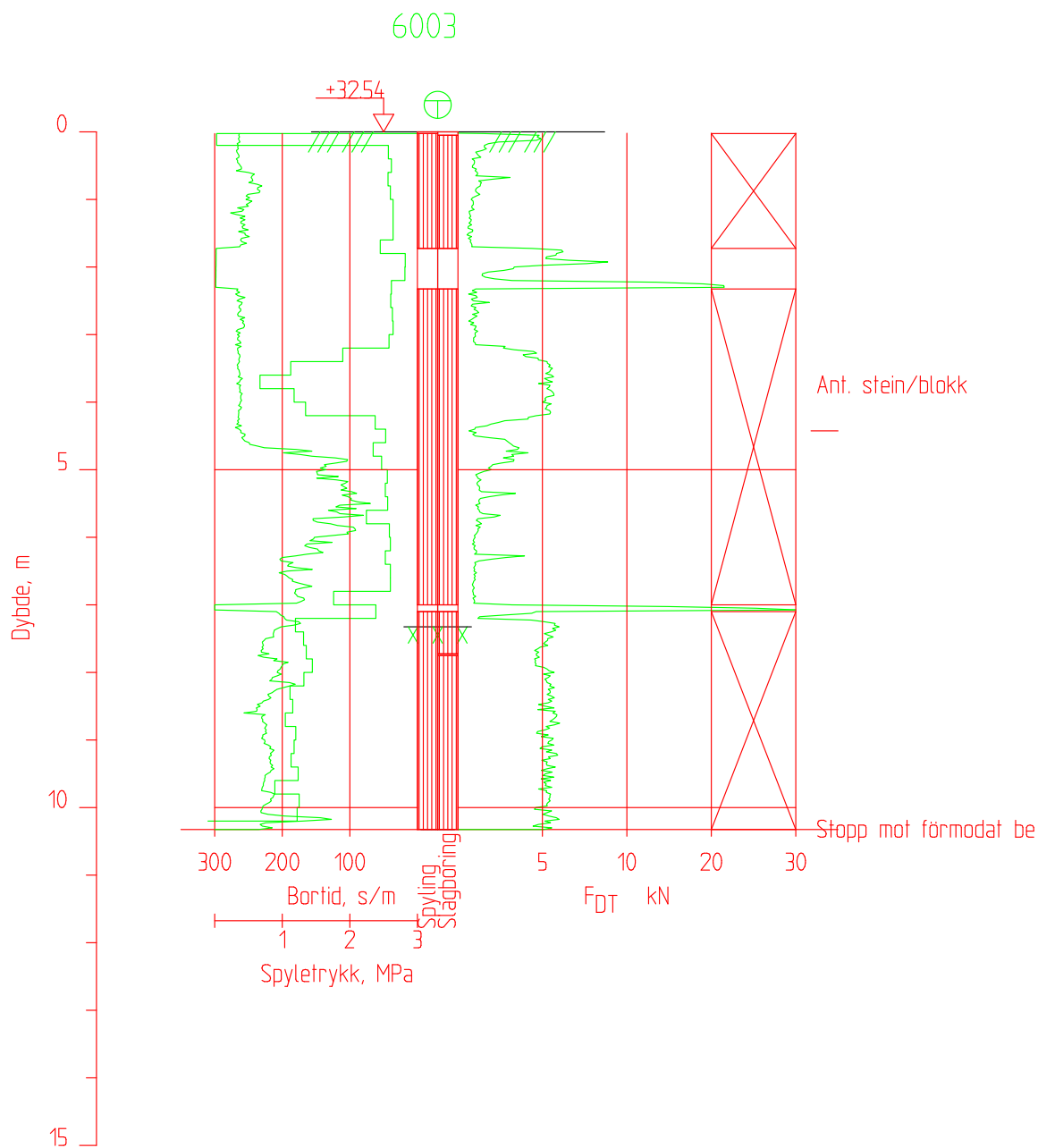
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122606.74 Y 109892.81

Totalsondering

Borhull 6003

Dato boret :08.04.2019

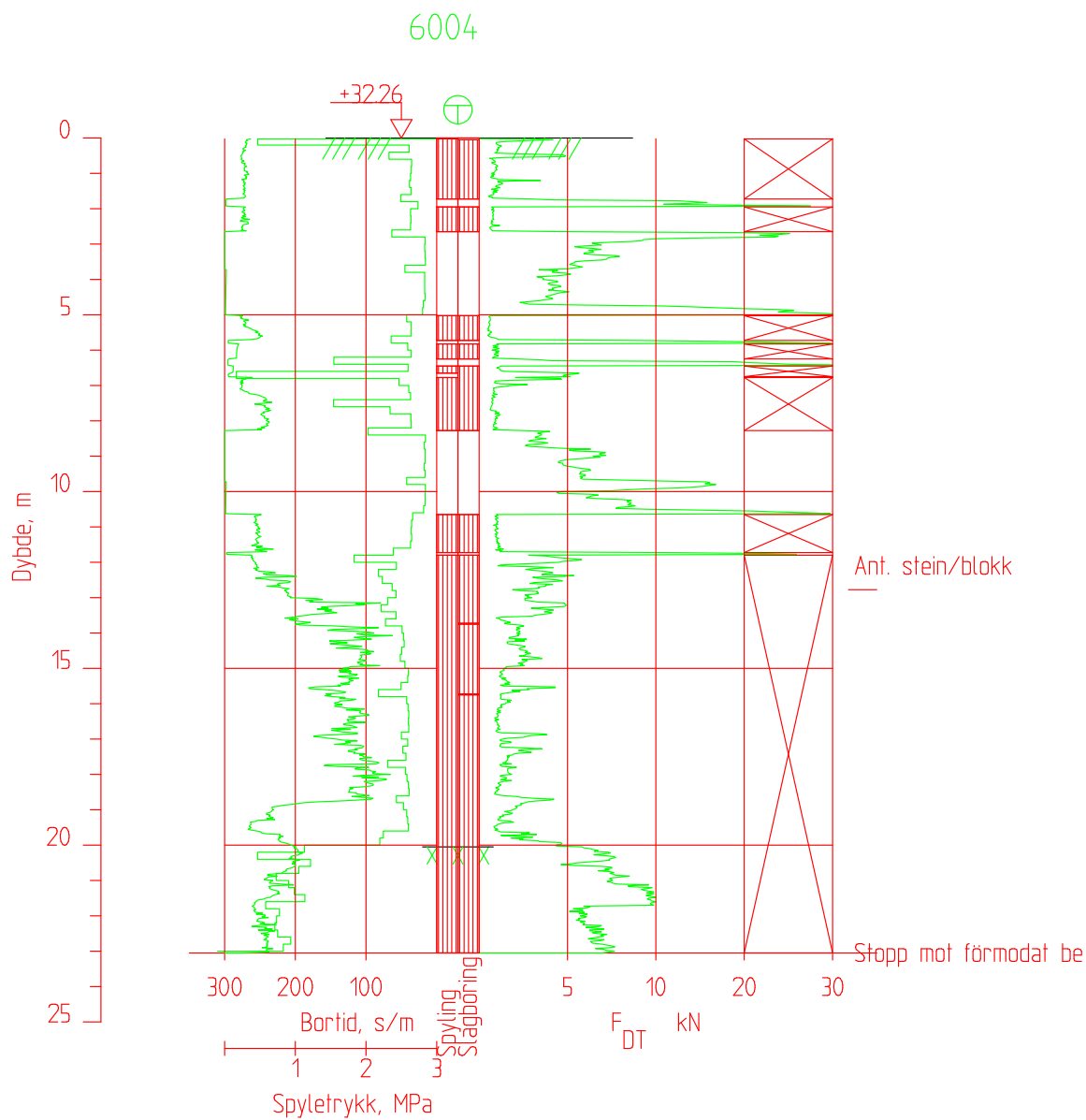
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122617.06 Y 109869.46

Totalsondering

Borhull 6004

Dato boret :08.04.2019

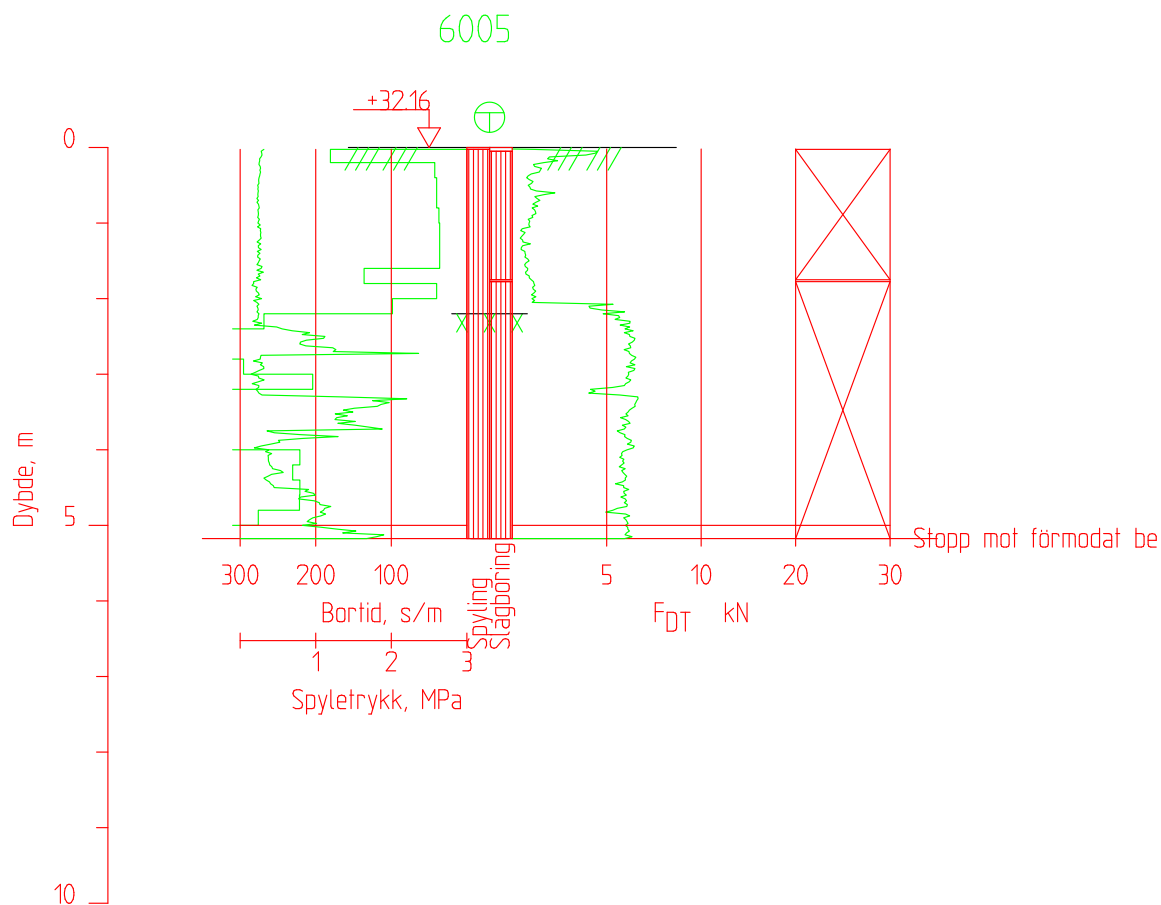
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122633.21 Y 109888.32

Totalsondering

Borhull 6005

Dato boret :08.04.2019

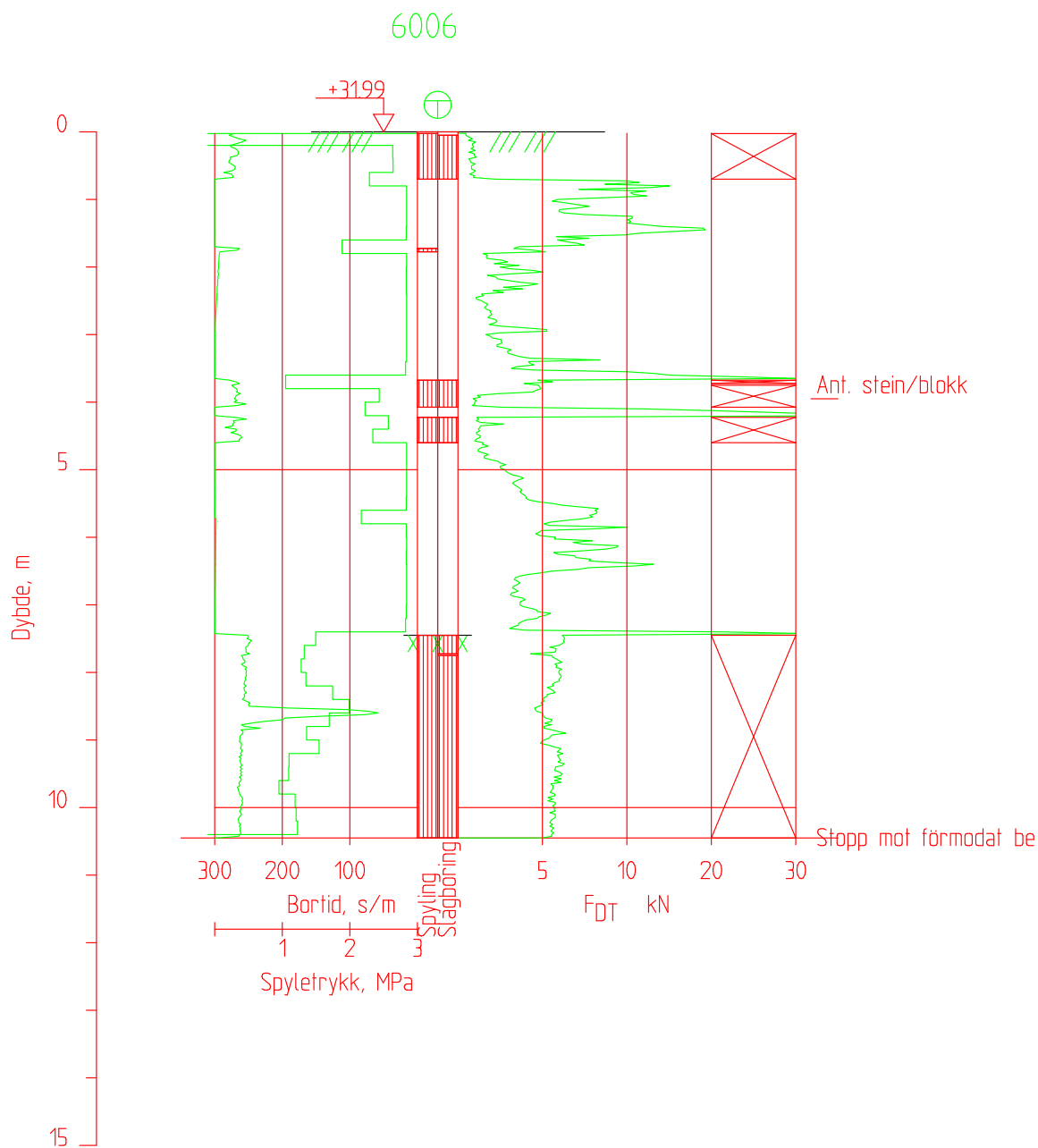
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122646.86 Y 109895.78

Totalsondering

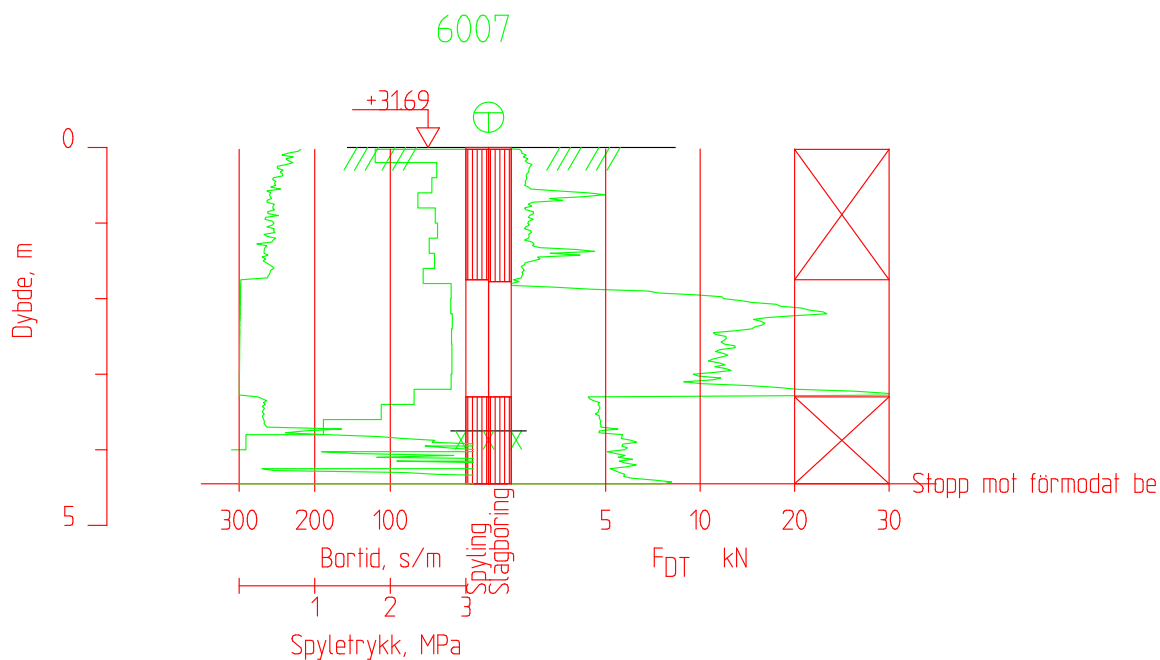
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E18 Langangen Rugtvedt

Borhull 6006

Dato boret :08.04.2019

M = 1 : 100



Posisjon: X 1122655.73 Y 109904.85

Totalsondering

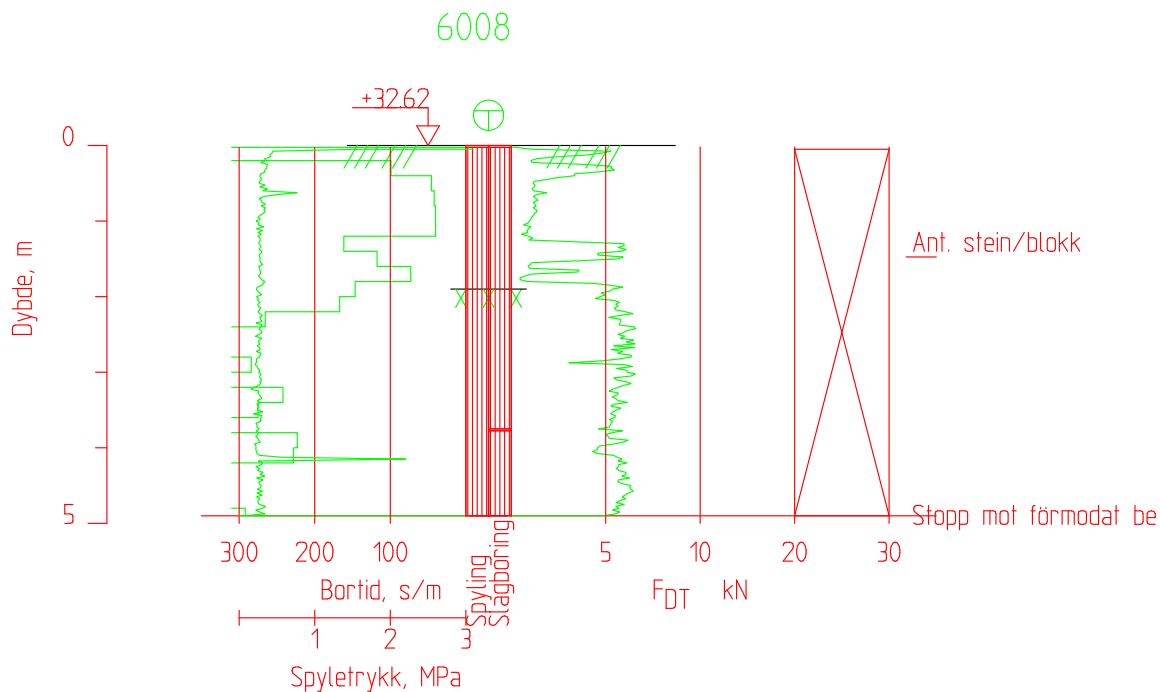
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E18 Langangen Rugtvedt

Borhull 6007

Dato boret :09.04.2019

M = 1 : 100



Posisjon: X 1122628.36 Y 109916.18

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

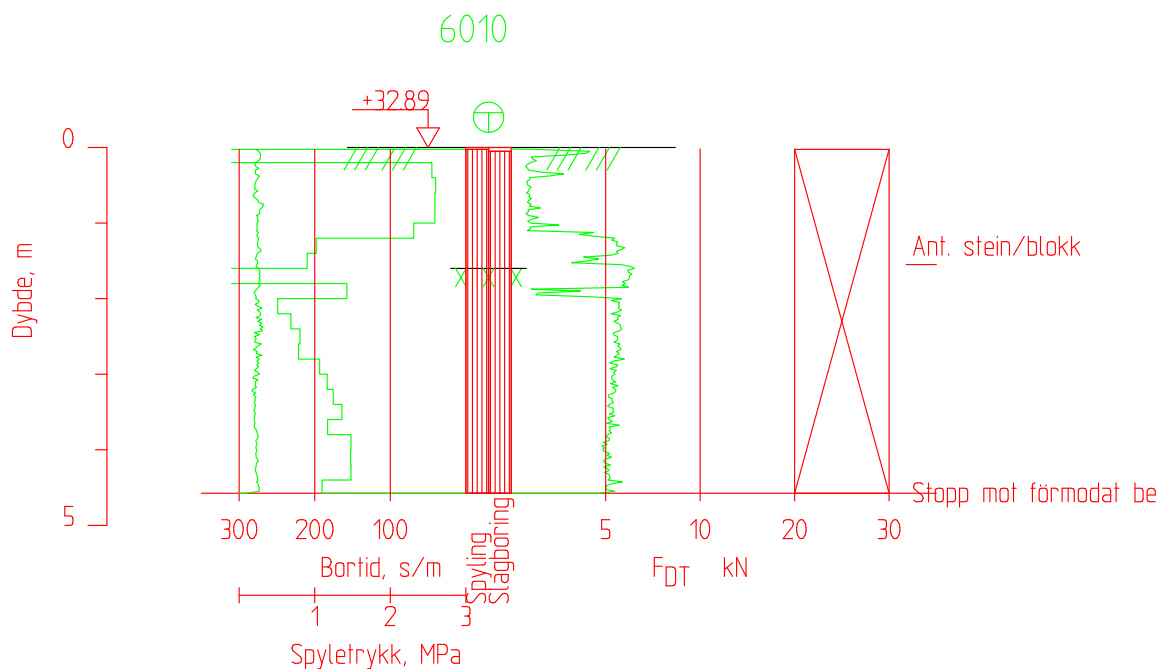
Borhull 6008

Dato boret :09.04.2019

M = 1 : 100

BG

19756



Posisjon: X 1122611.23 Y 109947.95

Totalsondering

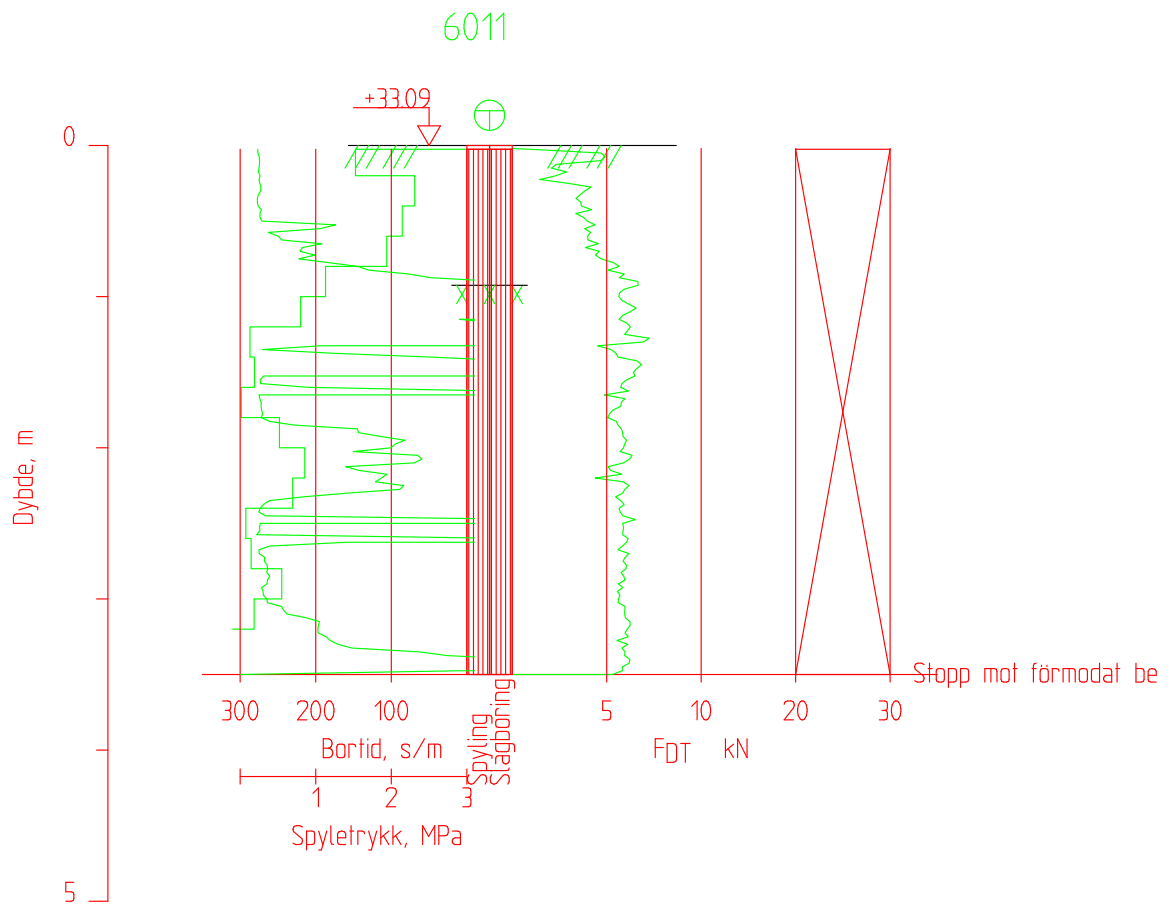
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E18 Langangen Rugtvedt

Borhull 6010

Dato boret :09.04.2019

M = 1 : 100



Posisjon: X 1122597.18 Y 109964.58

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

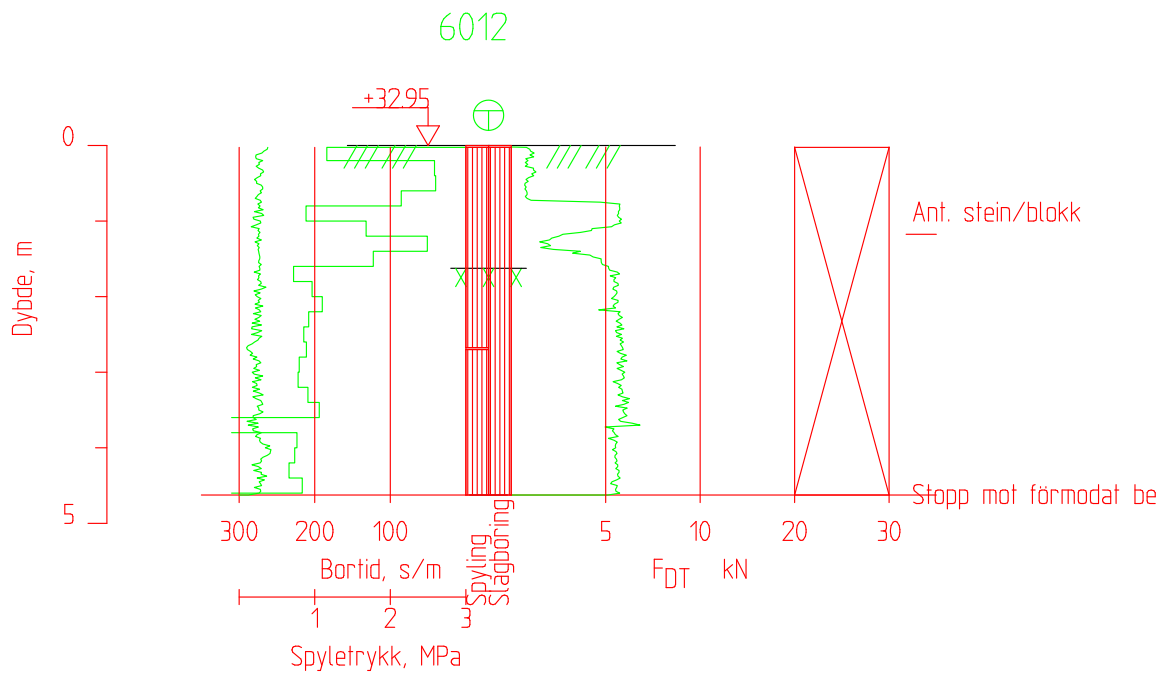
Borhull 6011

Dato boret :09.04.2019

M = 1 : 50

BG

19756



Posisjon: X 1122565.60 Y 109960.37

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

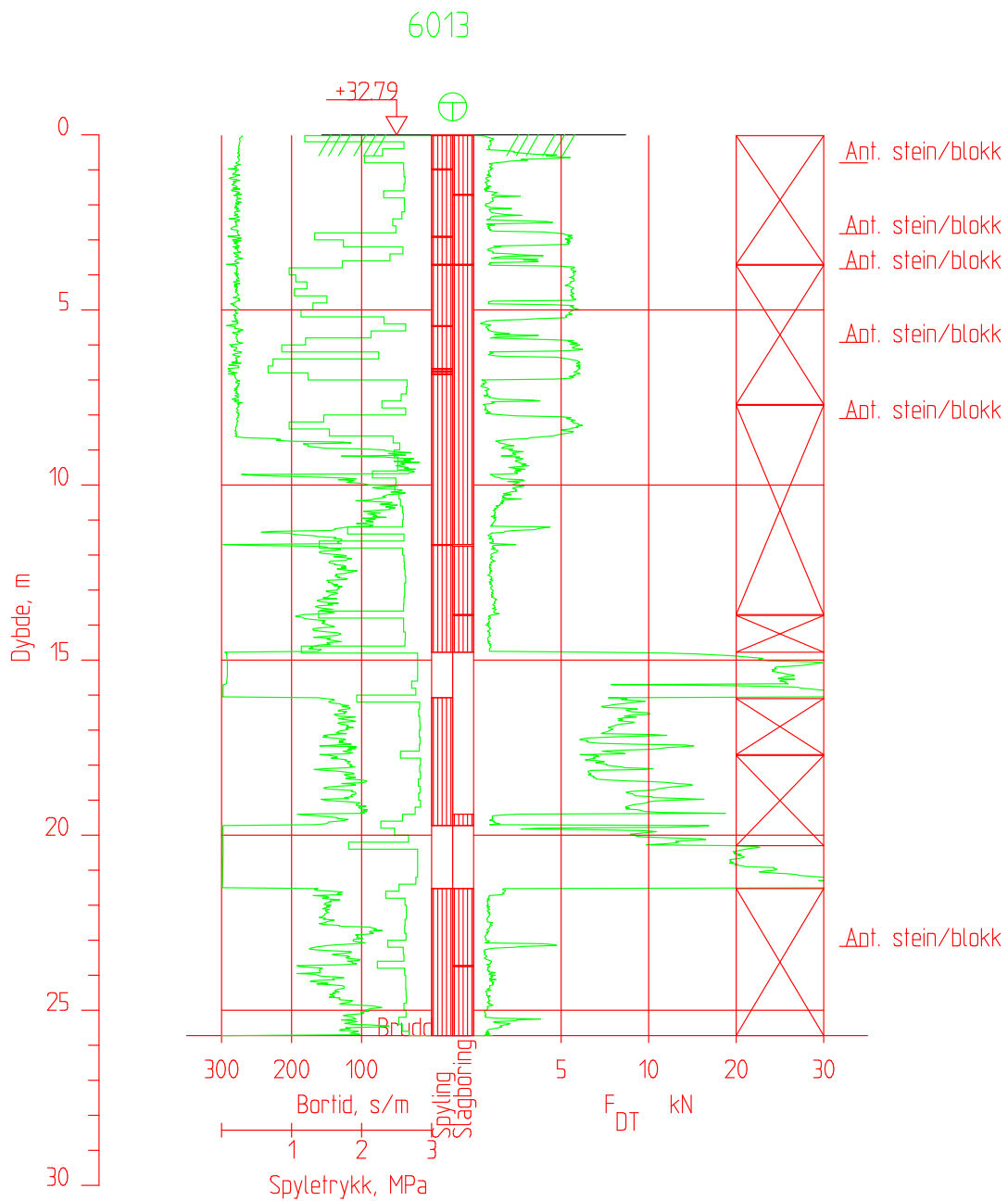
Borhull 6012

Dato boret :09.04.2019

$M = 1 : 100$

BG

19756



Posisjon: X 1122557.22 Y 109947.02

Totalsondering

Borhull 6013

Dato boreal :09.04.2019

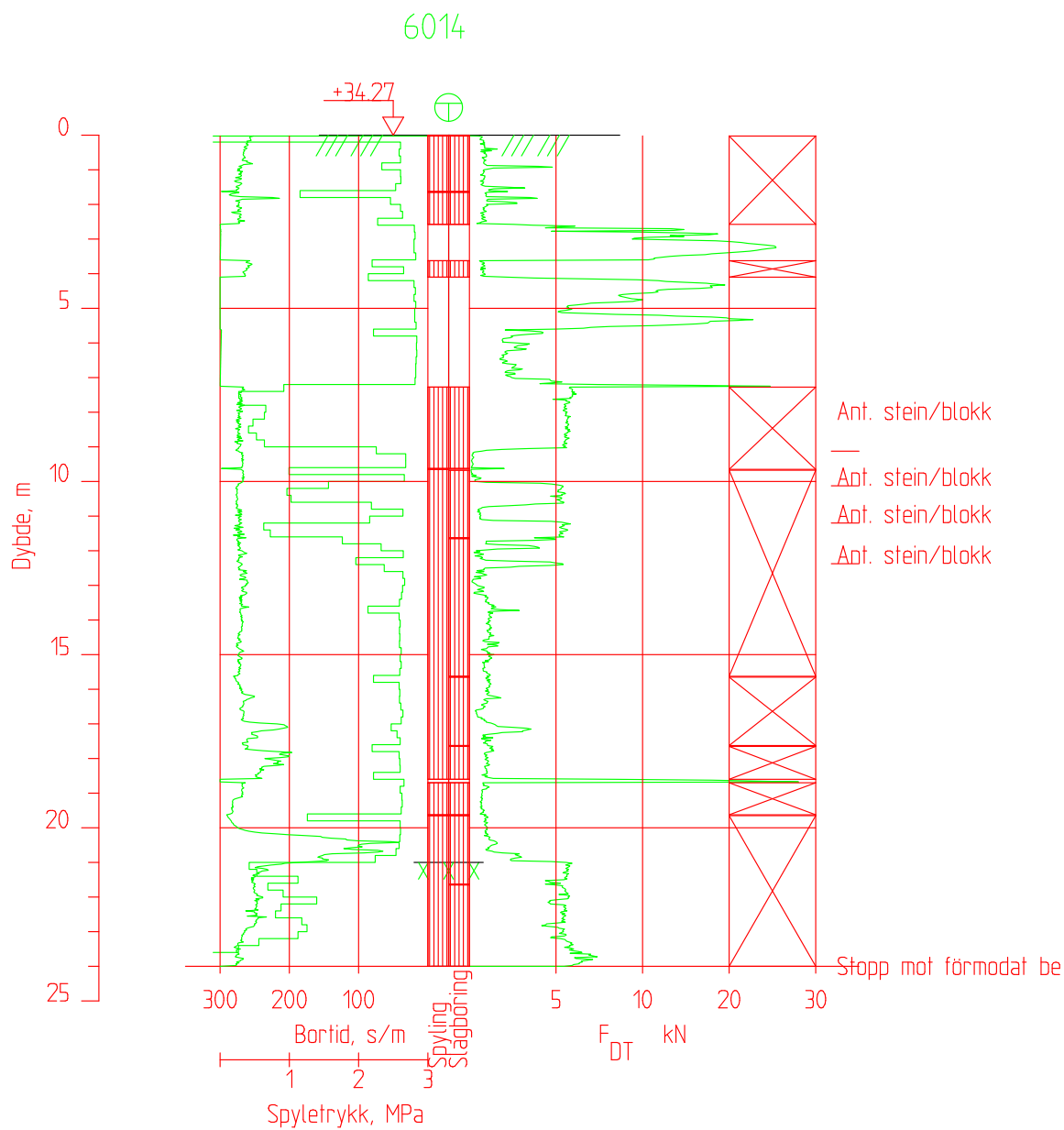
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122545.55 Y 110042.97

Totalsondering

Borhull 6014

Dato boret :09.04.2019

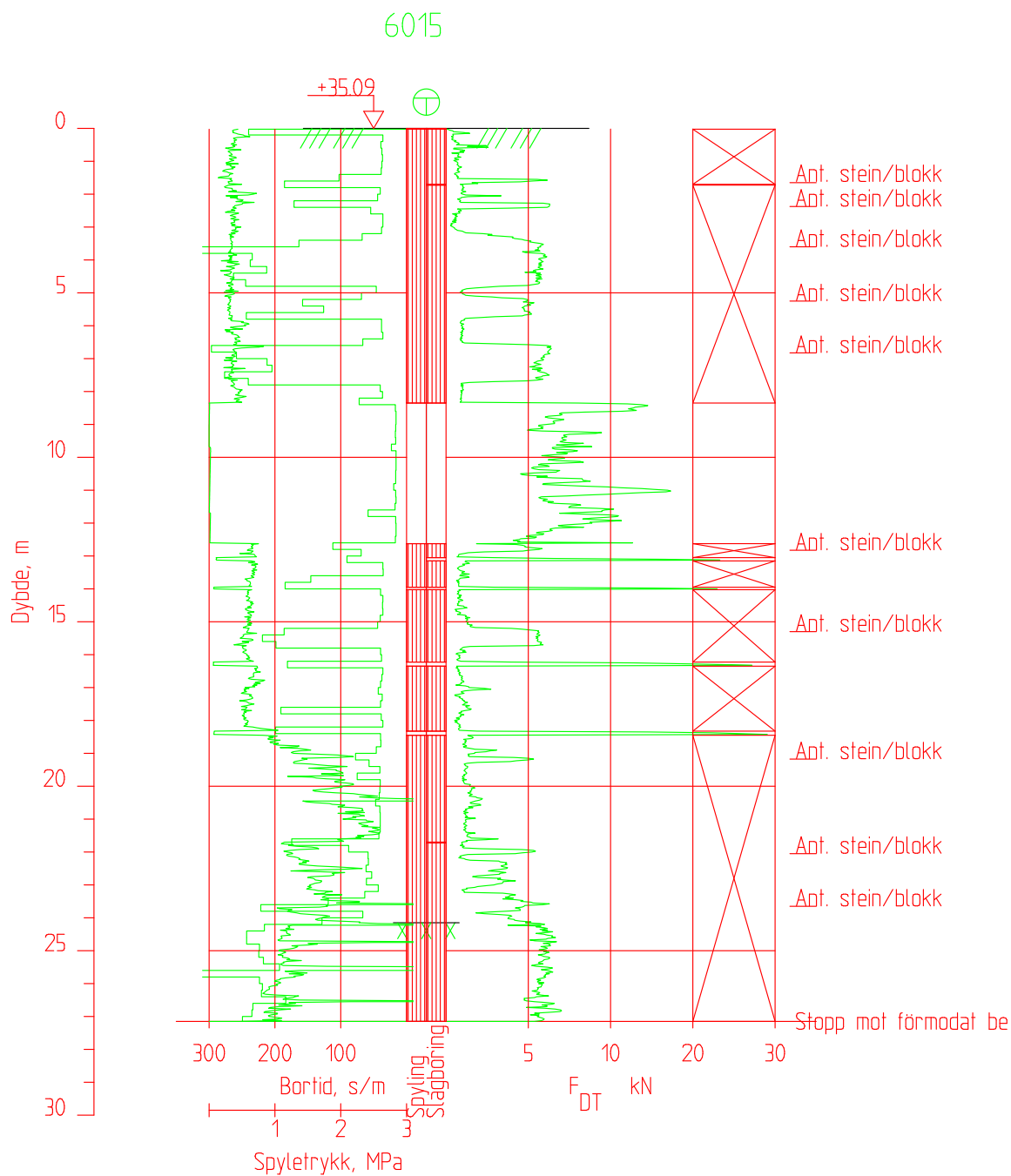
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122526.99 Y 110102.07

Totalsondering

Borhull 6015

Dato boret :10.04.2019

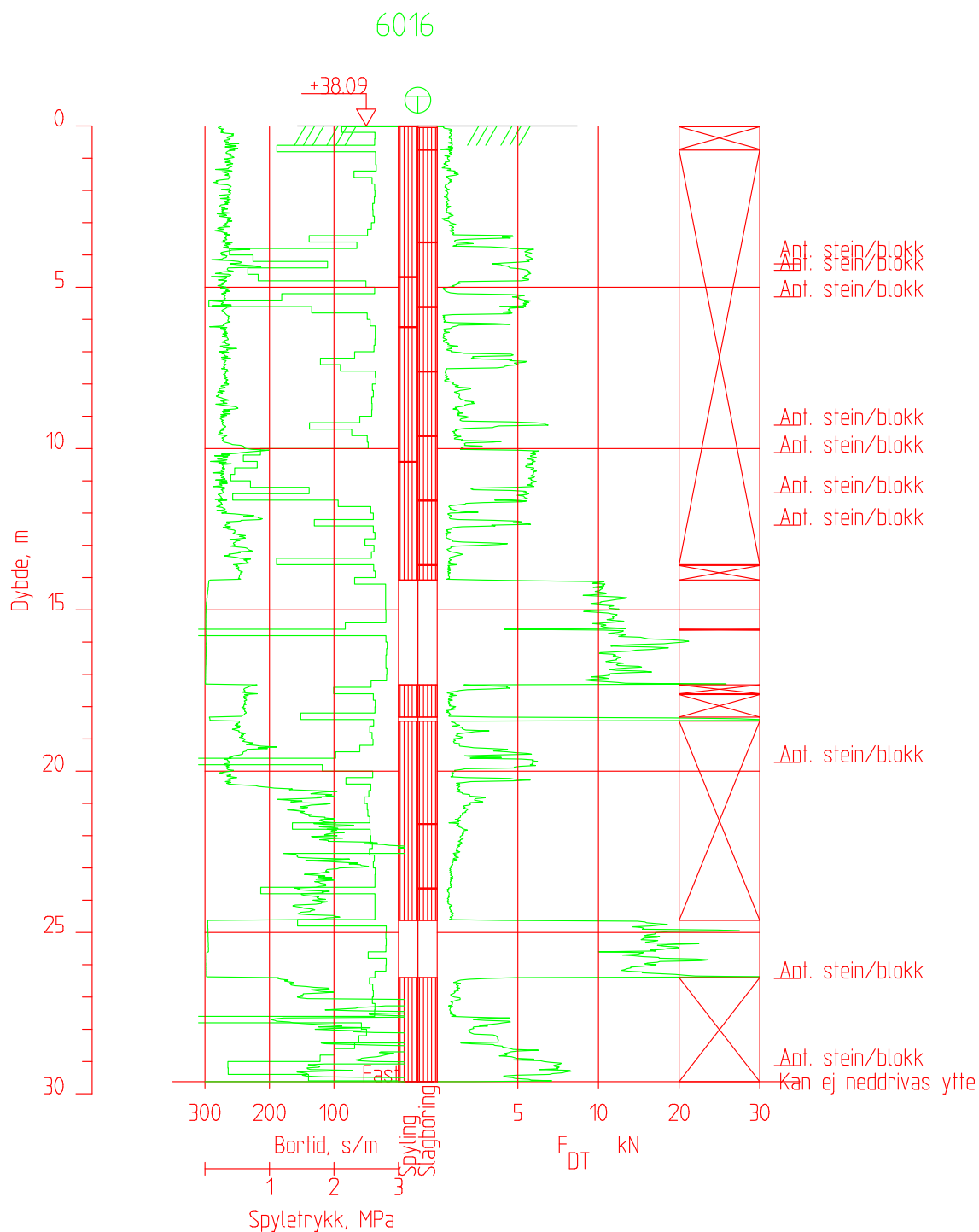
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M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122513.70 Y 110124.51

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

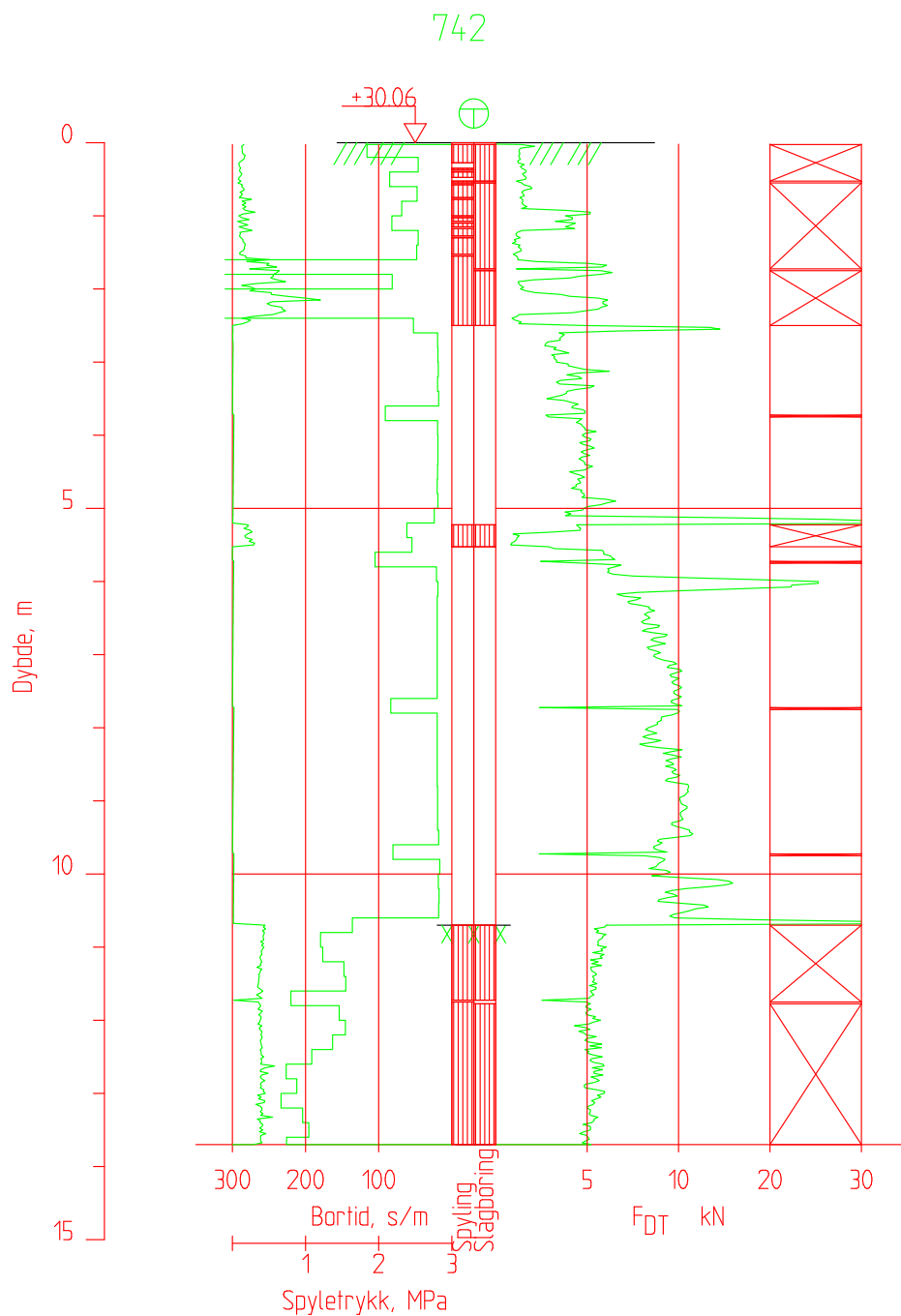
Borhull 6016

Dato boreal :10.04.2019

M = 1 : 200

BG

19756



Posisjon: X 1122740.78 Y 109734.35

Totalsondering

Borhull 742

Dato boret :28.03.2017

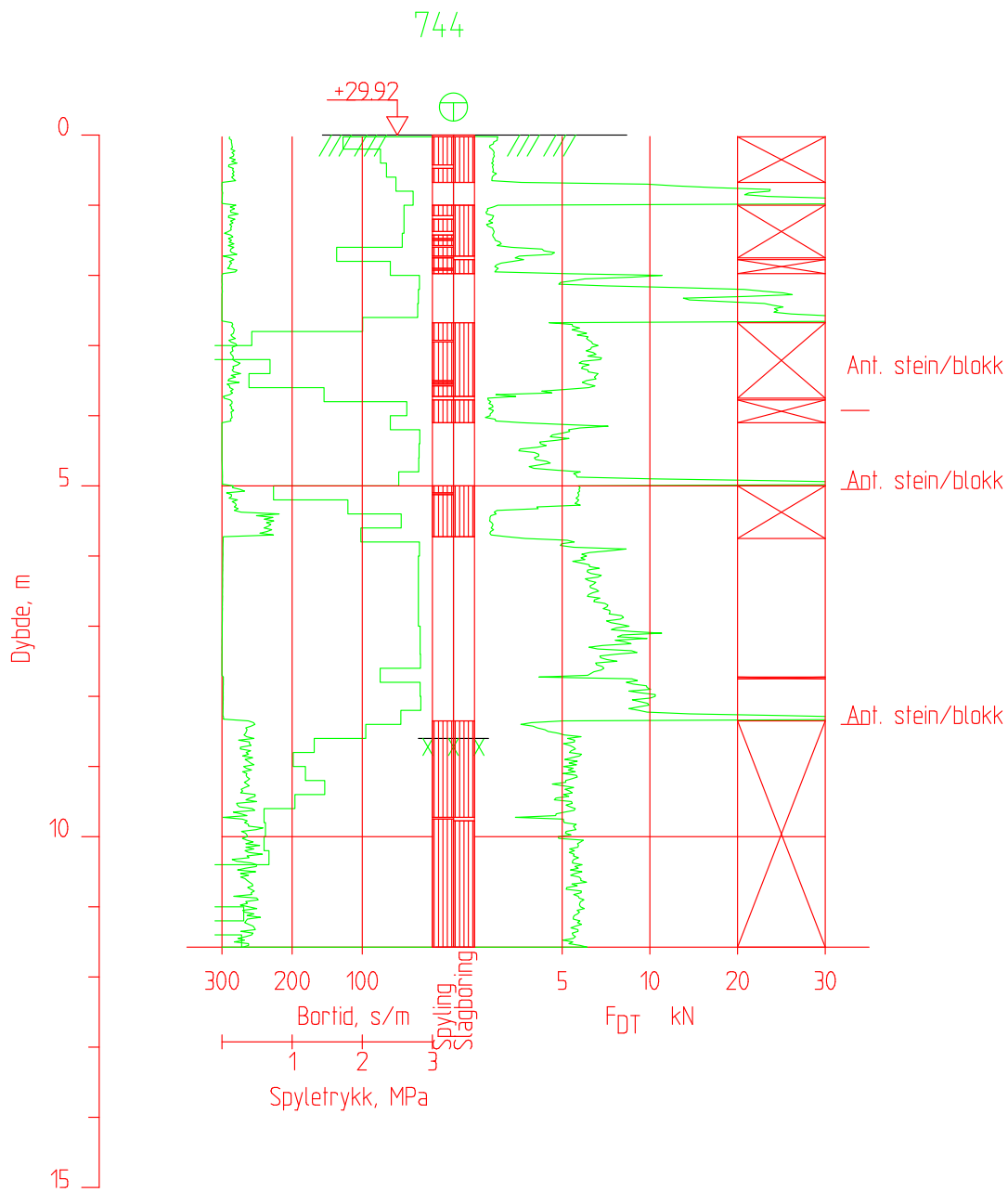
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M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122725.74 Y 109725.00

Totalsondering

Borhull 744

Dato boret :28.03.2017

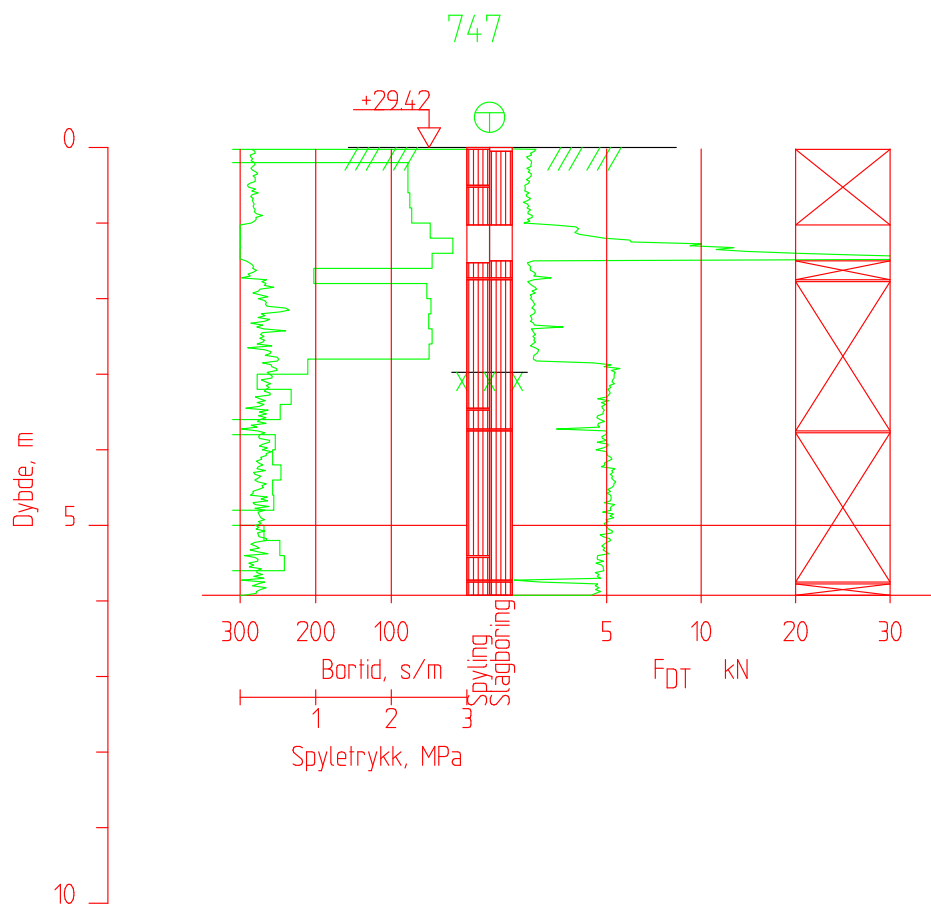
EIFFAGE

$M = 1 : 100$

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122692.72 Y 109709.35

Totalsondering

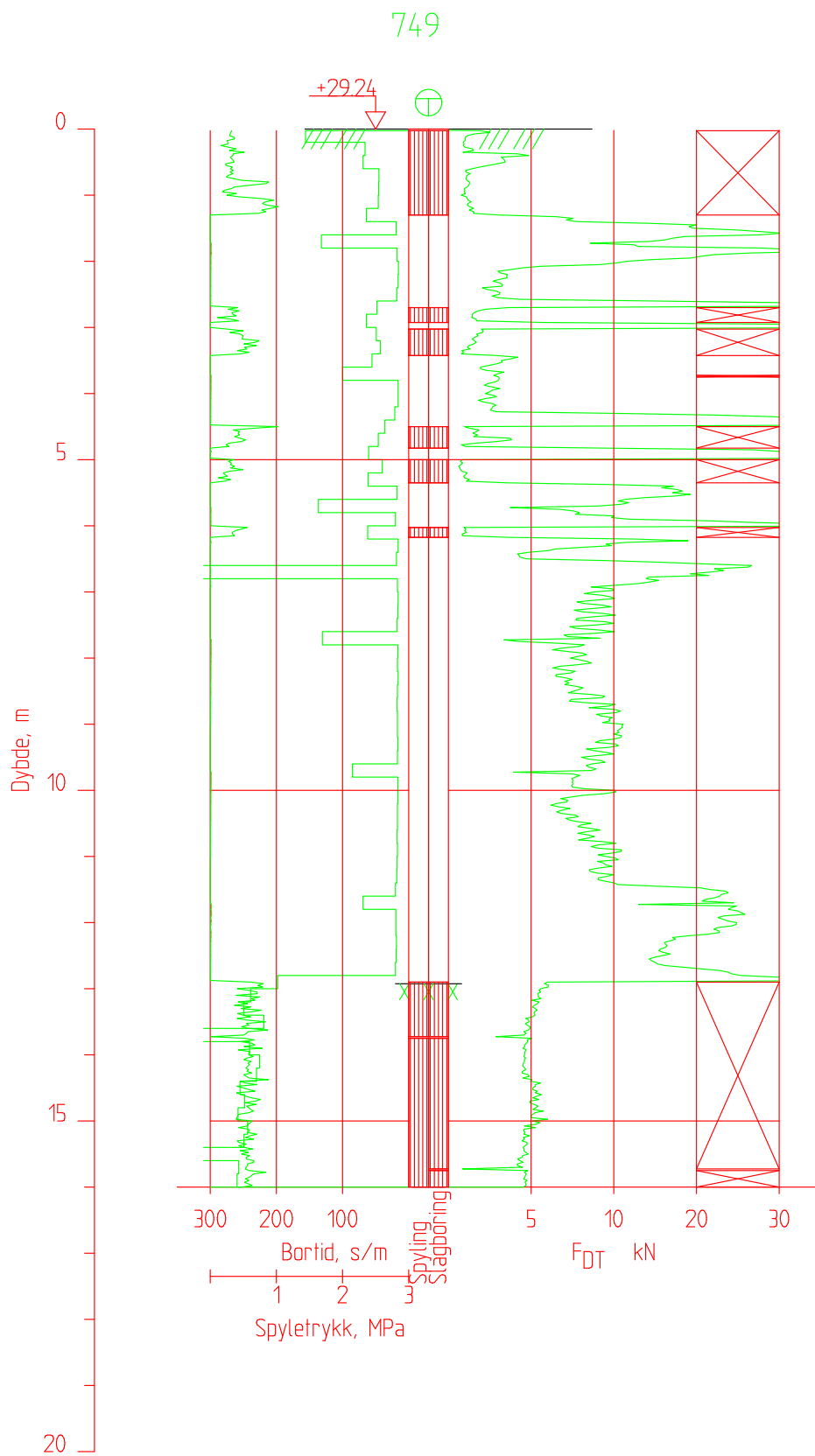
EIFFAGE

E18 Langangen Rugtvedt

Borhull 747

M = 1 : 100

Dato boret :28.03.2017



Posisjon: X 1122679.95 Y 109701.60

Totalsondering

Borhull 749

Dato boret :21.03.2017

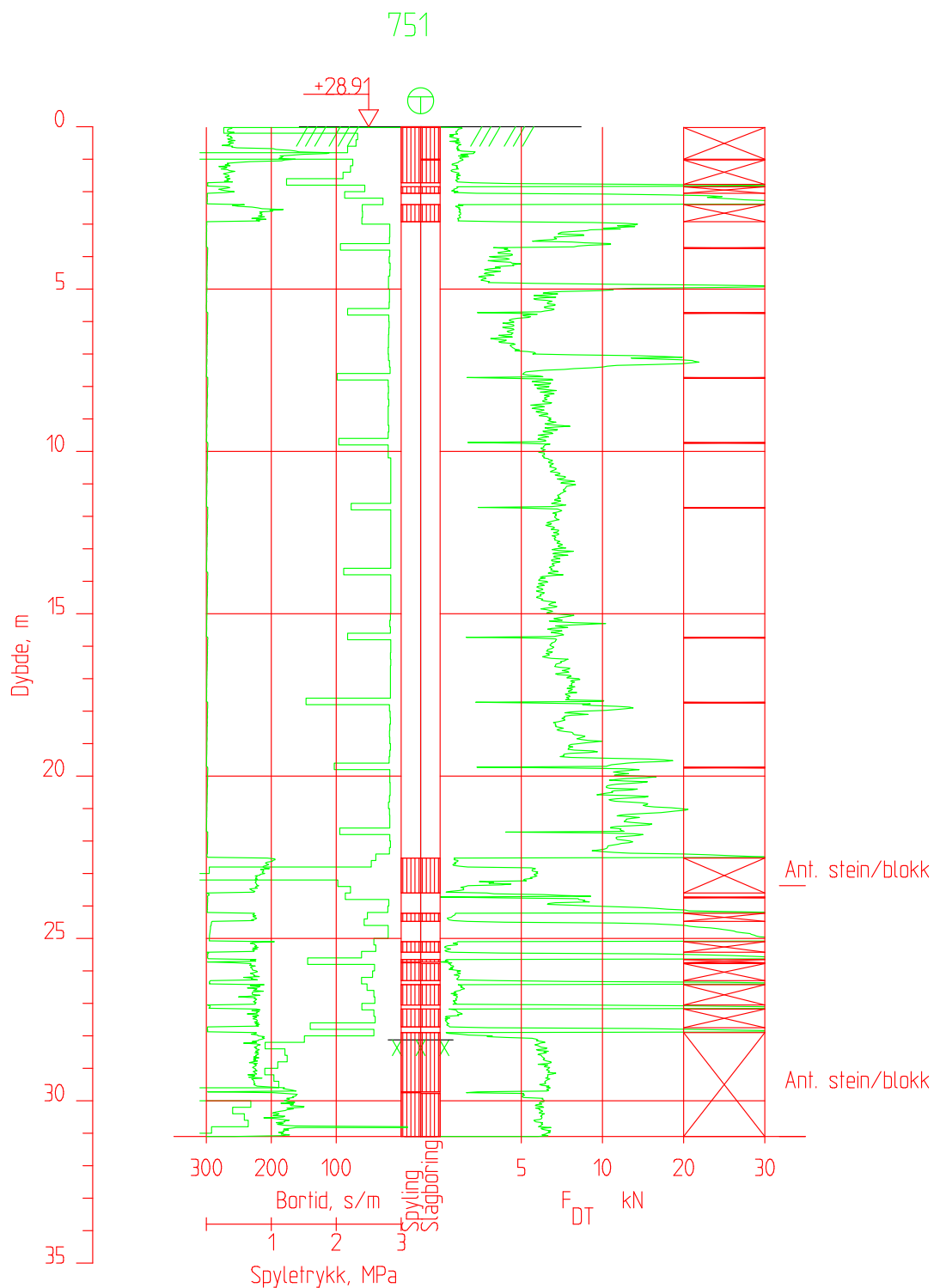
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122653.98 Y 109689.04

Totalsondering

Borhull 751

Dato boret :28.03.2017

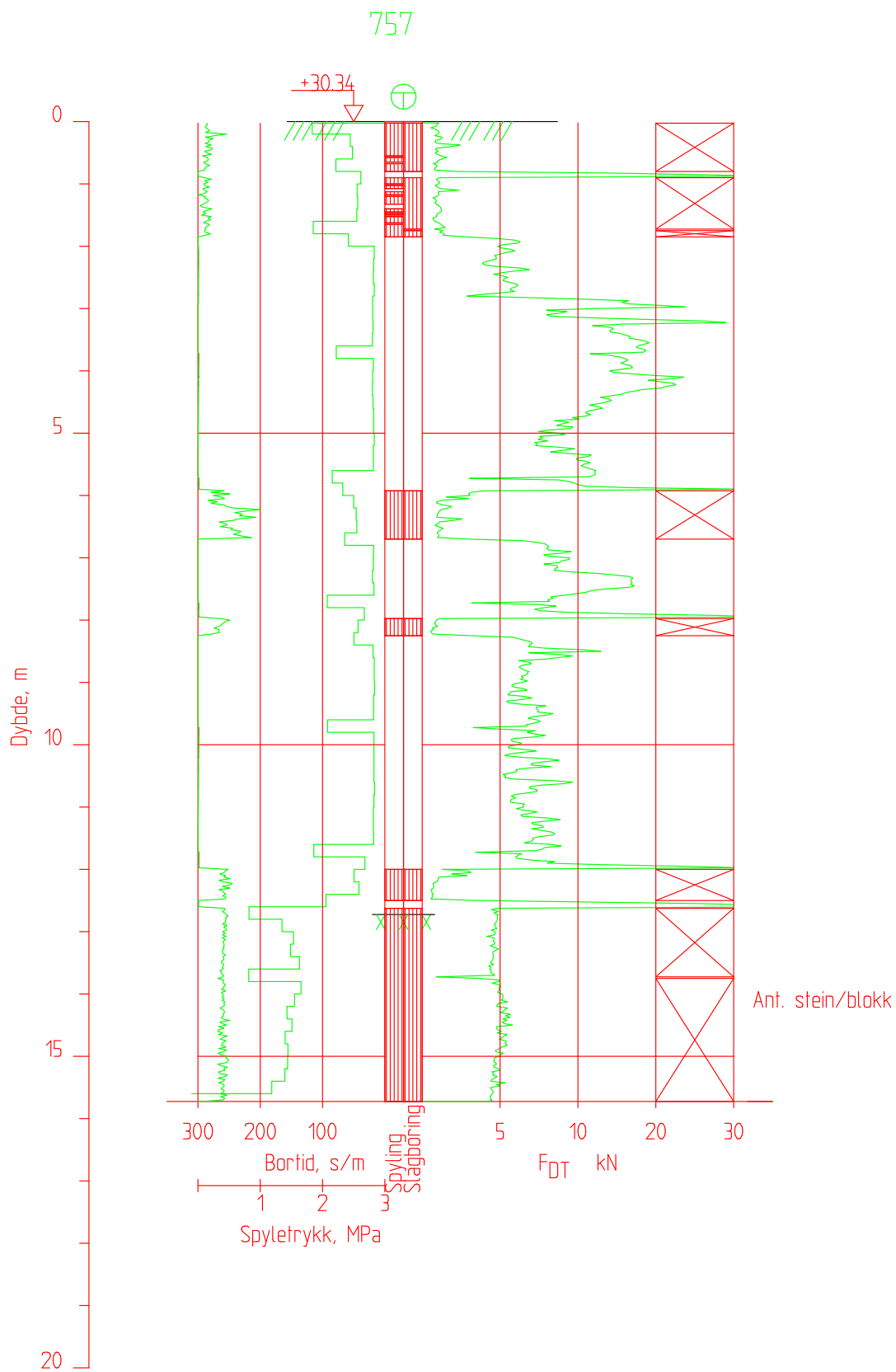
EIFFAGE

M = 1 : 200

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122698.57 Y 109747.33

Totalsondering

Borhull 757

Dato boret :28.03.2017

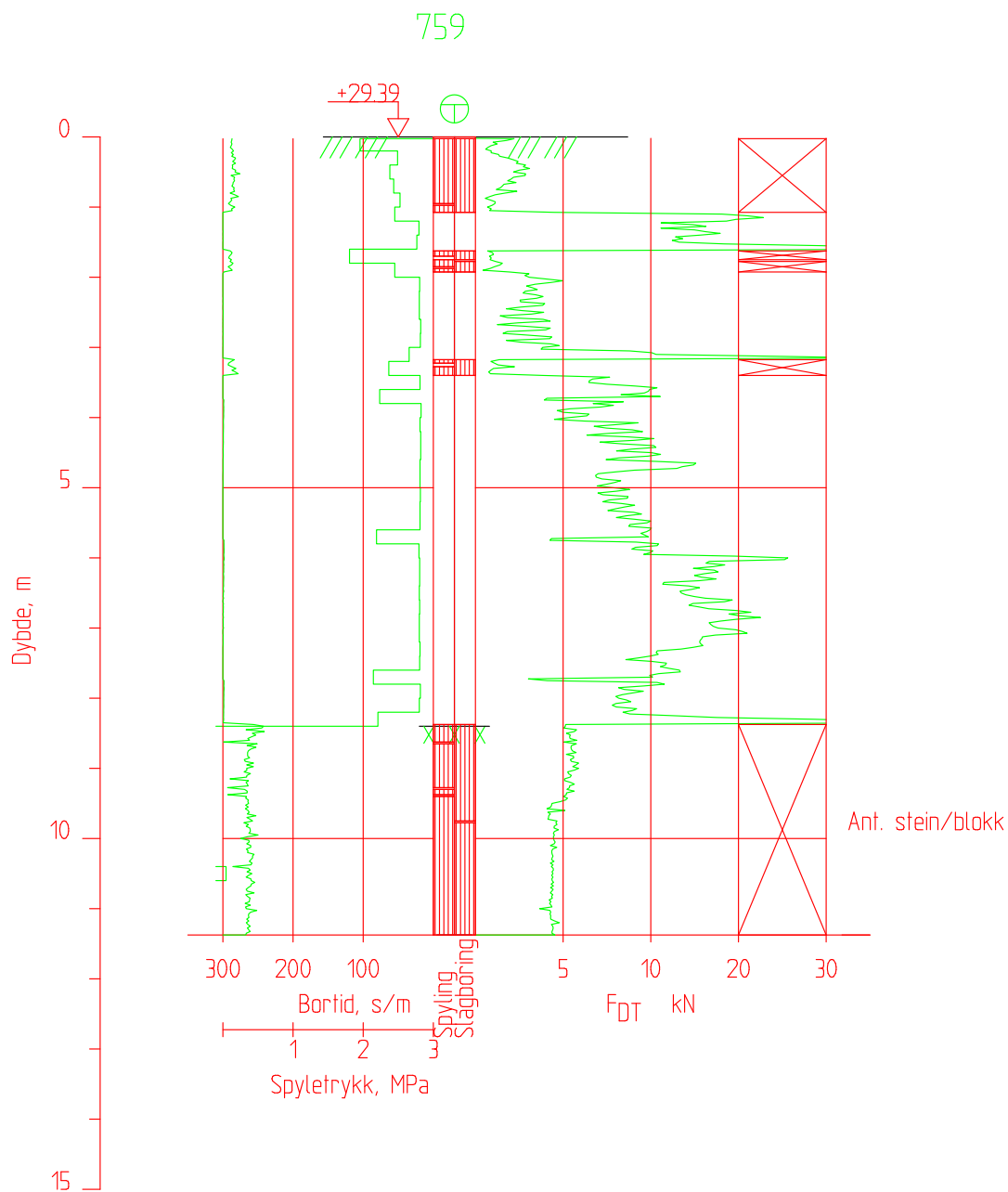
EIFPAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1122682.52 Y 109739.94

Totalsondering

Borhull 759

Dato boret :21.03.2017

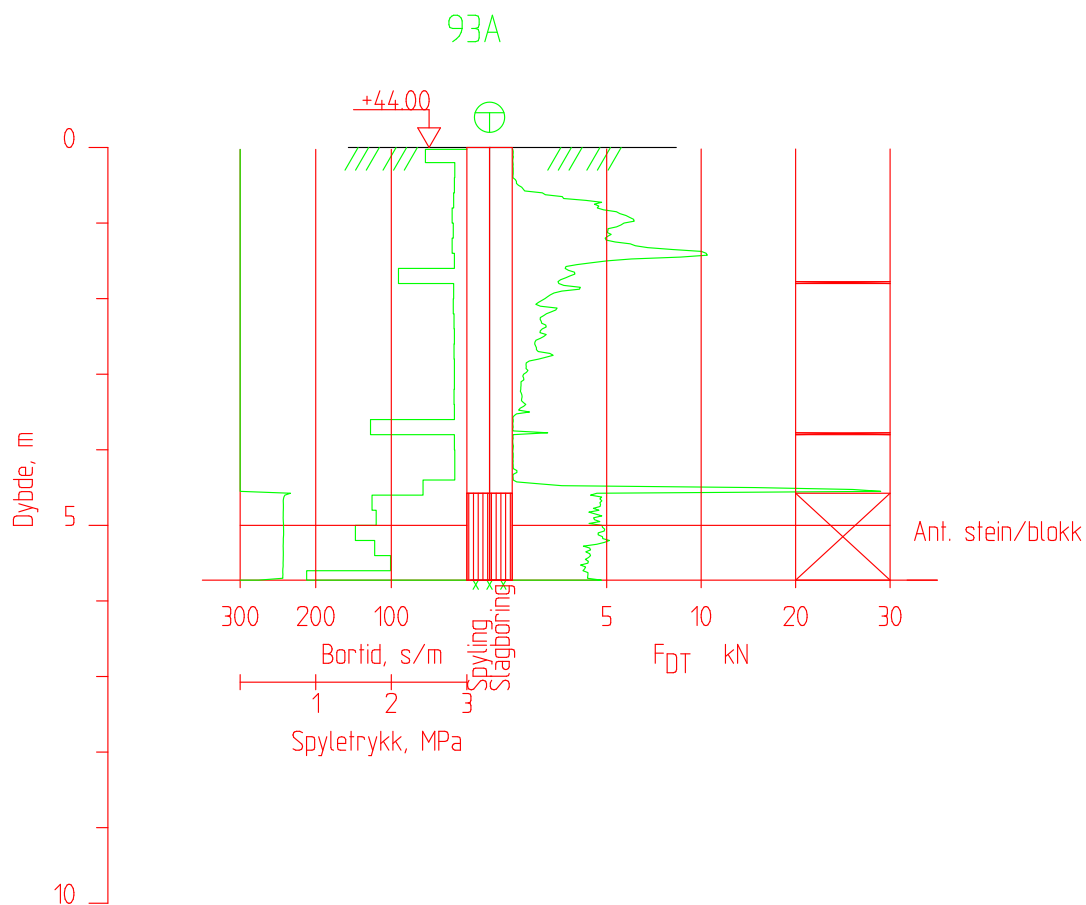
EIFPAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1120342.04 Y 109420.66

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

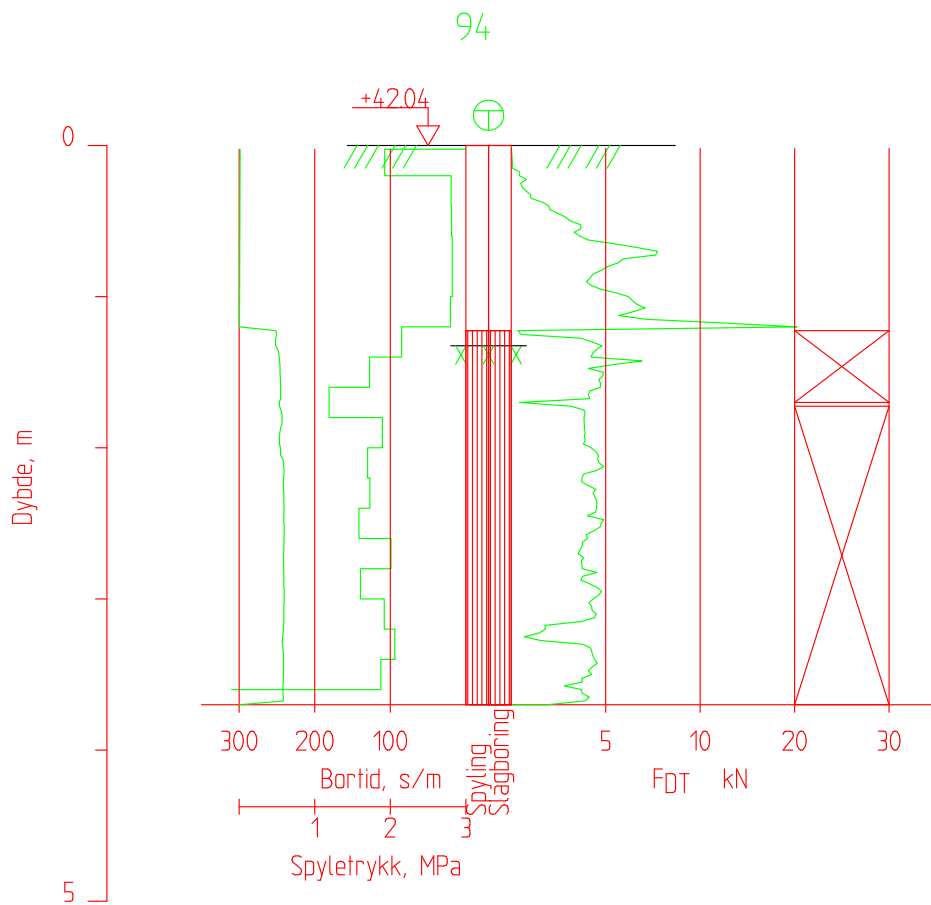
Borhull 93A

Dato boret :22.11.2016

M = 1 : 100

BG

19756



Posisjon: X 1120329.33 Y 109439.87

Totalsondering

EIFFAGE

E18 Langangen Rugtvedt

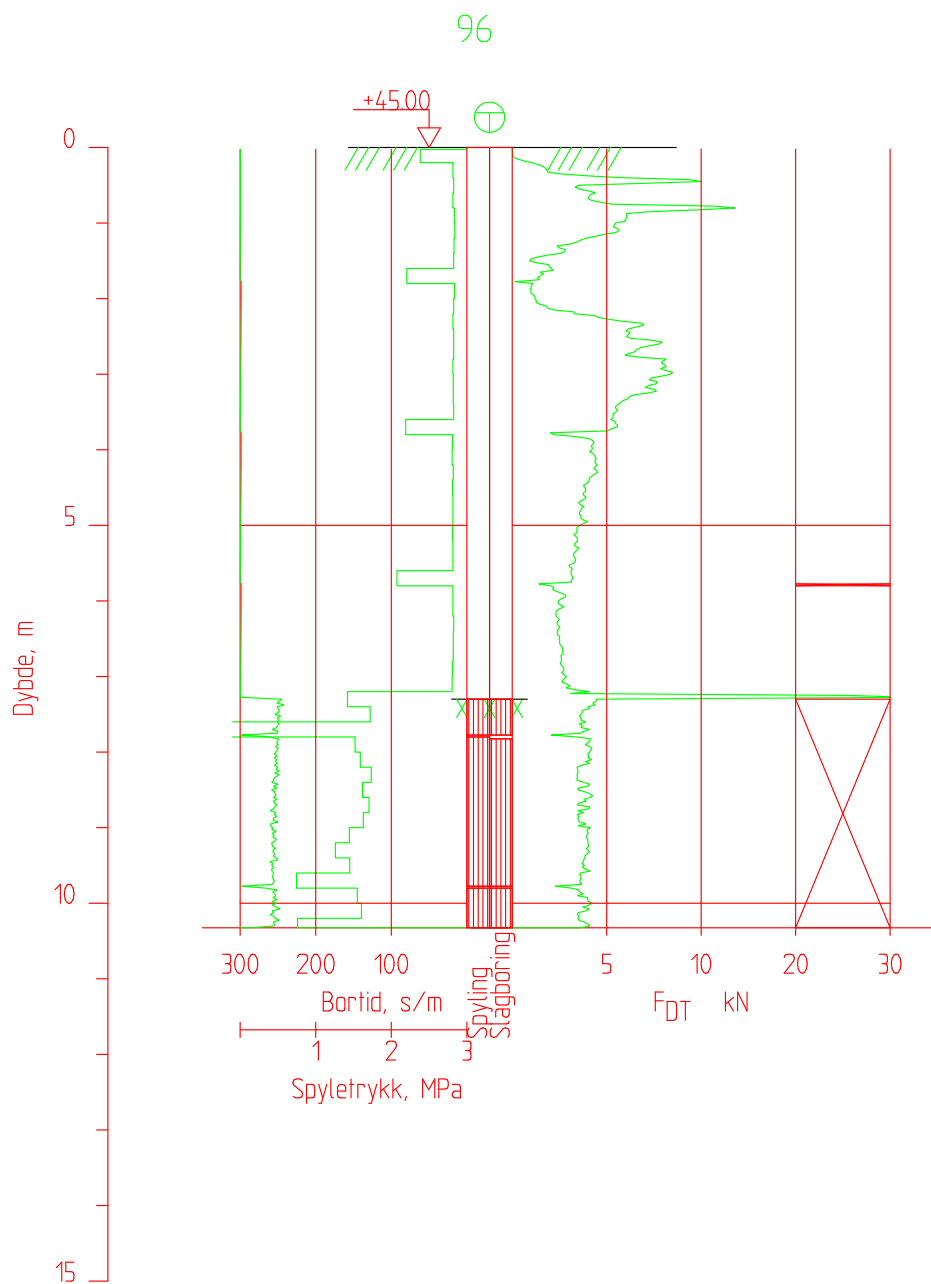
Borhull 94

Dato boreal :22.11.2016

M = 1 : 50

BG

19756



Posisjon: X 1120249.73 Y 109431.90

Totalsondering

Borhull 96

Dato boret :22.11.2016

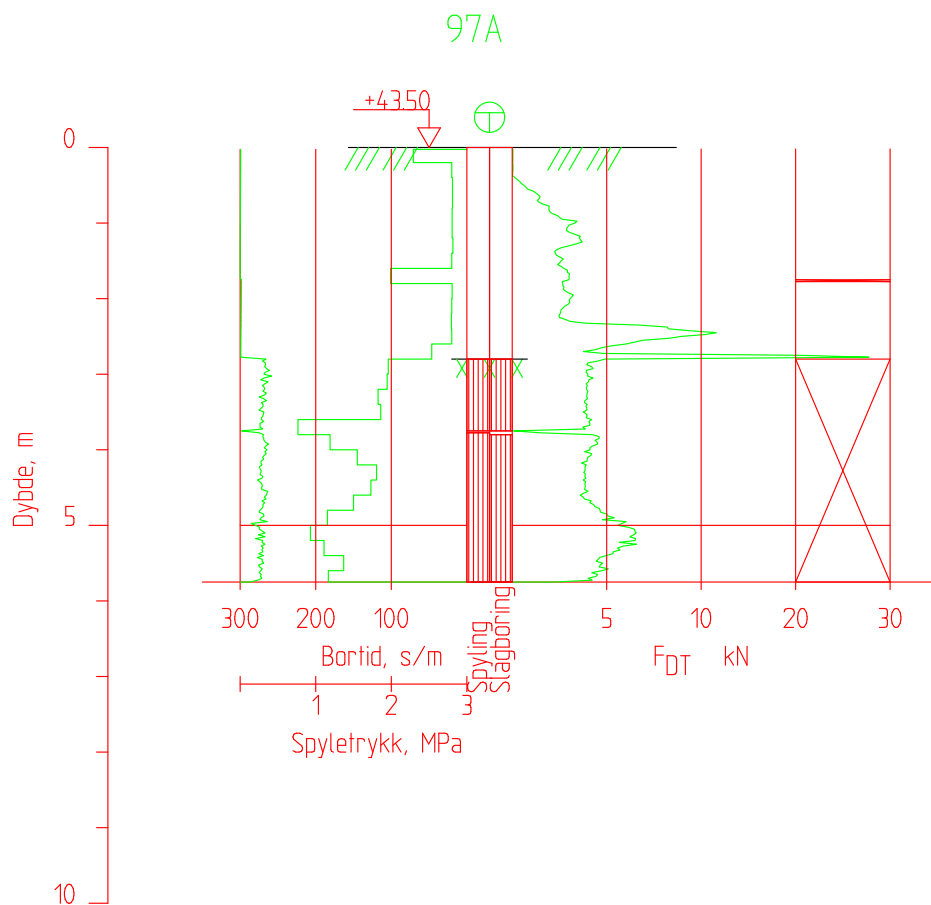
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1120240.23 Y 109401.17

Totalsondering

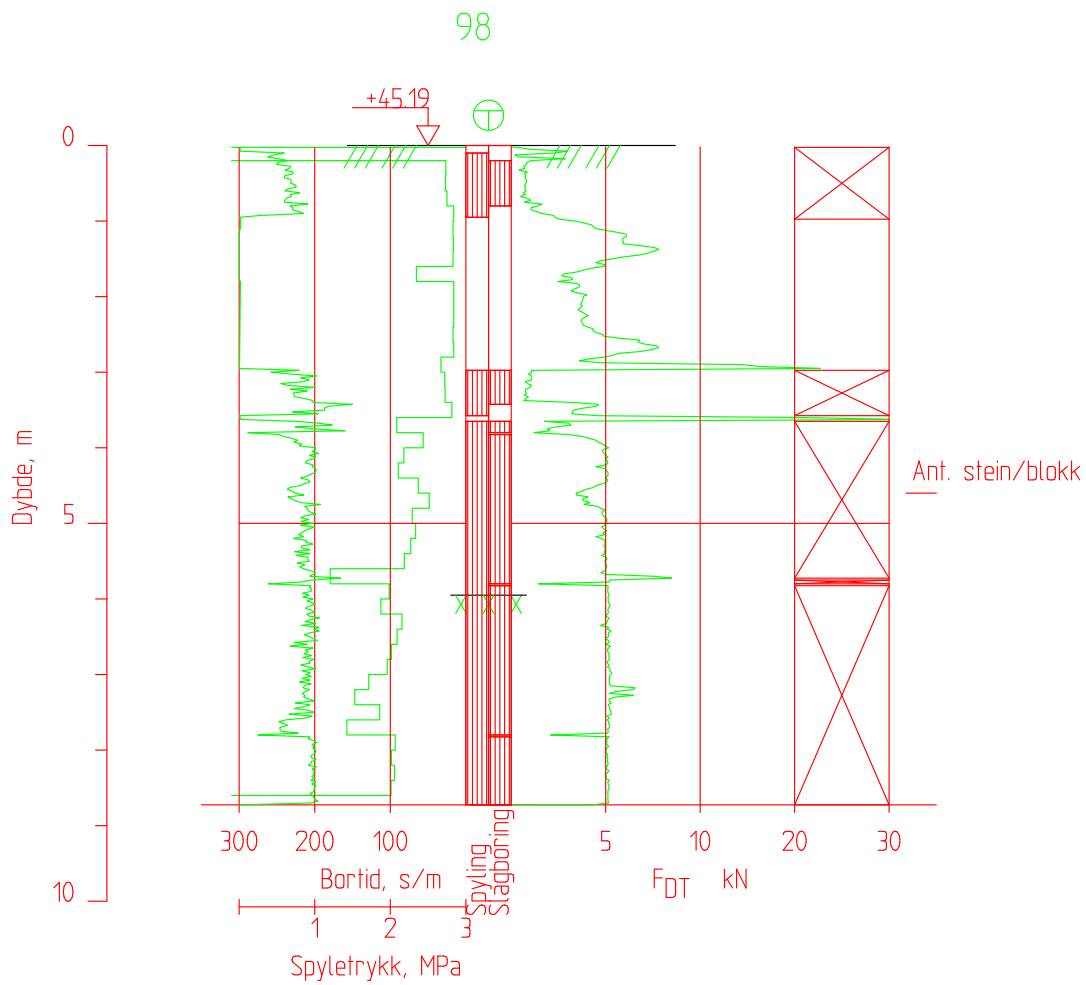
EIFFAGE

E18 Langangen Rugtvedt

Borhull 97A

Dato boref :22.11.2016

M = 1 : 100



Posisjon: X 1120210.51 Y 109418.12

Totalsondering

Borhull 98

Dato boreal :16.11.2016

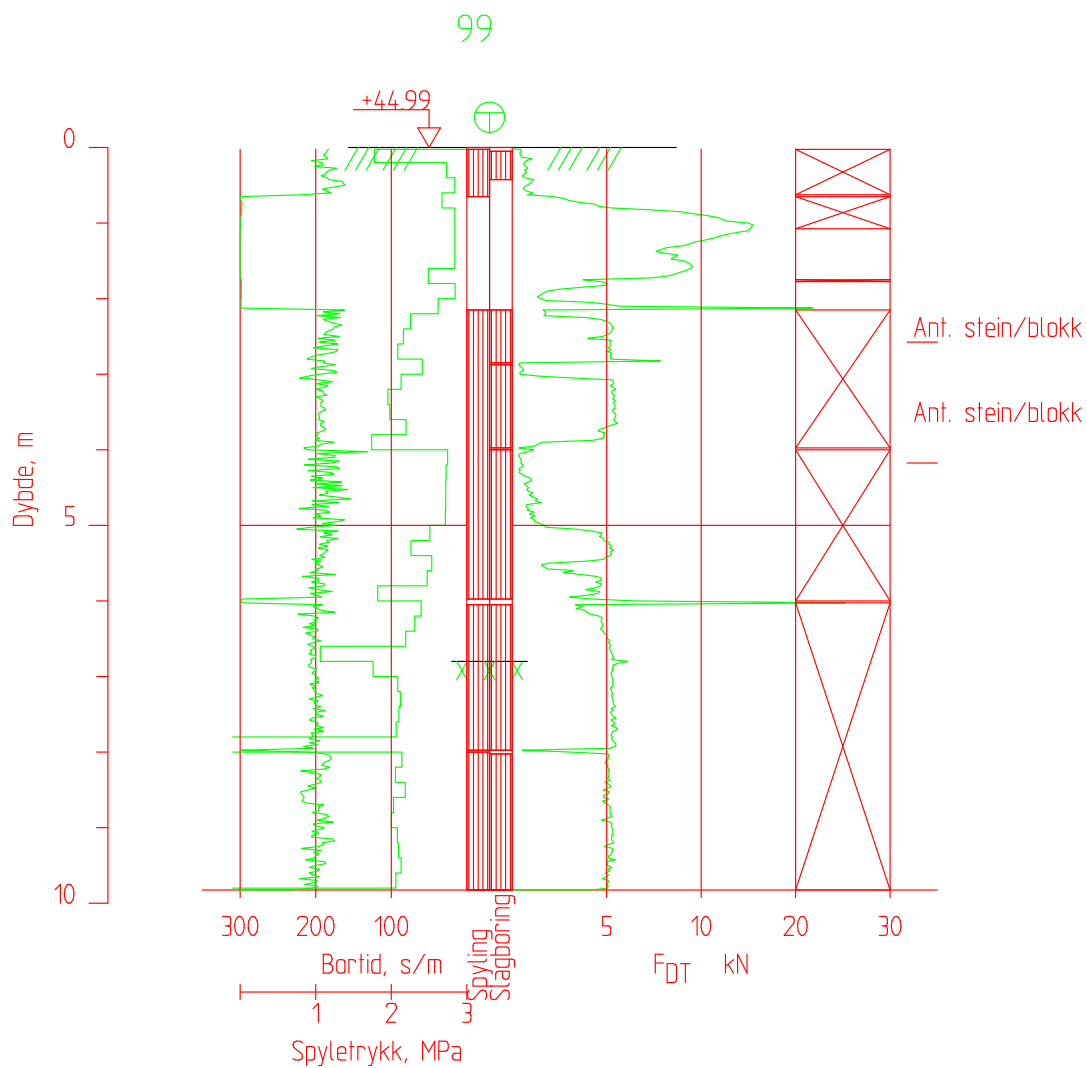
EIFFAGE

$M = 1 : 100$

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1120217.80 Y 109409.91

Totalsondering

Borhull 99

Dato boret :16.11.2016

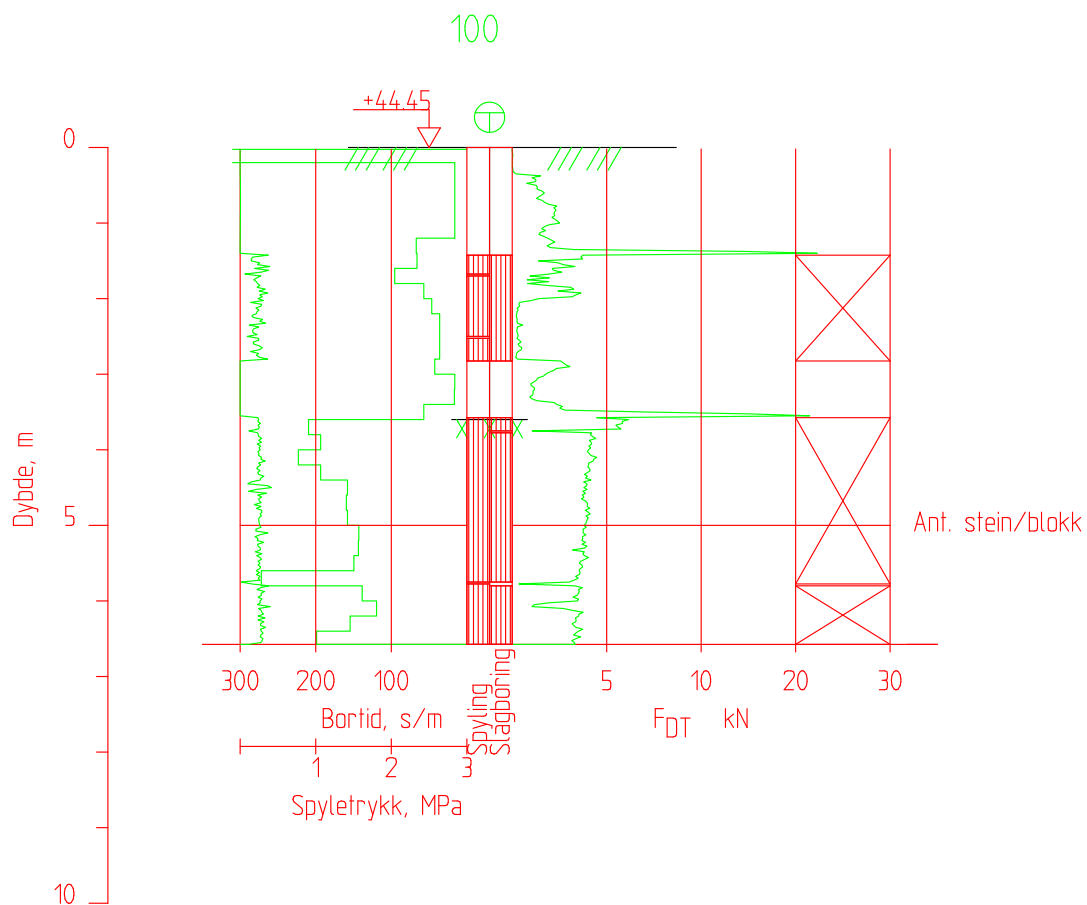
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1120224.93 Y 109391.83

Totalsondering

Borhull 100

Dato boret :17.11.2016

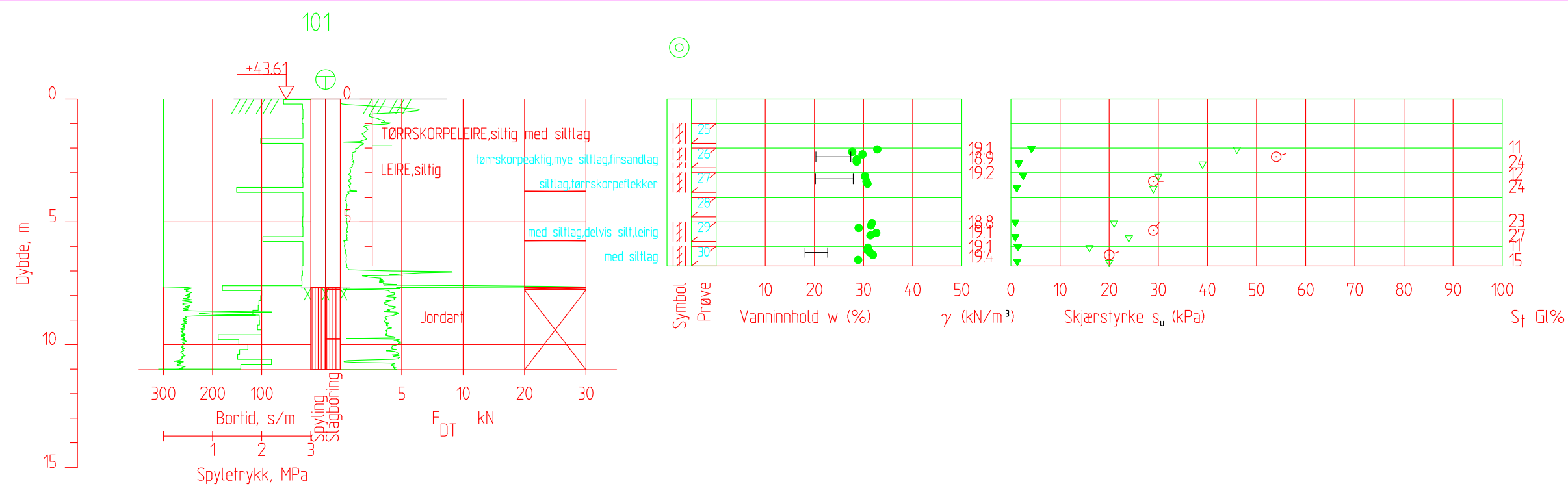
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1120165.09 Y 109399.88

Totalsondering Borprofil

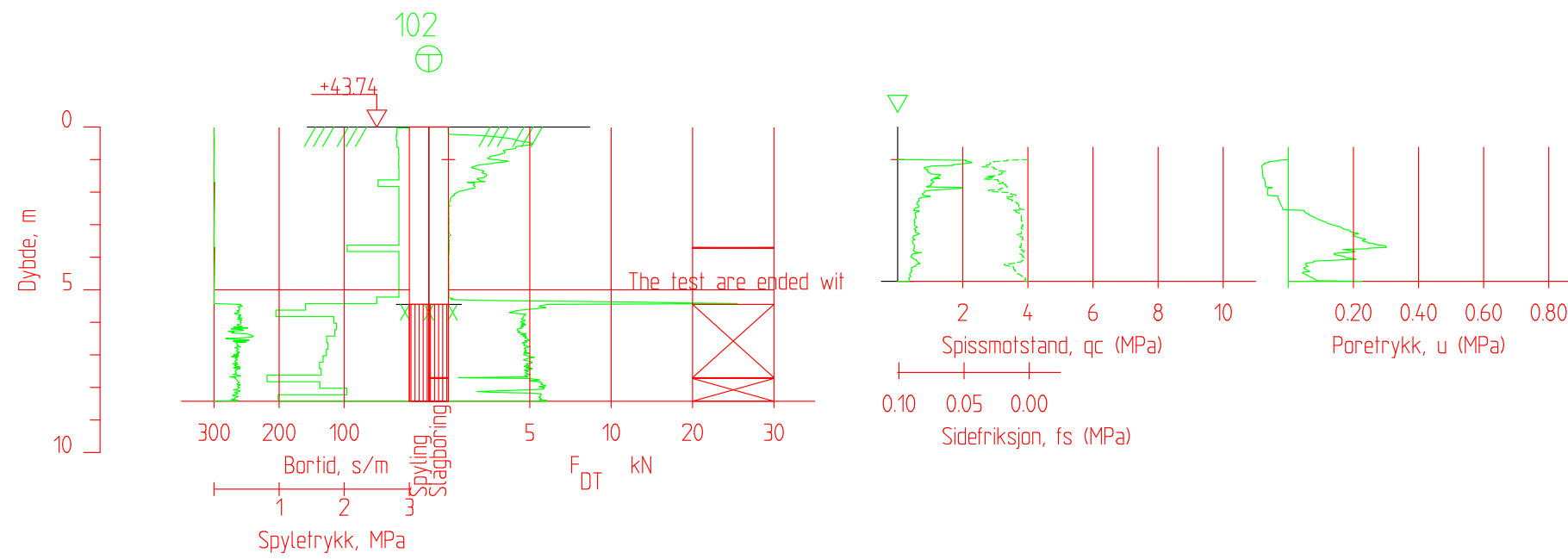
Borhull 101

Dato boret :17.11.2016

EIFFAGE

M = 1 : 200

E18 Langangen Rugtvedt



Posisjon: X 1120170.25 Y 109382.64

Totalsondering CPT-sondering

EIFFAGE

E18 Langangen Rugtvedt

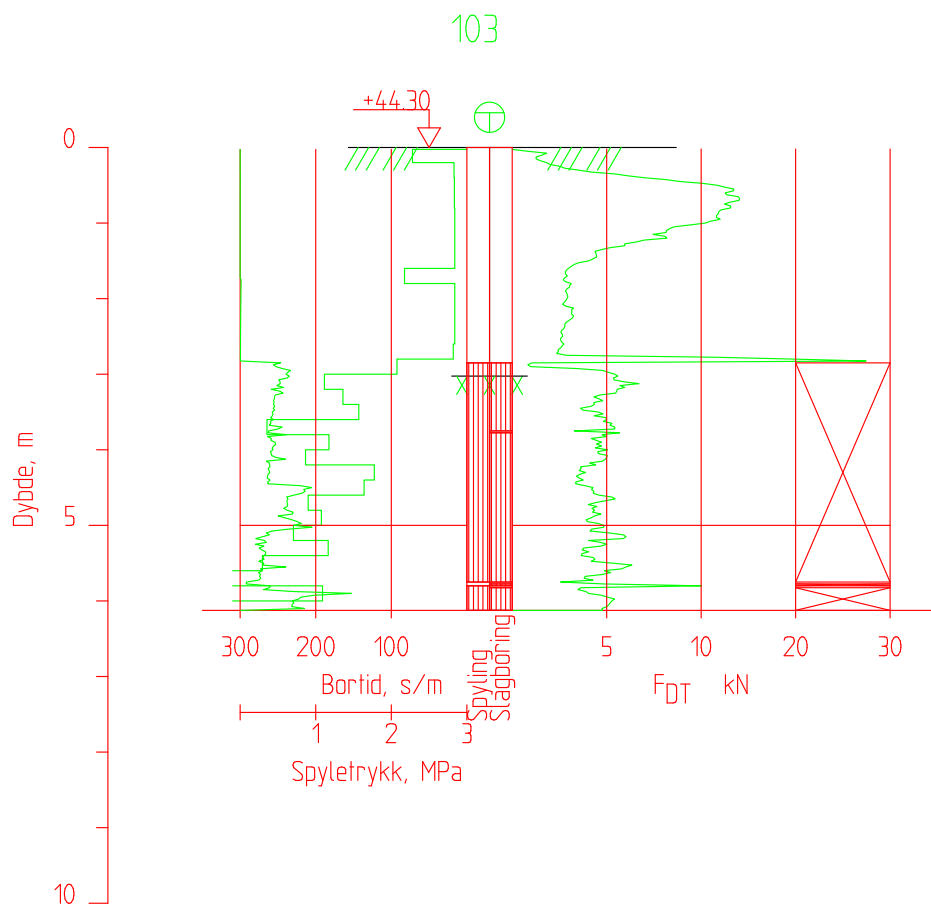
Borhull 102

Dato boreal :14.02.2017

$M = 1 : 200$

BG

19756



Posisjon: X 1120124.86 Y 109406.39

Totalsondering

Borhull 103

Dato boret :17.11.2016

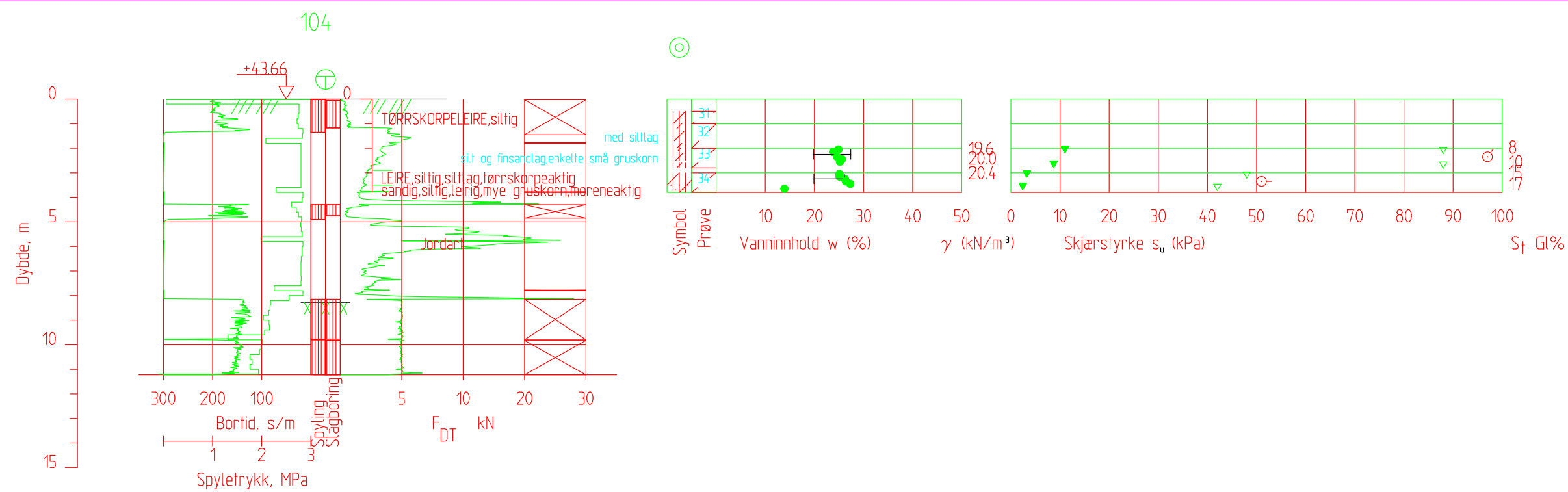
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



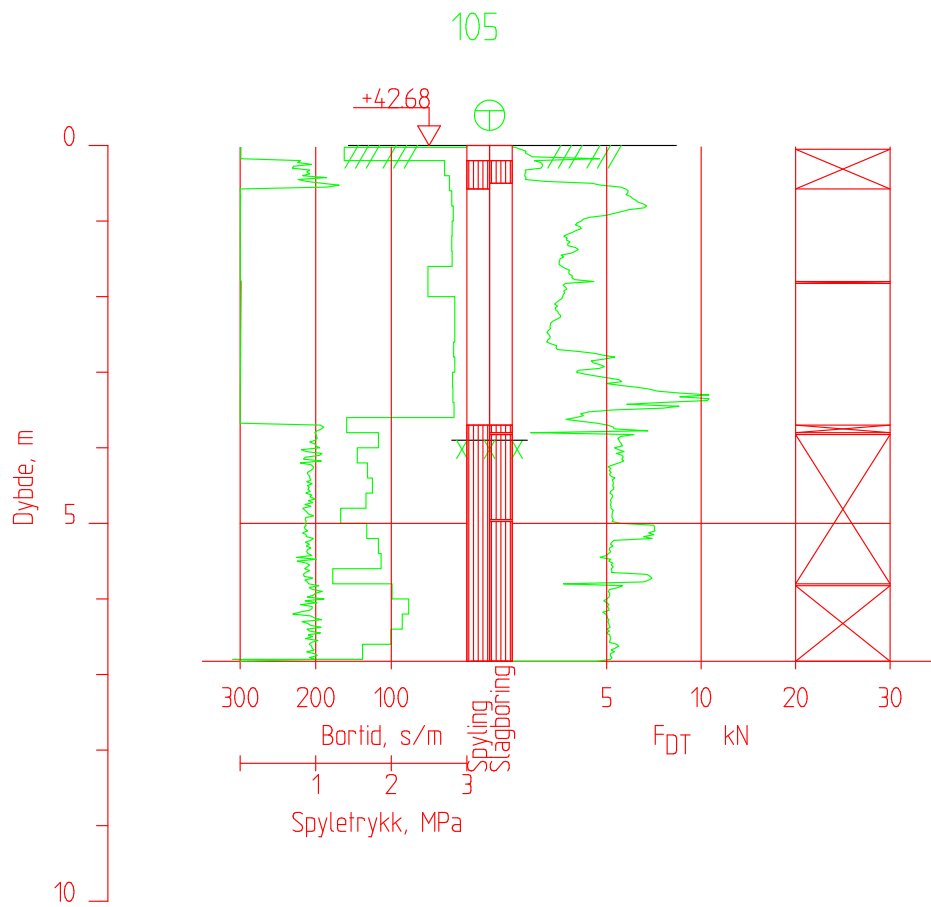
Posisjon: X 1120028.33 Y 109369.38

Totalsondering Borprofil
EIFFAGE
E18 Langangen Rugtvedt

Borhull 104

Dato boret :16.11.2016

M = 1 : 200



Posisjon: X 1120012.81 Y 109365.87

Totalsondering

Borhull 105

Dato boret :16.11.2016

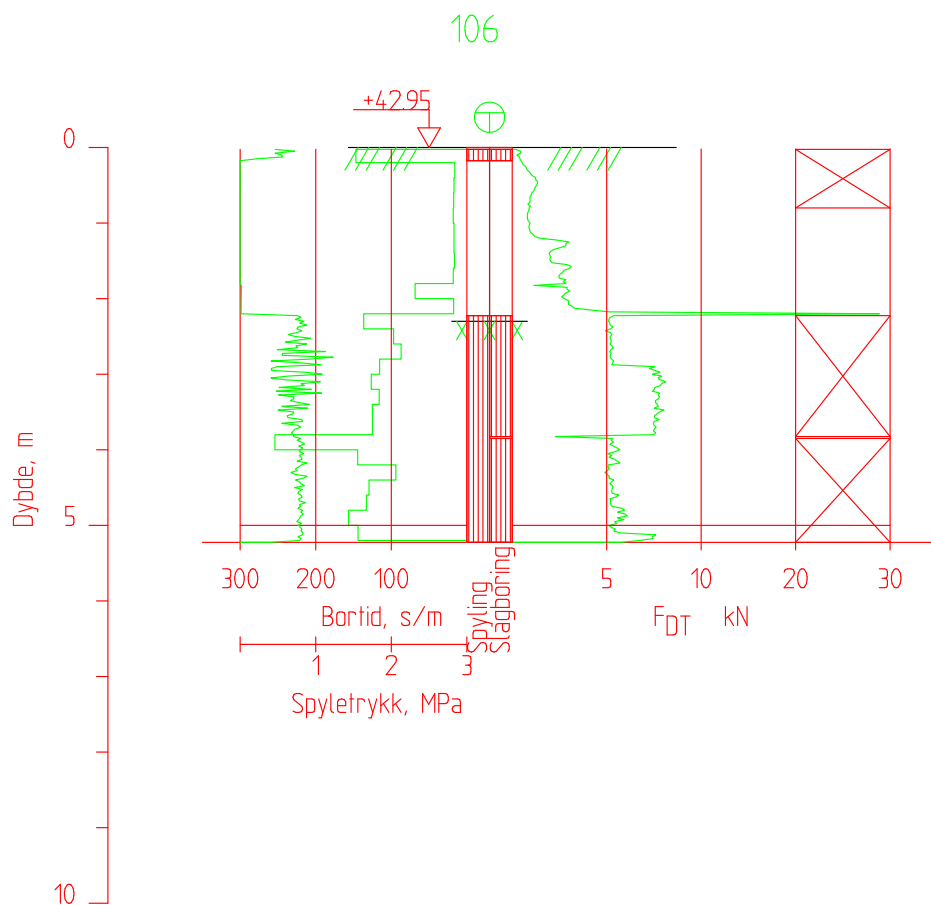
EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756



Posisjon: X 1120001.03 Y 109353.12

Totalsondering

Borhull 106

Dato boret :16.11.2016

EIFFAGE

M = 1 : 100

E18 Langangen Rugtvedt

BG

19756

Depth (m)	Description	el.	Sample	Test	Water content (%) and consistency limit					ρ (g/cm ³)	ρ_s (g/cm ³)	Organic content (%)	Undrained shear strength (kPa)					Sensitivity
					10	20	30	40	50				10	20	30	40	50	
5	Silty CLAY	weathered																
	Silty CLAY	weathered																
	Silty CLAY	a few sand grains																
	Silty CLAY	some thin layers of silt in bottom		TO						1,99	2,76		▼1,1	▼		○		13
													▼1,0	▼				18
	Silty CLAY												▼1,2	▼		○		14
	transition to QUICK CLAY, layers of silt/sand			GT						1,96	2,84		▼0,3	▼				38
	Silty CLAY	layers of various thickness of sand and silt								2,02			▼0,9	▼		○		13
10																		
	Silty CLAY												▼					18
	Silty CLAY	disturbed 20cm in top		O						1,91	2,77		▼0,7	▼		○		14
	Sandy, clayey SILT	disturbed											▼1,2	▼				15
15																		
20																		

Symbols:

Unconfined compression test (line specifies strain (%) at failure)

○ Water content
 — Plasticity Index (PI)

ISO 17892-6: 2017

▼ Disturbed fall cone
 ▼ Undisturbed fall cone

 ρ = Density ρ_s = Grain density

T = Triaxial test

O = Oedometer test

G = Grain size distribution

Ground water level:

Bore book:

2,0 m

Digital

Soil Sampling

Borehole:

3002

Nye Veier

Date:

2020-07-07

E18 Langangen-Rugtvedt, supplementary ground investigations

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Drawn by:

GEO

Reviewed by:

ANNM

Approved by:

STEG

Project number:

10217934-02

Drawing number:

RIG-TEG-201

Revision number:

00

Ground investigations field and lab profiles PZ-GIT-S143 (1)																			
Depth (m)	Description		Sample	Test	Water content (%) and consistency limit					ρ (g/cm ³)	ρ_s (g/cm ³)	Organic content (%)	Undrained shear strength (kPa)					Sensitivity	
					10	20	30	40	50				10	20	30	40	50		
	el.																		
5	SAND	a few gravel grains																	
	SAND	a few gravel grains		G	O							0,5							
	SAND																		
	SAND	traces of organic matter		OG	O														
	SAND																		
10	Silty SAND			G		O													
	Silty SAND																		
	Sandy, silty MATERIAL	weathered		OG		O													
	Silty SAND																		
	Silty SAND	a few shell fragments		G		O													
15																			
20																			

Symbols:

Unconfined compression test (line specifies strain (%) at failure)

○ Water content
 └─ Plasticity Index (PI)

ISO 17892-6: 2017
 ▼ Disturbed fall cone
 ▽ Undisturbed fall cone

ρ = Density
 ρ_s = Grain density

T = Triaxial test
 O = Oedometer test
 G = Grain size distribution

Ground water level: m
 Bore book: Digital

Soil Sampling

Borehole: 4003

Nye Veier

Date: 2020-07-09

E18 Langangen-Rugtvedt, supplementary ground investigations

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Drawn by:
 GEO

Project number:
 10217934-02

Reviewed by:
 ANNM

Drawing number:
 RIG-TEG-202

Approved by:
 STEG

Revision number:
 00

Ground investigations field and lab profiles FZ-GIT-S140 (1)																			
Depth (m)	Description		Sample	Test	Water content (%) and consistency limit					ρ (g/cm ³)	ρ_s (g/cm ³)	Organic content (%)	Undrained shear strength (kPa)					Sensitivity	
					10	20	30	40	50				10	20	30	40	50		
5																			
	PEAT H5-H6, mixed with lumps of sand																		
	PEAT H5-H6, mixed with lumps of sand								200	○		20,7							
	PEAT mixed with sand and silt, a few gravel grains																		
	Sandy, silty, organic MATERIAL a few gravel grains, a few shell fragments			OG				○				3,5							
	Sandy, organic SILT a few gravel grains																		
10	Sandy, organic SILT a few gravel grains			G					○			4,7							
15																			
20																			

Symbols:

Unconfined compression test (line specifies strain (%) at failure)

○ Water content
 Plasticity Index (PI)

ISO 17892-6: 2017
 ▼ Disturbed fall cone
 ▽ Undisturbed fall cone

ρ = Density
 ρ_s = Grain density

T = Triaxial test
 O = Oedometer test
 G = Grain size distribution

Ground water level: m
 Bore book: Digital

Soil Sampling

Borehole: 5001

Nye Veier

Date: 2020-07-09

E18 Langangen-Rugtvedt, supplementary ground investigations

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Drawn by:
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Project number:
 10217934-02

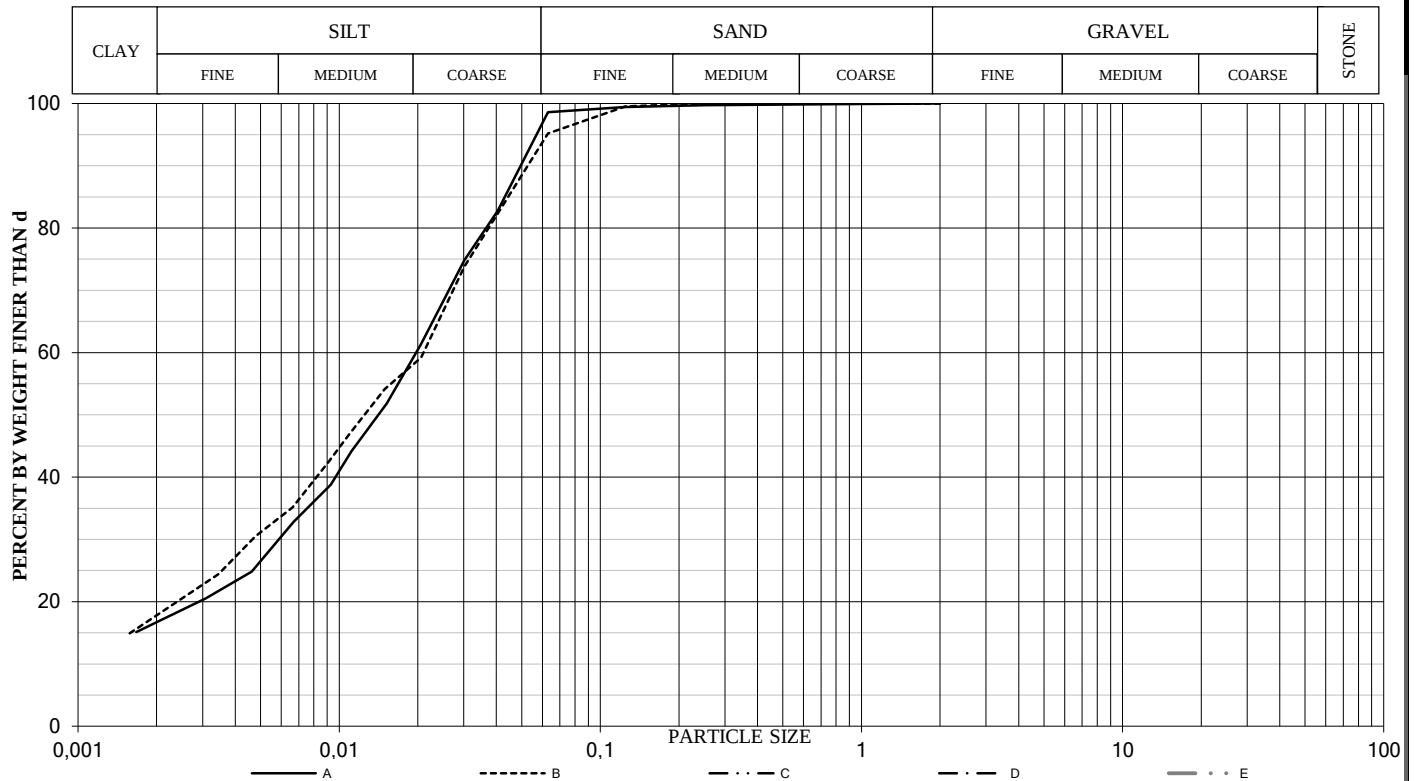
Reviewed by:
 ANNM

Drawing number:
 RIG-TEG-203

Approved by:
 STEG

Revision number:
 00

SERIES	BOREHOLE ID	DEPTH (m)	SOIL CLASSIFICATION	REMARKS	METHOD		
					DS	WS	HYD
A	2007	4,2-5,0	Silty CLAY			X	X
B	3002	4,2-5,0	Silty CLAY			X	X
C							
D							
E							



ABBREVIATIONS:

MC = Moisture content

FS = Frost susceptibility

$$C_z = \frac{D_{30}^2}{(D_{60})(D_{10})}$$

$$C_u = \frac{D_{60}}{D_{10}}$$

METHOD

DS = Dry Sieving

WS = Wet Sieving

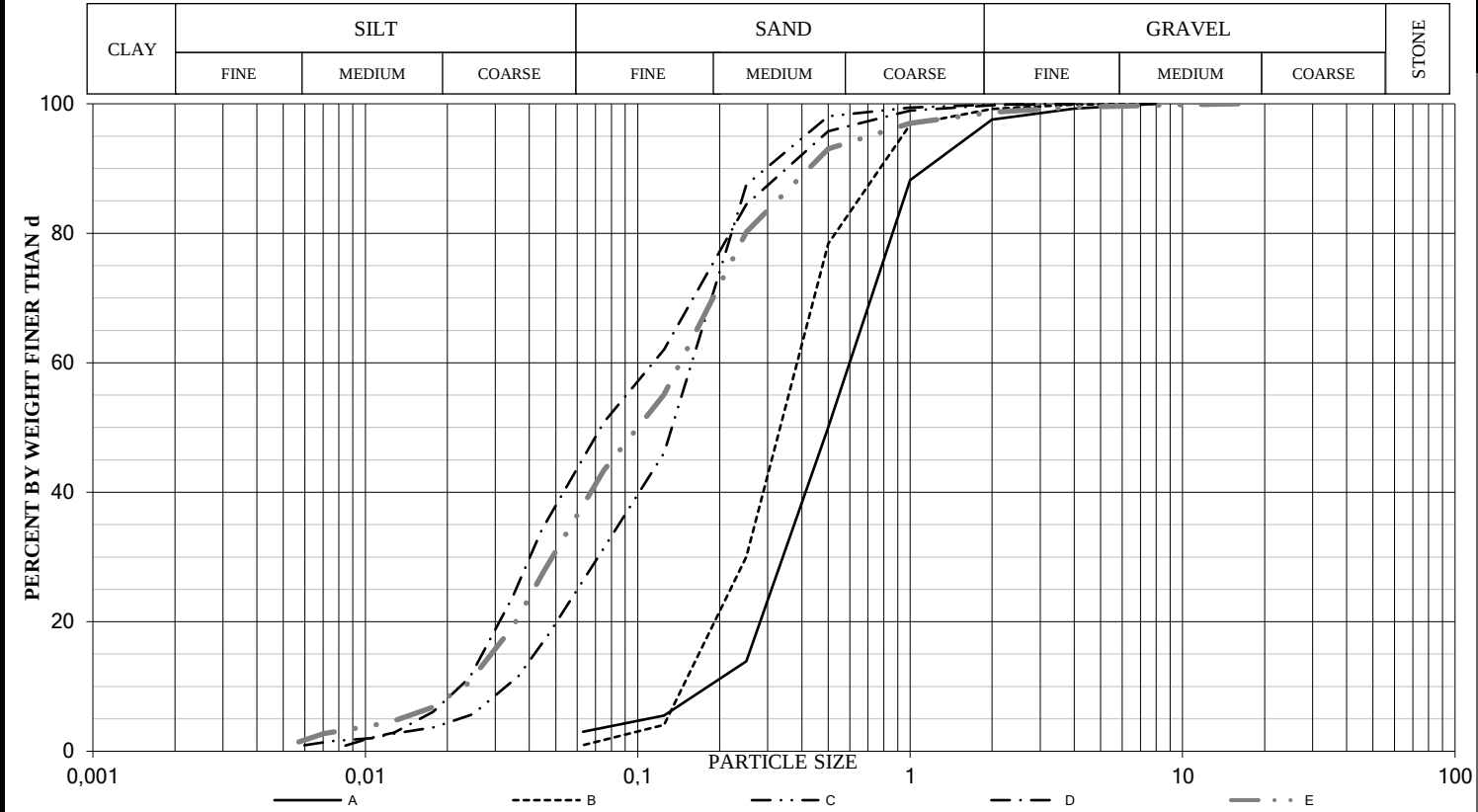
HYD = Hydrometer

SERIES	FS Group	MC %	C_u kN/m ²	C_{ur} kN/m ²	Plastic limit %	Plasticity index %	Organic Content %	< 0,02 mm %	Bulk density (g/m ³)	D_{10} mm	D_{30} mm	D_{50} mm	D_{60} mm
A											0,0060	0,0143	0,0198
B											0,0047	0,0127	0,0211
C													
D													
E													

GRAIN SIZE DISTRIBUTION

Nye Veier E18 Langangen-Rugtvedt, supplementary ground investigations			Prepared by: GEO	Reviewed by: ANNM
			Approved by: STEG	Date: 07.07.20
Multiconsult www.multiconsult.no		Project ID: 10217934-02	Drawing ID: RIG-TEG-300	Rev. 00

SERIES	BOREHOLE ID	DEPTH (m)	SOIL CLASSIFICATION	REMARKS	METHOD		
					DS	WS	HYD
A	4003	1,0-2,0	SAND		X		
B	4003	3,0-4,0	SAND		X		
C	4003	5,0-6,0	Silty SAND			X	X
D	4003	7,0-8,0	Sandy, silty MATERIAL			X	X
E	4003	9,0-10,0	Silty SAND			X	X



ABBREVIATIONS:

MC = Moisture content
FS = Frost susceptibility

$$C_z = \frac{D^2_{30}}{(D_{60})(D_{10})}$$

$$C_u = \frac{D_{60}}{D_{10}}$$

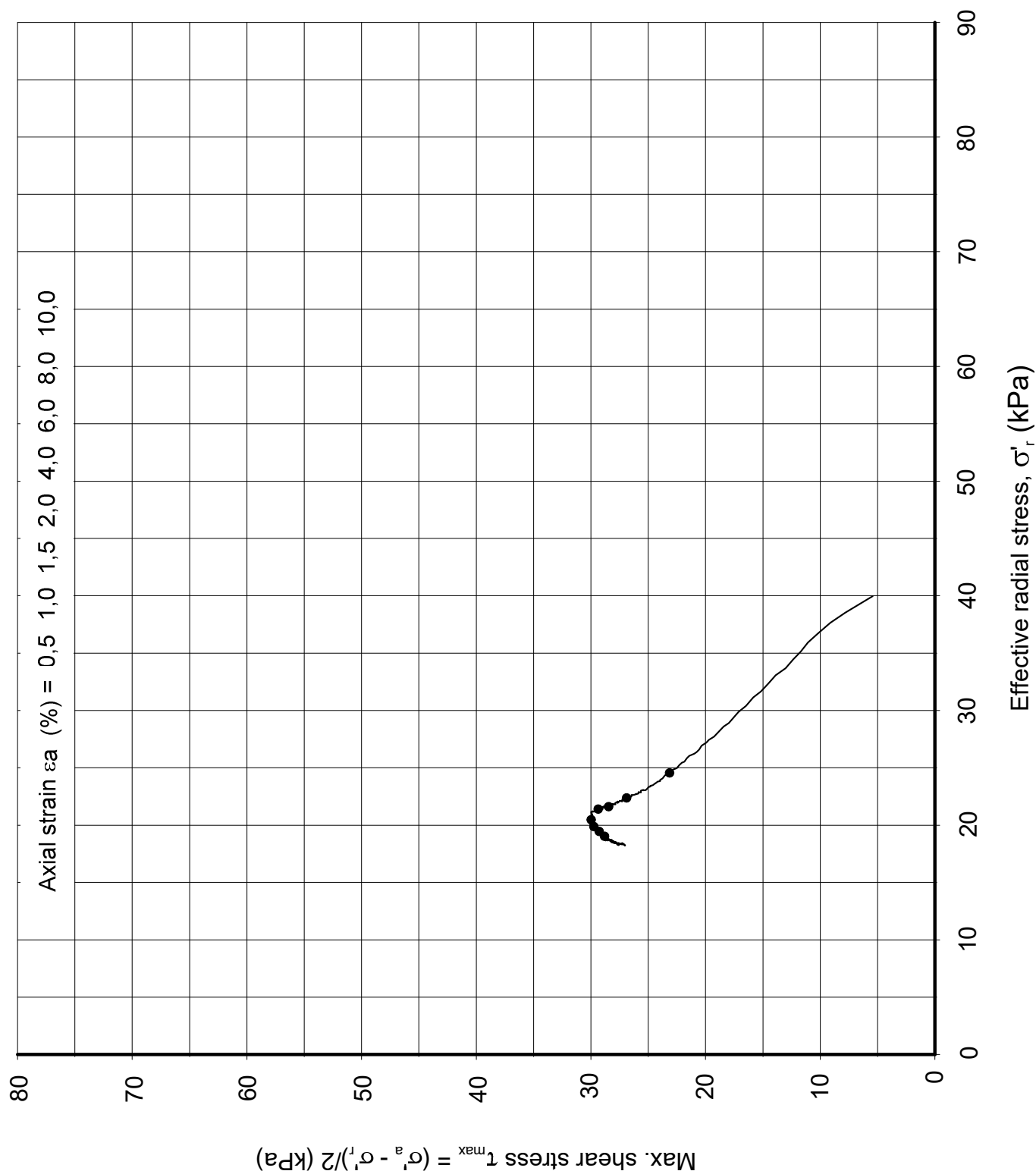
METHOD

DS = Dry Sieving
WS = Wet Sieving
HYD = Hydrometer

SERIES	FS Group	MC %	C _u kN/m ²	C _{ur} kN/m ²	Plastic limit %	Plasticity index %	Organic Content %	< 0,02 mm %	Bulk density (g/m ³)	D ₁₀ mm	D ₃₀ mm	D ₅₀ mm	D ₆₀ mm
A										0,1921	0,3616	0,5000	0,6308
B										0,1535	0,2498	0,3532	0,4049
C										0,0333	0,0721	0,1368	0,1670
D										0,0225	0,0405	0,0735	0,1158
E										0,0231	0,0494	0,1032	0,1493

GRAIN SIZE DISTRIBUTION

Nye Veier E18 Langangen-Rugtvedt, supplementary ground investigations	Prepared by: GEO	Reviewed by: ANNM
	Approved by: STEG	Date: 10.07.20
Project ID: 10217934-02		Drawing ID: RIG-TEG-301
Rev. 00		

**Test data**

Depth. 3,50 m
GWT = 2 m

$\gamma_i = 19,4 \text{ kN/m}^3$
 $\epsilon_{vol} = \Delta V/V = 2,54 \%$

$w_i = 27,8 \%$
 $w_f = - \%$
 $w_p = - \%$

$\tan \phi_f = -$
Attraction = - kPa

$\sigma'_{vo} = 53,4 \text{ kPa}$
 $\sigma'_{ac} = 53,5 \text{ kPa}$
 $\sigma'_{rc} = 42,7 \text{ kPa}$

Triaxial test CAUa Deviator stress path - NTNU-plot

Boring no.
3002

Nye Veier

Date
03.07.2020

E18 Langangen-Rugtvedt, supplementary ground investigations

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Drawn.

RHS

Checked.

ANNM

Approved

STEG

Job no.

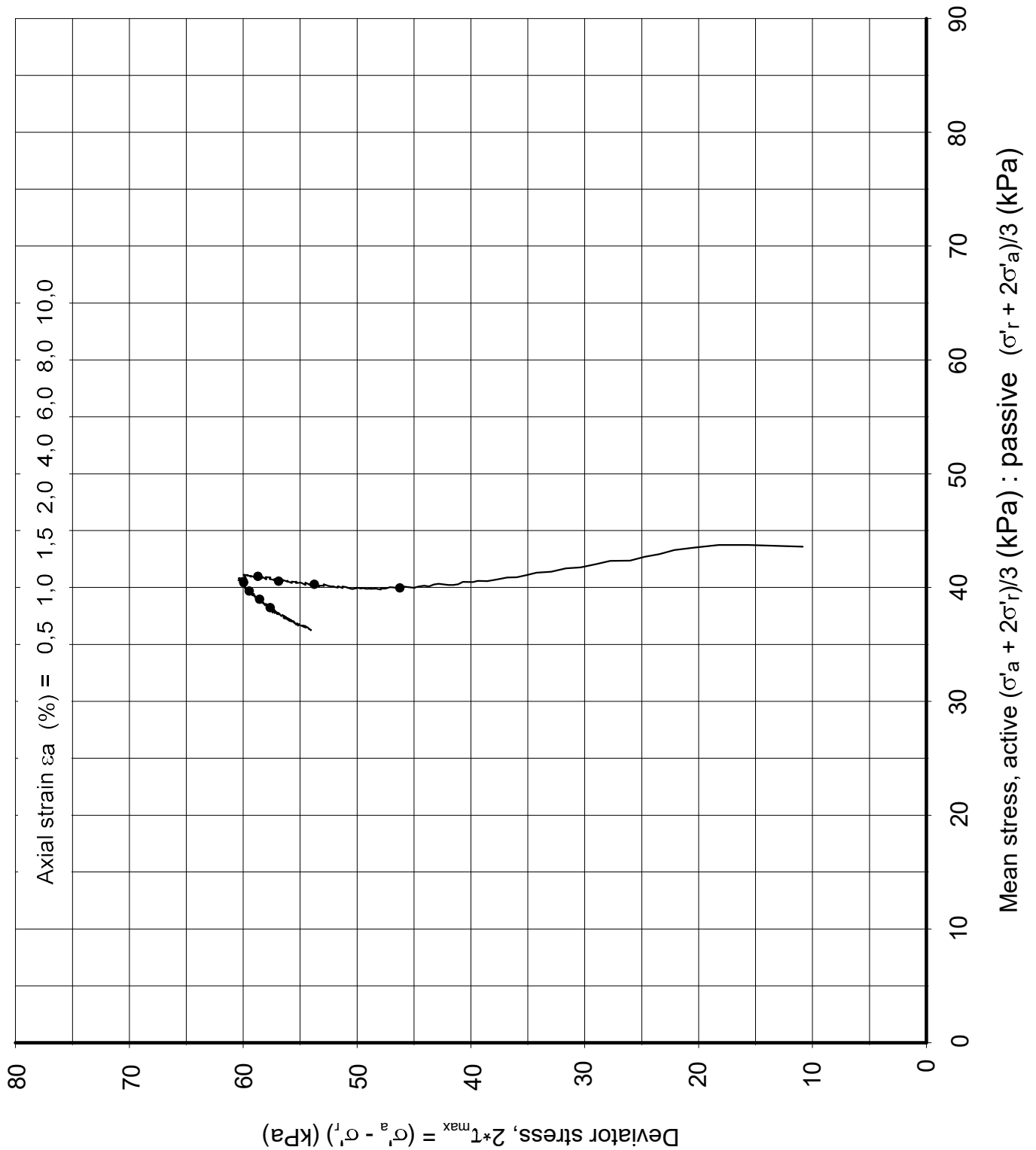
10217934-02

Dwg. no.

RIG-TEG-452.1

Rev

00

**Test data**

	$\gamma_i = 19,4 \text{ kN/m}^3$	$w_i = 27,8 \%$	$\sigma'_{vo} = 53,4 \text{ kPa}$
Depth. 3,50 m	$\varepsilon_{vol} = 2,54 \%$	$w_f = - \%$	$\sigma'_{ac} = 53,5 \text{ kPa}$
GWT = 2,0 m	$\Delta e/e_0 (-) = 0,058$	$w_p = - \%$	$\sigma'_{rc} = 42,7 \text{ kPa}$

Triaxial test CAUa

Bore hole:

3002

Nye Veier

Date.
03.07.2020

E18 Langangen-Rugtvedt, supplementary ground investigations

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Drawn by:

RHS

Checked by:

ANNM

Approved by:

STEG

Job no.:

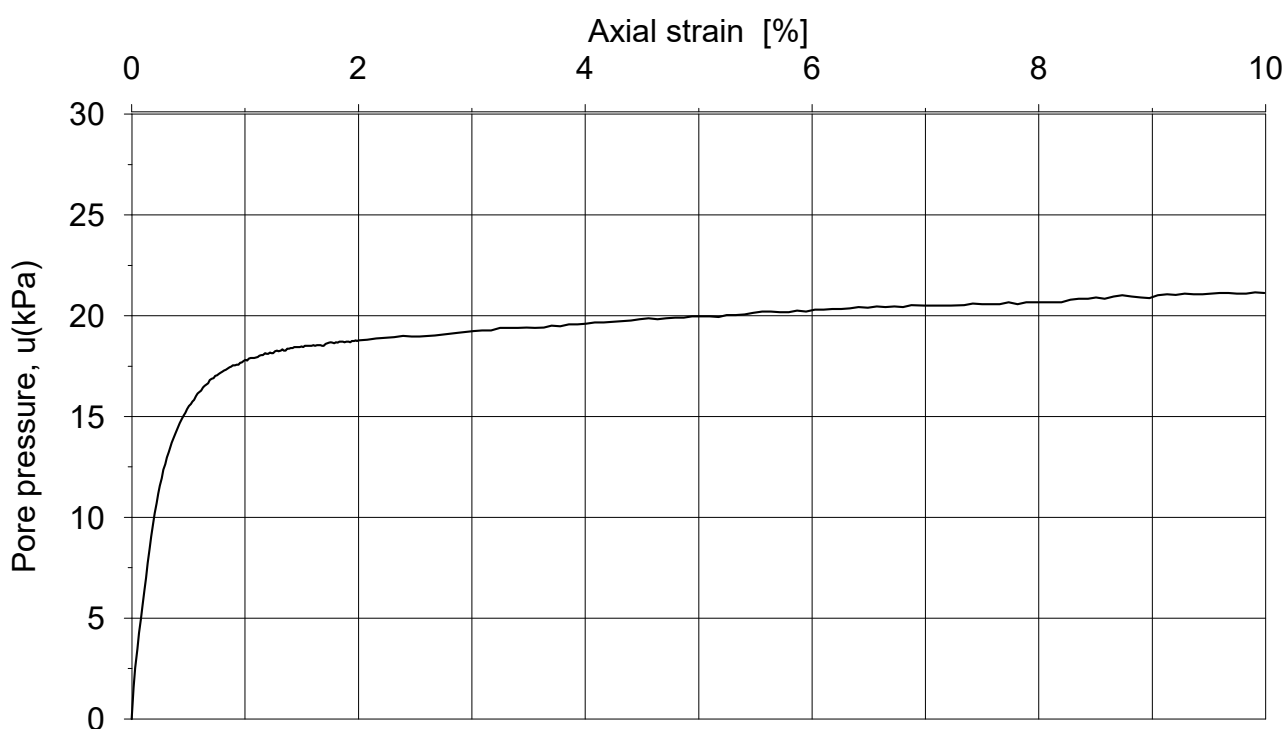
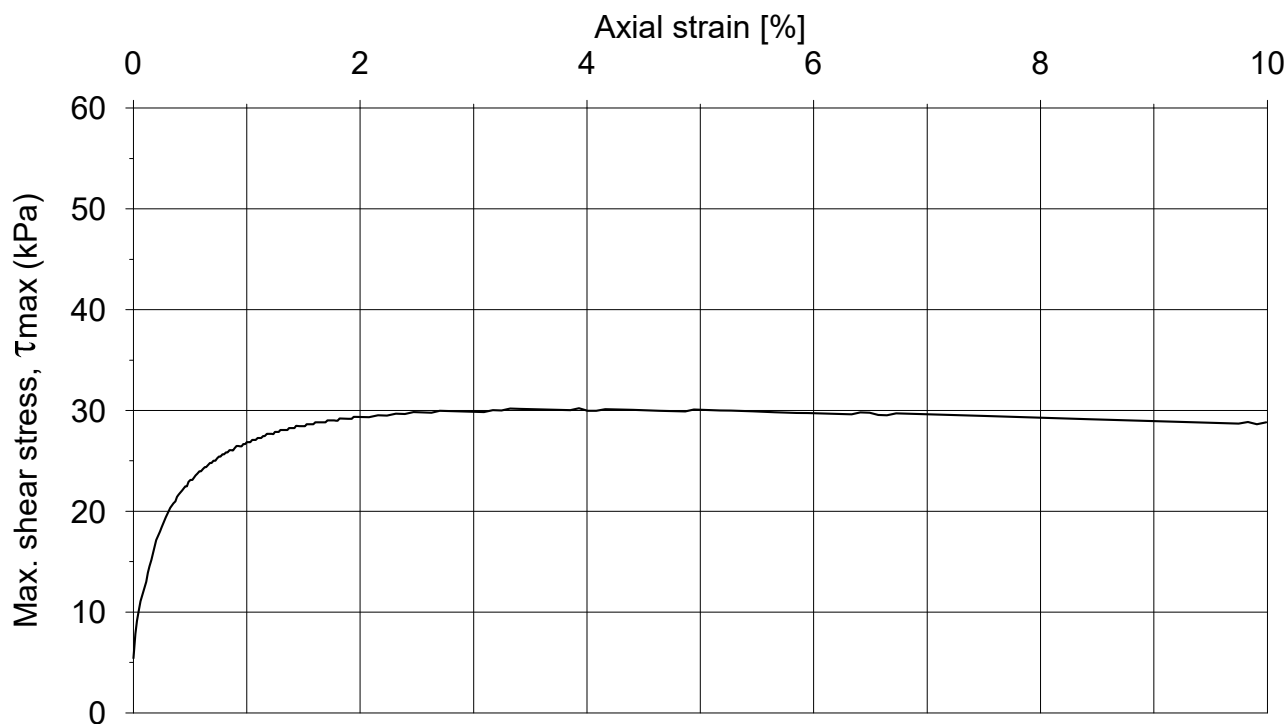
10217934-02

DWG.no.:

RIG-TEG-452.2

Rev.no.:

00

**Test data**

	$\gamma_i = 19,4 \text{ kN/m}^3$	$w_i = 27,8 \%$	$\sigma'_{vo} = 53,4 \text{ kPa}$
Depth 3,50 m	$\varepsilon_{vol} = \Delta V/V = 2,54 \%$	$w_f = - \%$	$\sigma'_{ac} = 53,5 \text{ kPa}$
GWT= 2 m	$\Delta e/e_0 (-) = 0,058$	$w_p = - \%$	$\sigma'_{rc} = 42,7 \text{ kPa}$

Triaxial test CAUa Pore- and max.shear stress

Boring no.

3002

Nye Veier

Date

03.07.2020

E18 Langangen-Rugtvedt, supplementary ground investigations

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Drawn

RHS

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ANNM

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Job no.

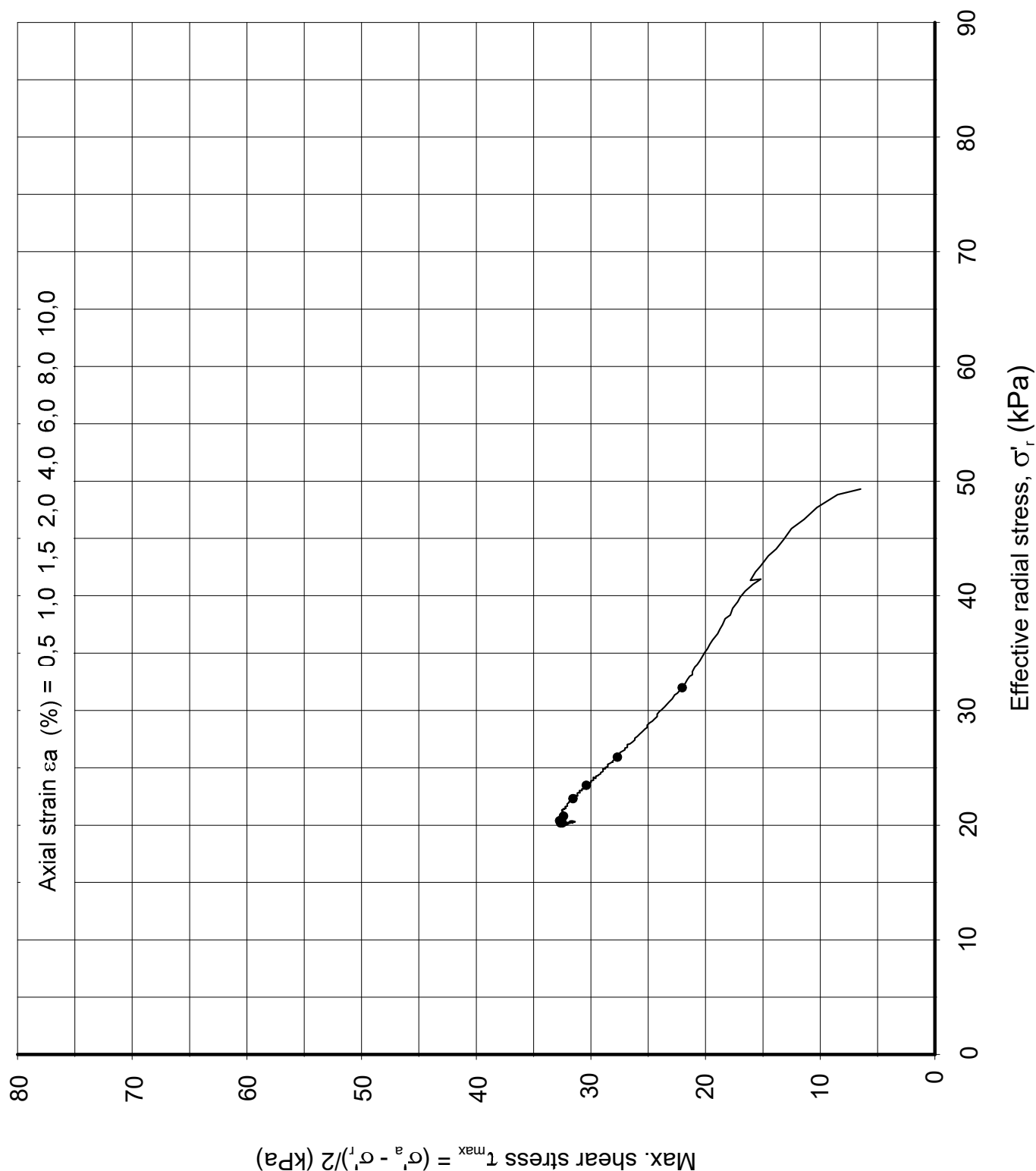
10217934-02

Dwg.no.

RIG-TEG-452.3

Rev.

00

**Test data**

Depth. 4,70 m
GWT = 2 m

$\gamma_i = 19,8 \text{ kN/m}^3$
 $\varepsilon_{\text{vol}} = \Delta V/V = 3,67 \%$

$w_i = 27,6 \%$
 $w_f = - \%$
 $w_p = - \%$

$\tan \phi_f = -$
Attraction = - kPa

$\sigma'_{\text{vo}} = 66,2 \text{ kPa}$
 $\sigma'_{\text{ac}} = 64,9 \text{ kPa}$
 $\sigma'_{\text{rc}} = 51,9 \text{ kPa}$

Triaxial test CAUa Deviator stress path - NTNU-plot

Boring no.
3002

Nye Veier

E18 Langangen-Rugtvedt, supplementary ground investigations

Date
03.07.2020

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Drawn.

RHS

Job no.

10217934-02

Checked.

ANNM

Dwg. no.

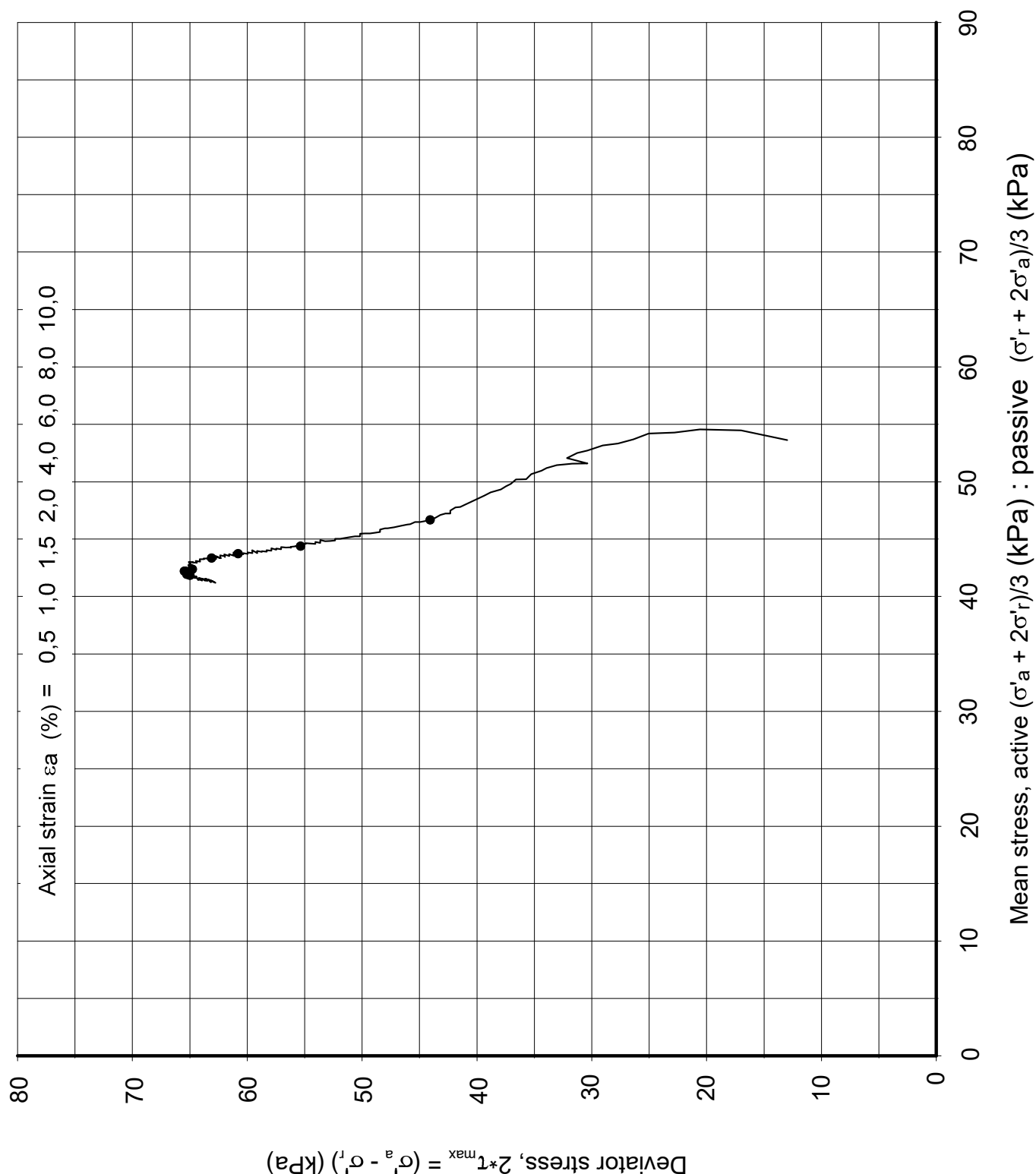
RIG-TEG-453.1

Approved

STEG

Rev

00

**Test data**

	$\gamma_i = 19,8 \text{ kN/m}^3$	$w_i = 27,6 \%$	$\sigma'_{vo} = 66,2 \text{ kPa}$
Depth. 4,70 m	$\varepsilon_{vol} = 3,67 \%$	$w_f = - \%$	$\sigma'_{ac} = 64,9 \text{ kPa}$
GWT = 2 m	$\Delta e/e_0 (-) = 0,083$	$w_p = - \%$	$\sigma'_{rc} = 51,9 \text{ kPa}$
		$\tan. \phi_f = -$	
		Attraction = - kPa	

Triaxial test CAUa

Bore hole:

3002

Nye Veier

Date.
03.07.2020

E18 Langangen-Rugtvedt, supplementary ground investigations

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Drawn by:

RHS

Checked by:

ANNM

Approved by:

STEG

Job no.:

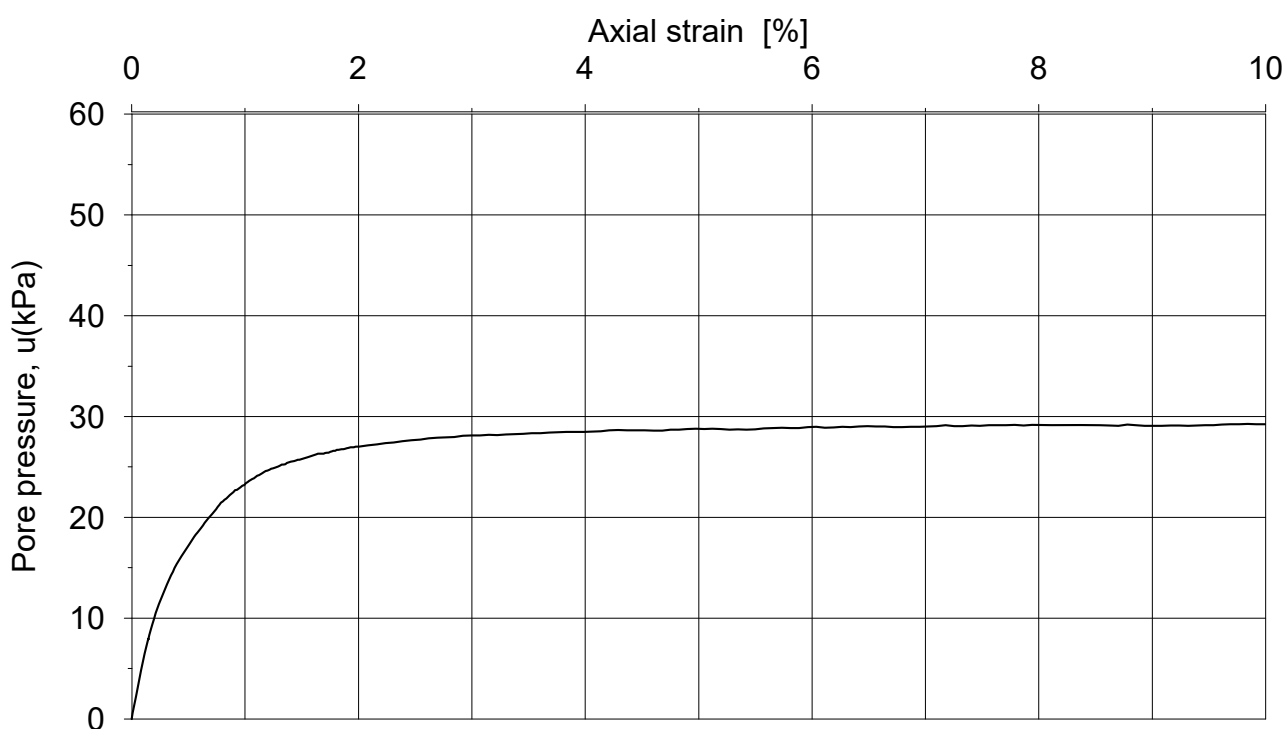
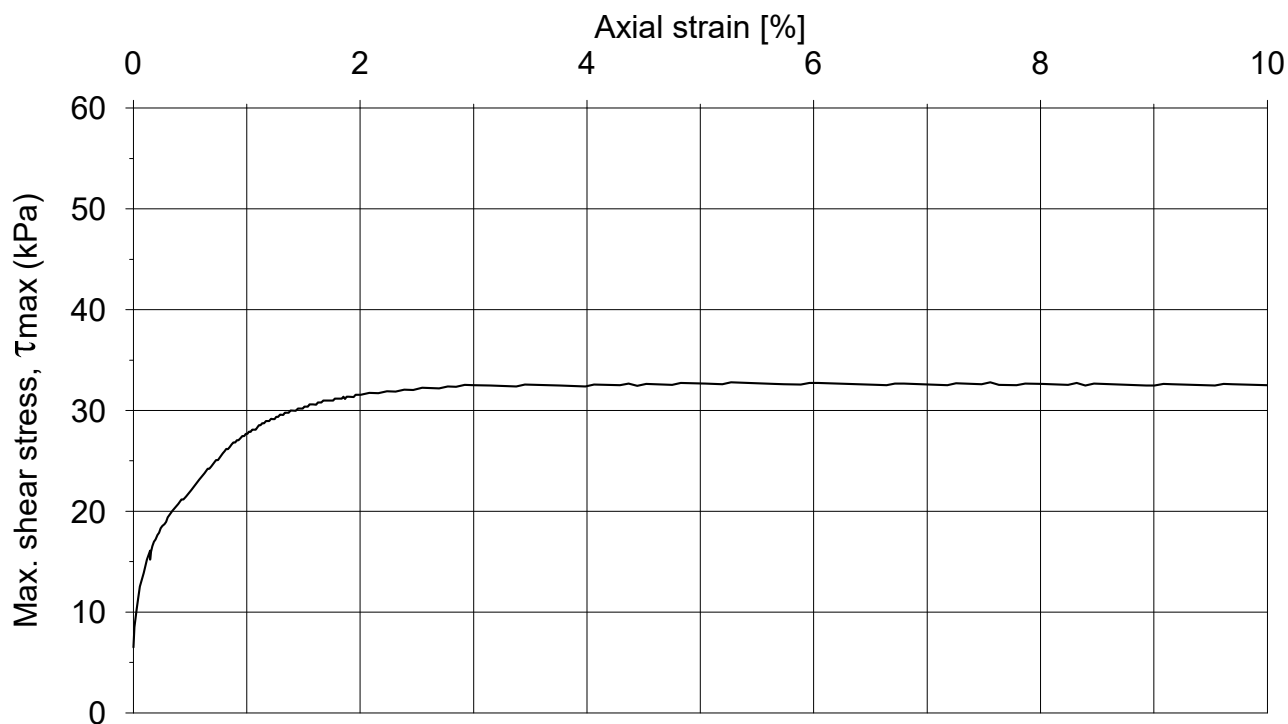
10217934-02

DWG.no.:

RIG-TEG-453.2

Rev.no.:

00

**Test data**

	$\gamma_i = 19,8 \text{ kN/m}^3$	$w_i = 27,6 \%$	$\sigma'_{vo} = 66,2 \text{ kPa}$
Depth 4,70 m	$\varepsilon_{vol} = \Delta V/V = 3,67 \%$	$w_f = - \%$	$\sigma'_{ac} = 64,9 \text{ kPa}$
GWT= 2 m	$\Delta e/e_0 (-) = 0,083$	$w_p = - \%$	$\sigma'_{rc} = 51,9 \text{ kPa}$

Triaxial test CAUa Pore- and max.shear stress

Boring no.

3002

Nye Veier

Date

03.07.2020

E18 Langangen-Rugtvedt, supplementary ground investigations

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Drawn

RHS

Checked

ANNM

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STEG

Job no.

10217934-02

Dwg.no.

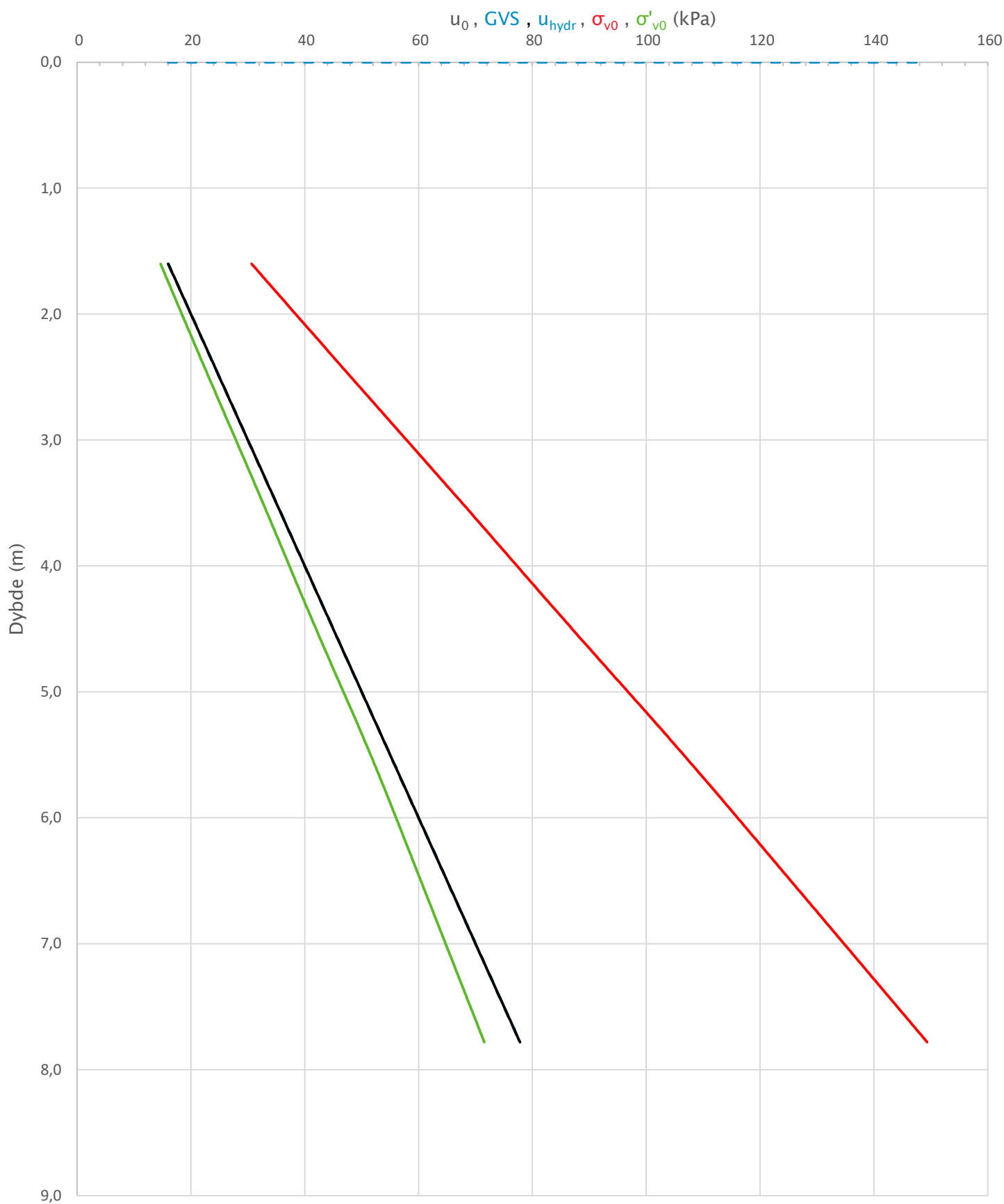
RIG-TEG-453.3

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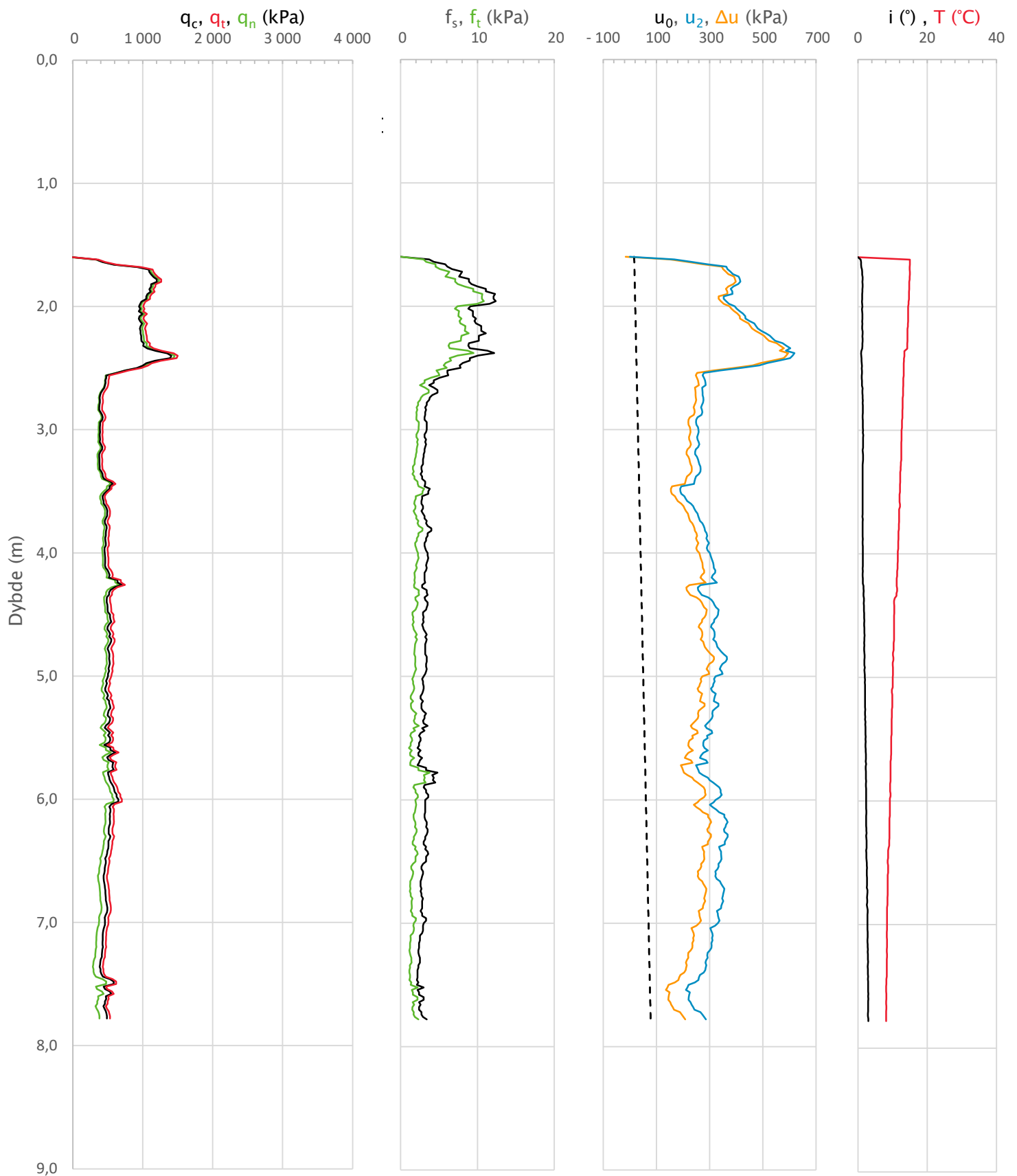
Sonde og utførelse						
Sondennummer	4704		Boreleder		Sigmund	
Type sonde	Nova		Temperaturendring (°C)		15	
Kalibreringsdato	24-01-2020		Maks helning (°)		3,0	
Dato sondering	20-06-22		Maks avstand målinger (m)		0,02	
Filtertype						
Kalibreringsdata						
	Spissmotstand		Sidefriksjon		Poretrykk	
Maksimal last (MPa)	50		0,5		2	
Måleområde (MPa)	50		0,5		2	
Skaleringsfaktor	1289		3702		3559	
Oppløsning 2 ¹² bit (kPa)	-		-		-	
Oppløsning 2 ¹⁸ bit (kPa)	0,5919		0,0103		0,0214	
Arealforhold	0,8480		0,0020			
Maks ubelastet temp. effekt (kPa)	18,929		0,453		0,857	
Temperaturområde (°C)	40					
Nullpunktskontroll						
	NA		NA		NA	
Registrert før sondering (kPa)	7210,3		128,3		260,1	
Registrert etter sondering (kPa)	0,0		-0,8		-4,1	
Avvik under sondering (kPa)	0,0		0,8		4,1	
Maksimal temperatureffekt (kPa)	7,1		0,2		0,3	
Maksverdi under sondering (kPa)	1408,5		12,4		619,1	
Vurdering av anvendelsesklasse ihht. ISO 22476-1:2012						
	Spissmotstand		Sidefriksjon		Poretrykk	
	(kPa)	(%)	(kPa)	(%)	(kPa)	(%)
Samlet nøyaktighet (kPa)	7,7	0,5	1,0	7,9	4,4	0,7
Tillatt nøyaktighet klasse 1	35	5	5	10	10	2
Tillatt nøyaktighet klasse 2	100	5	15	15	25	3
Tillatt nøyaktighet klasse 3	200	5	25	15	50	5
Tillatt nøyaktighet klasse 4	500	5	50	20		
Anvendelsesklasse	1	1	1	1	1	1
Anvendelsesklasse måleintervall	1					
Anvendelsesklasse	1					
Måleverdier under kapasitet/krav						
Spissmotstand	Sidefriksjon		Poretrykk		Helning	
OK	OK		OK		OK	
Kommentarer:						
Prosjekt			Prosjektnummer: 10217934 Rapportnummer: -1		Borhull	
E18 Langangen-Rugtvedt					3002	
Innhold					Sondennummer	
Dokumentasjon av utstyr og målenøyaktighet					4704	
Multiconsult	Tegnet	Kontrollert	Godkjent		Anvend.klasse	
	HalE	MRL	SteG		1	
	Utførende	Dato sondering	Revisjon		RIG-TEG	
	Multiconsult	20-06-22	0		501.1	
			Rev. dato 20.07.2020			

Ground investigations field and lab profiles P2-G11 s156(172)



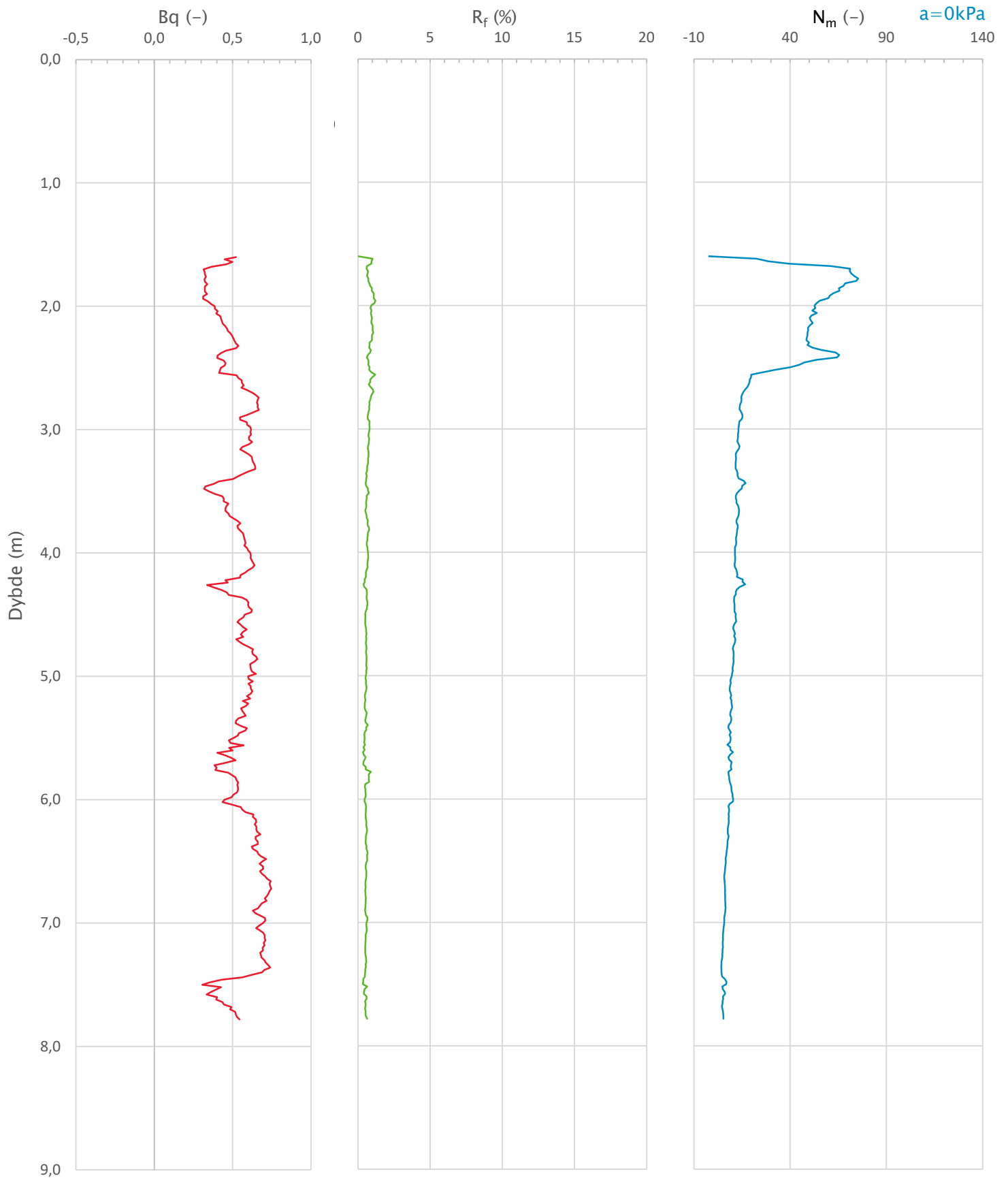
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E18 Langangen-Rugtvedt						3002	
Innhold						Sondennummer	
In-situ poretrykk, total- og effektiv vertikalspenning i beregninger						4704	
Multiconsult	Tegnet	Kontrollert	Godkjent	Anvend.klasse		1	
	HalE	MRL	SteG				
	Utførende	Dato sondering	Revisjon	RIG-TEG		501.2	
	Multiconsult	20-06-22	0				
			Rev. dato	20.07.2020			

Ground investigations field and lab profiles P2-G11 s157(172)



Prosjekt		Prosjektnummer: 10217934 Rapportnummer: -1		Borhull
E18 Langangen-Rugtvedt				3002
Innhold				Sondennummer
Måledata og korrigerte måleverdier				4704
Multiconsult	Tegnet	Kontrollert	Godkjent	Anvend.klasse
	HaE	MRL	SteG	1
Multiconsult	Utførende	Dato sondering	Revisjon	RIG-TEG
	Multiconsult	20-06-22	0 Rev. dato 20.07.2020	
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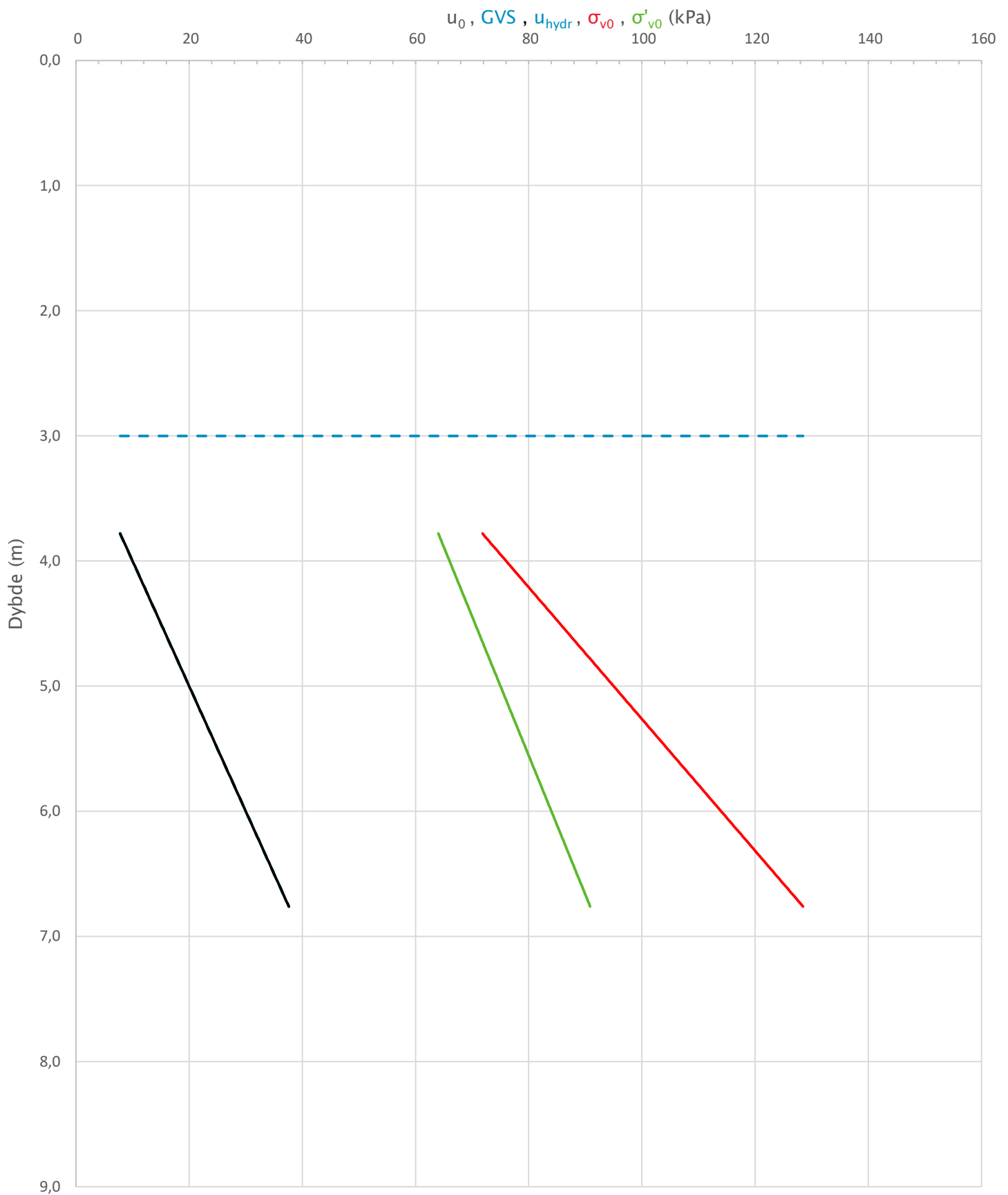
Ground investigations field and lab profiles P2-G11 s158(172)



Prosjekt		Prosjektnummer: 10217934 Rapportnummer: -1		Borhull
E18 Langangen-Rugtvedt				3002
Innhold				Sondennummer
Avledede dimensjonsløse forhold				4704
Multiconsult	Tegnet	Kontrollert	Godkjent	Anvend.klasse
	HaE	MRL	SteG	1
Multiconsult	Utførende	Dato sondering	Revisjon	RIG-TEG
	Multiconsult	20-06-22	0 Rev. dato 20.07.2020	
				501.4

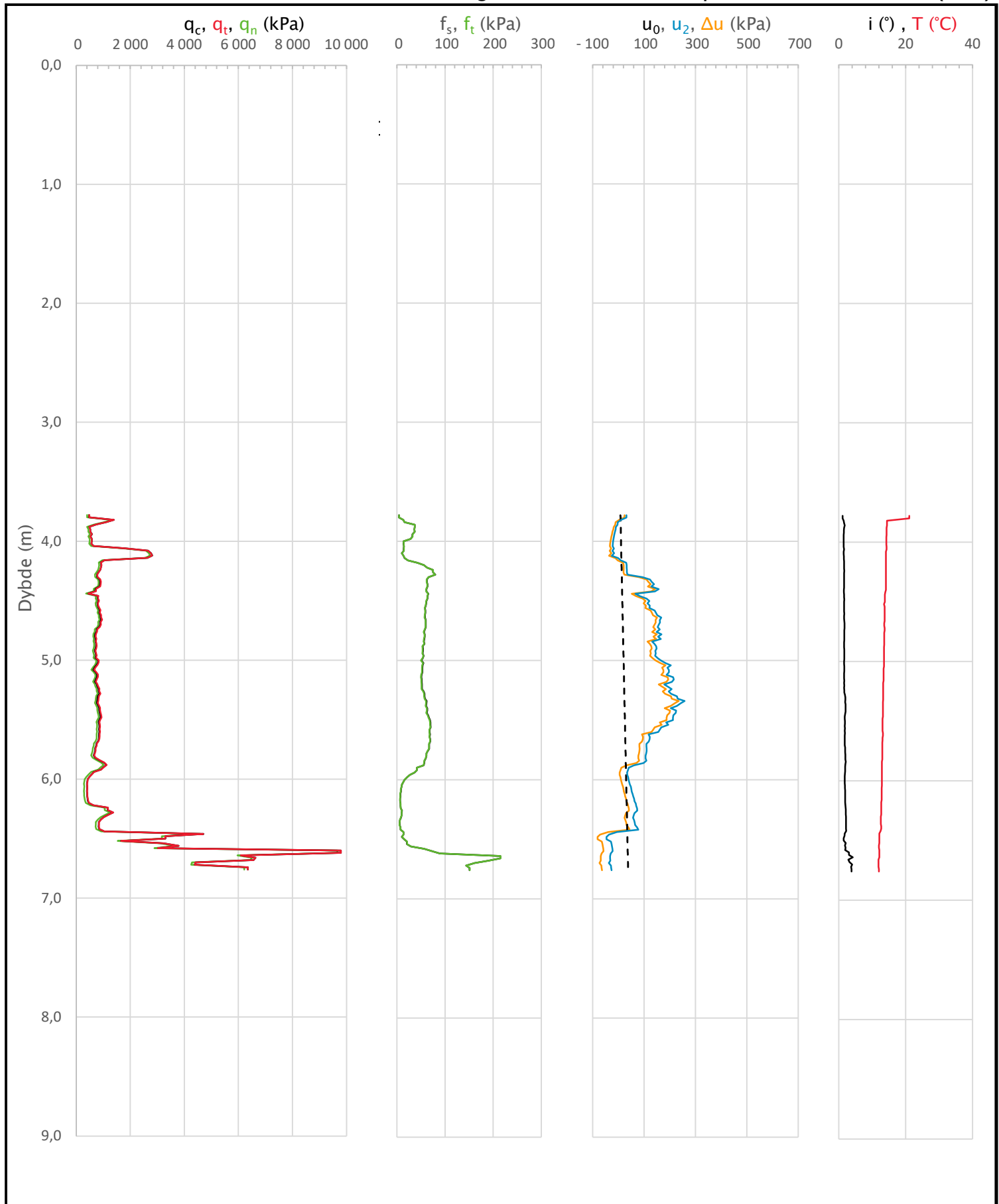
Sonde og utførelse						
Sondennummer	4704		Boreleder		Sigmund	
Type sonde	Nova		Temperaturendring (°C)		9,2	
Kalibreringsdato	24-01-2020		Maks helning (°)		4,2	
Dato sondering	20-06-30		Maks avstand målinger (m)		0,02	
Filtertype						
Kalibreringsdata						
	Spissmotstand		Sidefriksjon		Poretrykk	
Maksimal last (MPa)	50		0,5		2	
Måleområde (MPa)	50		0,5		2	
Skaleringsfaktor	1289		3702		3559	
Oppløsning 2 ¹² bit (kPa)	-		-		-	
Oppløsning 2 ¹⁸ bit (kPa)	0,5919		0,0103		0,0214	
Arealforhold	0,8480		0,0020			
Maks ubelastet temp. effekt (kPa)	18,929		0,453		0,857	
Temperaturområde (°C)	40					
Nullpunktskontroll						
	NA		NA		NA	
Registrert før sondering (kPa)	7177,8		129,7		257,9	
Registrert etter sondering (kPa)	-0,6		-2,1		-14,7	
Avvik under sondering (kPa)	0,6		2,1		14,7	
Maksimal temperatureffekt (kPa)	4,4		0,1		0,2	
Maksverdi under sondering (kPa)	9792,4		215,0		258,4	
Vurdering av anvendelsesklasse ihht. ISO 22476-1:2012						
	Spissmotstand		Sidefriksjon		Poretrykk	
	(kPa)	(%)	(kPa)	(%)	(kPa)	(%)
Samlet nøyaktighet (kPa)	5,5	0,1	2,2	1,0	14,9	5,8
Tillatt nøyaktighet klasse 1	35	5	5	10	10	2
Tillatt nøyaktighet klasse 2	100	5	15	15	25	3
Tillatt nøyaktighet klasse 3	200	5	25	15	50	5
Tillatt nøyaktighet klasse 4	500	5	50	20		
Anvendelsesklasse	1	1	1	1	2	OBS
Anvendelsesklasse måleintervall	1					
Anvendelsesklasse	2					
Måleverdier under kapasitet/krav						
Spissmotstand	Sidefriksjon		Poretrykk		Helning	
OK	OK		OK		OK	
Kommentarer:						
Prosjekt		Prosjektnummer: 10217934 Rapportnummer: -1			Borhull	
E18 Langangen-Rugtvedt					5001	
Innhold					Sondennummer	
Dokumentasjon av utstyr og målenøyaktighet					4704	
Multiconsult	Tegnet	Kontrollert	Godkjent		Anvend.klasse	
	HalE	MRL	SteG		2	
	Utførende	Dato sondering	Revisjon		RIG-TEG	
	Multiconsult	20-06-30	0 Rev. dato 20.07.2020		502.1	

Ground investigations field and lab profiles P2-G11 s160(172)



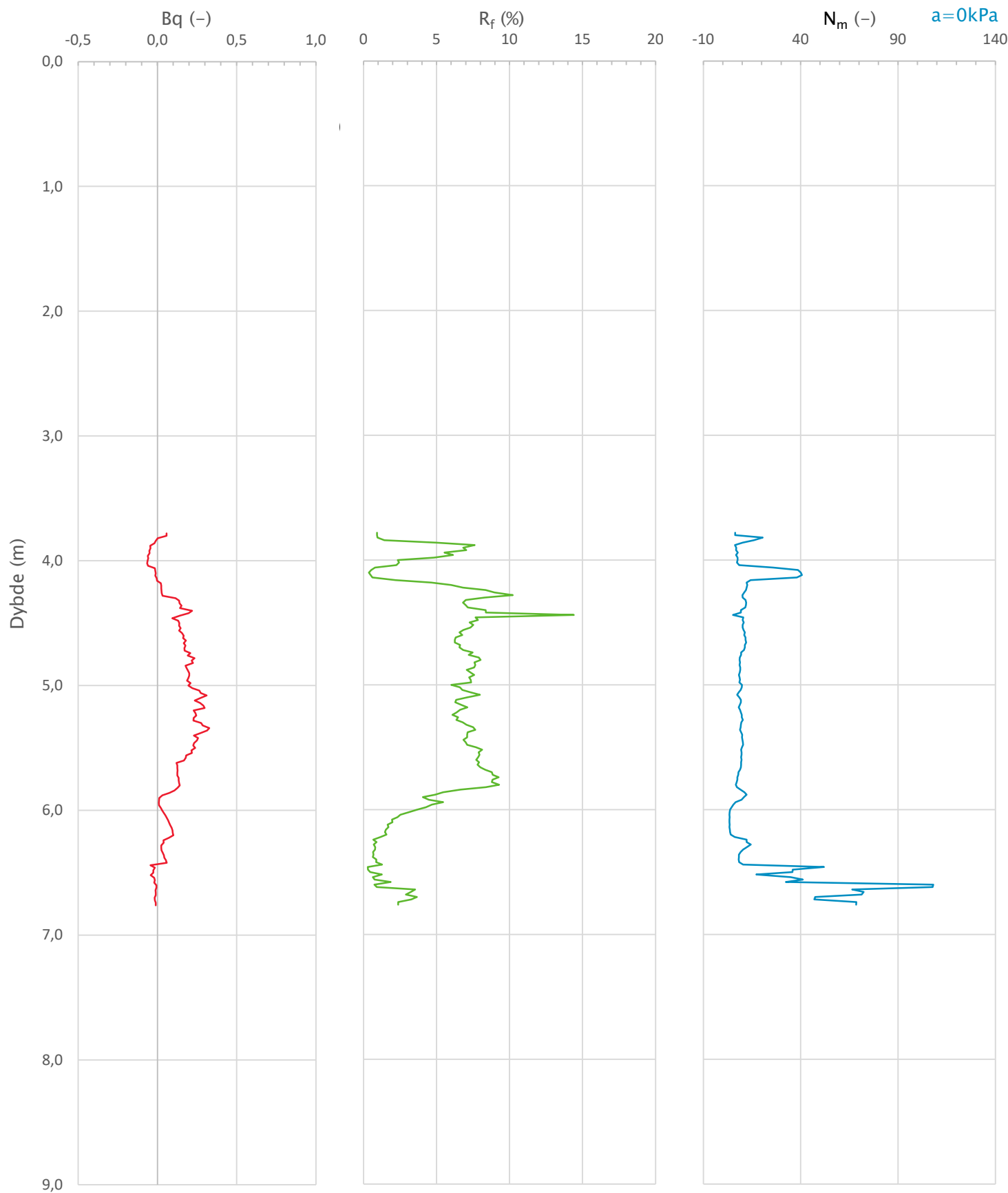
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E18 Langangen–Rugtvedt						5001	
Innhold						Sondennummer	
In-situ poretrykk, total- og effektiv vertikalspenning i beregninger						4704	
Multiconsult	Tegnet	Kontrollert	Godkjent		Anvend.klasse		2
	Hale	MRL	SteG				
	Utførende	Dato sondering	Revisjon	0	RIG-TEG		502.2
Multiconsult	20-06-30	Rev. dato	20.07.2020				

Ground investigations field and lab profiles P2-G11 s161(172)



Prosjekt		Prosjektnummer: 10217934 Rapportnummer: -1		Borhull
E18 Langangen-Rugtvedt				5001
Innhold				Sondennummer
Måledata og korrigerte måleverdier				4704
Multiconsult	Tegnet	Kontrollert	Godkjent	Anvend.klasse
	HaE	MRL	SteG	2
Multiconsult	Utførende	Dato sondering	Revisjon	RIG-TEG
	Multiconsult	20-06-30	0 20.07.2020	
				502.3

Ground investigations field and lab profiles P2-G11 s162(172)



Prosjekt		Prosjektnummer: 10217934 Rapportnummer: -1		Borhull
E18 Langangen-Rugtvedt				5001
Innhold				Sondennummer
Avledede dimensjonsløse forhold				4704
Multiconsult	Tegnet	Kontrollert	Godkjent	Anvend.klasse
	HaE	MRL	SteG	2
Multiconsult	Utførende	Dato sondering	Revisjon	RIG-TEG
	Multiconsult	20-06-30	0 Rev. dato 20.07.2020	
				502.4

CALIBRATION CERTIFICATE FOR CPT PROBE 4704

Probe No 4704
 Date of Calibration 2020-01-24
 Calibrated by Mikael Engdahl.....
 Run No 1276
 Test Class: ISO 1

Point Resistance		Tip Area 10cm ²
Maximum Load	50	MPa
Range	50	MPa
Scaling Factor	1289	
Resolution	0,5919	kPa
Area factor (a)	0,848	

ERRORS

Max. Temperature effect when not loaded 18,929 kPa
 Temperature range 5 –40 deg. Celsius.

Local Friction		Sleeve Area 150cm ²
Maximum Load	0,5	MPa
Range	0,5	MPa
Scaling Factor	3702	
Resolution	0,0103	kPa
Area factor (b)	0,002	

ERRORS

Max. Temperature effect when not loaded 0,453 kPa
 Temperature range 5 –40 deg. Celsius.

Pore Pressure		
Maximum Load	2	MPa
Range	2	MPa
Scaling Factor	3559	
Resolution	0,0214	kPa

ERRORS

Max. Temperature effect when not loaded 0,857 kPa
 Temperature range 5 –40 deg. Celsius.

Tilt Angle.	Scaling Factor: 0,92	
Range	0 - 40	Deg.

Backup memory
Temperature sensor



Specialists in
 Geotechnical
 Field Equipment

Cptlog Cone data base information

Göteborg: 2020-01-24

Cone name	4704	Serial number	4704	Date of purchase	
Ranges		Geometric parameters		Scaling factors	
Point resistance	50 (Mpa)	Area factor a	0,848	Point resistance	1289
Local friction	0,5 (Mpa)	Area factor b	0,002	Local friction	3702
Pore pressure	2 (Mpa)	Tip area	10 (cm ²)	Pore pressure	3559
Tilt sensor	40 (Deg)	Sleeve area	150 (cm ²)	Tilt sensor	0,92
temperature	°C			temperature	1
Elect. Conductivity	(mS/m)			Elect. Conductivity A	
				Elect. Conductivity B	
				Type	NOVA cone
				Memory option	With memory



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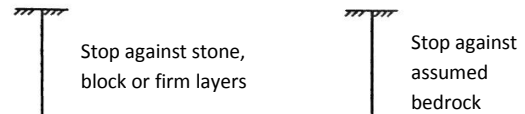
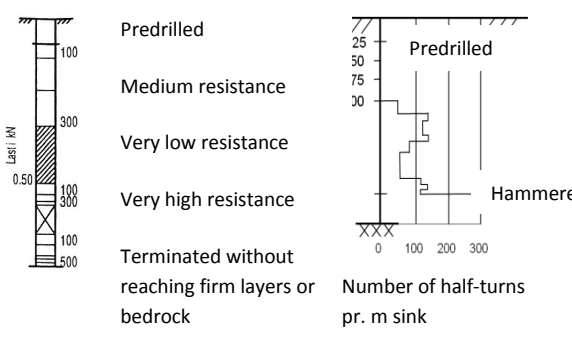
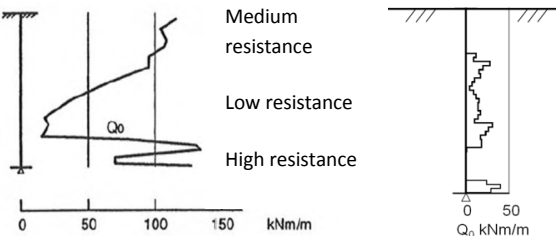
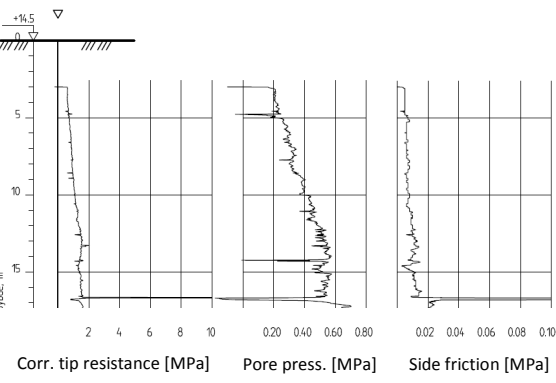
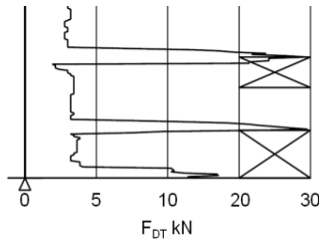
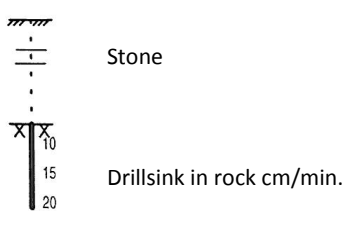
Ingenjörfirman Geotech AB +46 (0)31-28 99 20 www.geotech.se
Datavägen 53 +46 (0)31-68 16 39 VAT No.



Geotechnical enclosures

Field investigations

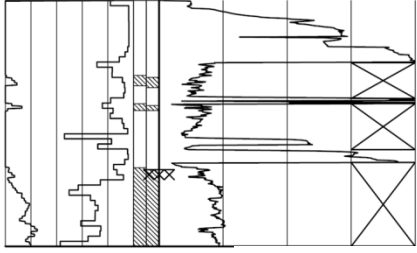
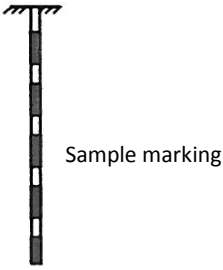
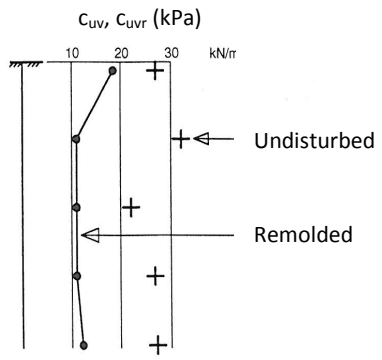
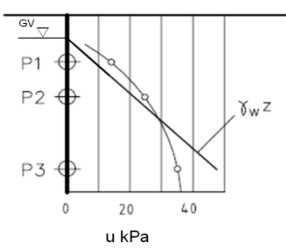
Multiconsult

 Stop against stone, block or firm layers Stop against assumed bedrock	Soundings are carried out to obtain an indication of the relative stiffness of the penetrated soils. From that, the stratification and depth to the bedrock surface or firm layers may be estimated. Reference is made to «Geotechnical enclosure – test standards and guidelines».
 Predrilled Medium resistance Very low resistance Very high resistance Terminated without reaching firm layers or bedrock Number of half-turns pr. m sink Predrilled Hammered	● ROTARY WEIGHT SOUNDING Performed with jointed $\varnothing 22$ mm drillrods with a 200 mm twisted point. The drillrods are rotated manually or by a drilling machine into the soil with maximum 1 kN (100 kg) vertical load on the rods. If the rod assembly does not sink from this weight, the rods are rotated manually or by machine operation. The number of half-turns per 0.2 m penetration is recorded. The drilling resistance is presented in a diagram with vertical depth-scale and a cross-line for every 100 half-turns. Hatching represents sinking without rotation, with the vertical load during sinking added to the left. A cross indicates that the drillrods are hammered into the ground.
 Medium resistance Low resistance High resistance Q_0 Q_0 kNm/m	▼ RAM OR HAMMER SOUNDING The drilling is carried out with jointed $\varnothing 32$ mm drillrods and a tip with standardized geometry. The drillrods are struck with an energy of 0.38 kNm. The number of blows per 0.2 m penetration is recorded. The drilling resistance is recorded as Q_0 per m sink, where Q_0 = deadweight * falling height/sink per blow (kNm/m)
 Corr. tip resistance [MPa] Pore press. [MPa] Side friction [MPa] F_{DT} kN	▽ CONE PENETRATION TEST (CPTU) A cylindrical, instrumented probe with a conical tip is pushed into the ground at a constant penetration rate of 20 mm/sec. During penetration, the forces against the tip and the friction sleeve are recorded, so that the cone resistance q_c and the sleeve friction f_s can be deduced (CPT). In addition, the penetration pore pressure u is measured just behind the conical tip (CPTU). The recordings are taken continuously every 0.02 m, and the method therefore gives very detailed information of the ground conditions. The results can also be used to determine soil stratification, soil type and mechanical properties of the soils (shear strength, deformation and consolidation parameters).
 F_{DT} kN	◒ ROTARY PRESSURE SOUNDING The test is carried out with smooth, jointed $\varnothing 36$ mm drillrods with a standardized tip equipped with a welded hard alloy edge. The drillrods are pushed into the ground with a constant penetration rate of 3 m/min and a constant rotation rate of 25 rpm. The thrust F_{DT} (kN) is recorded automatically under these conditions, and may be used to evaluate the ground conditions. The method is particularly well suited for indication of quick clay. On the other hand it does not verify the depth to bedrock.
 Stone Drillsink in rock cm/min.	✠ Rock control drilling Rock control drilling is carried out using jointed $\varnothing 45$ mm drillrods and a hard alloy drillbit with a return valve. A heavy percussion hammer and water flushing at high pressures is used during drilling. Drilling through layers with different properties, for example gravel and clay, can be interpreted, also penetration of blocks and large stones. For verification of the rock surface, an intrusion of 3 m is required, including recording of the sink during drilling.

Geotechnical enclosures

Field investigations

Multiconsult

 Drilltime, s/m Flushing pressure, MPa Thrust F_{DT} (kN)	T TOTAL SOUNDING This method combines rotary pressure sounding and rock control drilling. $\phi 45$ mm jointed rods and a $\phi 57$ mm drillbit with impregnated hard metal or diamond fragments are used. During drilling in soft layers, the rotary pressure mode is used, with drillrods given constant penetration and rotation rates. When a dense layer is encountered, the rotation rate is increased. If this is not sufficient to advance the drillrods, water or air flushing and strokes on the drillstring are used. The thrust F_{DT} (kN) is recorded continuously and is shown to the right on the diagram, whereas flushing pressure, number of strokes and drilling time is shown to the left.
 Sample marking	SAMPLING Carried out to obtain samples for determination of the geotechnical properties of the soils in the laboratory. <u>Machine operated auger drilling (disturbed bag samples):</u> This method is carried out using hollow drillrods, with a metal spiraled plate welded to the drillrod. If a drillrig is used, it may be drilled in the range of 5-20 m depth, depending on the soil, density and the level of the groundwater table. With this method, disturbed bag samples may be taken by collecting the materials gathered between the spirals. <u>Core/block sampling (undisturbed samples):</u> Carried out to obtain samples for determination of the mechanical properties of soils in the laboratory. Usually, piston sampling is used to extract 60-100 cm long core samples. Cylinders made of PVC, steel or similar, and both equipment with or without an inner liner may be used. At the sampling depth, the sample cylinder is pushed down into the soil, while the inner rod with the piston is fixed. By this procedure, a soil sample is sheared and later extracted to the surface. The sample cylinder is then sealed and transported to the laboratory. The diameter of the sample may vary between $\phi 54$ mm (most common) and $\phi 95$ mm. It is also possible to use other samplers, such as hammer samplers or block samplers. The sample quality is classified in Quality classes 1-3, where 1 is the best. Piston sampling usually provides samples in Quality classes 1-2 for clays.
 C_{uv}, C_{uvr} (kPa) kN/m² Undisturbed Remoulded	+ Vane testing A vane with dimensions $b \times h = 55 \times 110$ mm or 65×130 mm is pushed into the ground to the required test level. A gradually increasing torque is applied to the vane until it reaches failure. The corresponding torque is recorded. The procedure is carried out for both undisturbed and remoulded conditions, where the latter torque value is recorded after 25 repeated rotations of the vane assembly. The undrained shear strengths C_{uv} and C_{ur} are calculated from the torque at first failure and after remoulding, respectively. From this, the sensitivity $S_t = C_{uv}/C_{ur}$ can be determined. The interpreted values must usually be empirically corrected for the effective overburden stress at the test level, and for the plasticity of the soil.
 GV P1 P2 P3 $\gamma_w z$ u kPa	⊖ PORE PRESSURE MEASUREMENTS The measurements are carried out utilizing a standpipe with a filter tip, or by a hydraulic (open)/electric piezometer. The filter or piezometer tip, extended with open piezometer tubes, is pushed into the ground to the required depth. A stable pore pressure is recorded from the elevated height of the water in the tube, or by readings from an electric pressure transducer in the tip. Choice of equipment is made based on the ground conditions and the purpose of the tests. The ground water table is observed or measured in the hole.

Geotechnical enclosure

Laboratory testing

Laboratory testing give precise classifications of soil and determines mechanical parameters. The tests are performed on samples retrieved from the field. Relevant standards and guidelines are given in Geotechnical enclosure – Test standards and guidelines.

MINERAL SOILS

The soil is classified and identified after sample extrusion. Mineral soils are usually classified according to their grain size distribution. Identification and grain size for the various fractions are:

Fraction	Clay	Silt	Sand	Gravel	Stone	Block
Grain size (mm)	< 0,002	0,002-0,063	0,063-2	2-63	63-630	> 630

A soil may contain one or more of the fractions above. The soil is identified in accordance with the grading curve, with the principal fraction having the dominating influence on the soil properties. This is identified by a noun, with secondary contributing fractions as adjectives (for example silty sand). The clay content has the largest influence on the identification of the soil. Moraine is a poorly sorted glacial deposit that can contain all fractions from clay to block. The major fraction is given first in the description according to specific identification rules, for example gravelly moraine.

ORGANIC SOILS

Organic soils are classified according to their origin and degree of transition of the soils. The most important types are:

Identification	Description
Peat	Marsh plants, more or less transformed.
<i>Fibrous peat</i>	Fibrous with easily recognizable plant structure. Shows some strength.
<i>Pseudo-fibrous peat, medium peat</i>	Recognizable plant structure, no strength in the plant debris.
<i>Amorphous peat, black peat</i>	No visible plant structure, spongy consistency.
Gyttja and dy	Transformed structure of organic material, may contain mineral constituents.
Humus	Plant debris, biological organisms with non-organic content.
Mold and topsoil	Strongly transformed organic materials with loose structure, usually comprises the top soil layer.

GRAIN SIZE DISTRIBUTION ANALYSIS

A grain size distribution is carried out by wet or dry sieving of the fractions with diameter $d > 0,063$ mm. For fractions of particles with smaller diameter, the grain size distribution is determined by a suspension analysis and use of a hydrometer. In the suspension analysis, the material is suspended in water and the density of the suspension is measured by the hydrometer at certain time intervals. The grain size distribution can then be determined from Stokes law on sedimentation of spherically shaped particles in water. It will often be necessary to combine ordinary sieving with a suspension analysis.

WATER CONTENT (w %)

Water content is defined as the ratio of the mass of water to the mass of dry matter in a sample, expressed as a percentage. It is determined by drying a soil sample at 110°C for 24 hours.

ATTERBERG CONSISTENCY LIMITS – LIQUID LIMIT (w_l %) AND PLASTICITY LIMIT (w_p %)

The consistency limits (Atterberg's limits) for a soil express the range of water contents where the material is plastic and possible to form. The liquid limit expresses the water content where the material goes from a plastic to a liquid state. The plastic limit expresses the water content where the material no longer can be formed, but is cracking up during mechanical treatment. The plasticity index $I_p = w_l - w_p$ (%) expresses the plastic range in water content for the soil, and is used to classify the plasticity properties. If the natural water content is higher than the liquid limit, the material liquifies when remoulded (common for quick clays).

HUMUS CONTENT

The humus content is determined by colorimetry and use of NaOH for chemical reaction with the organic contents. The method gives the content of humified organic content in a relative scale. Other methods, such as loss on ignition (LOI) of a soil sample in a muffle furnace or wet-oxidation by hydrogen peroxide, may also be used.

Geotechnical enclosure

Laboratory testing

DENSITY, UNIT WEIGHT, VOID RATIO AND POROSITY

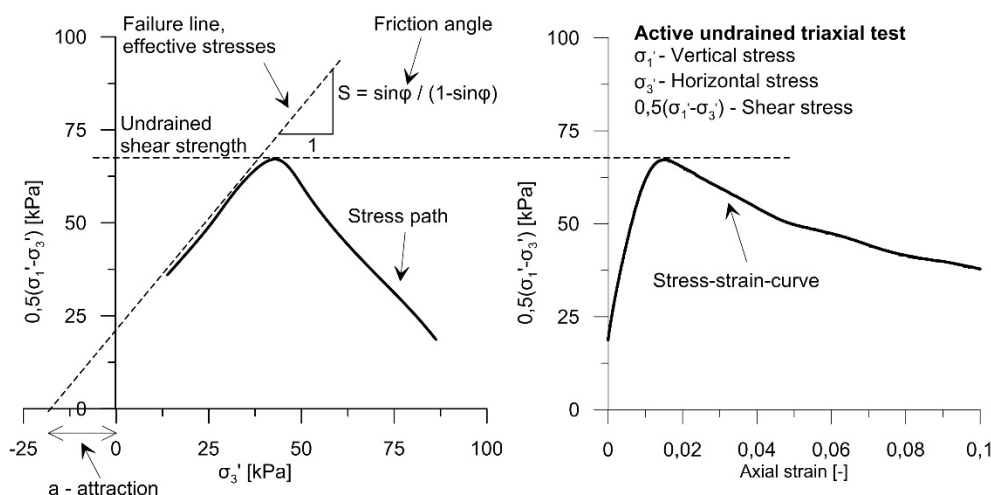
Property	Symbol	Unit	Description
Bulk density	ρ	g/cm ³	Mass of specimen per volume unit. Determined for the whole cylinder and a small sample
Grain density	ρ_s	g/cm ³	Mass of solid matter per volume unit of solid material
Dry density	ρ_d	g/cm ³	Mass of dry matter per volume unit
Unit weight of soil	γ	kN/m ³	Weight of specimen per volume unit ($\gamma = \rho g = \gamma_s(1+w/100)(1-n/100)$, where $g = 10 \text{ m/s}^2$)
Unit weight of solids	γ_s	kN/m ³	Weight of solid matter per volume unit ($\gamma_s = \rho_s g$)
Dry unit weight of soil	γ_d	kN/m ³	Weight of dry material per volume unit ($\gamma_d = \rho_d g = \gamma_s(1-n/100)$)
Void ratio	e	-	Volume of pores divided by volume of solid particles ($e = n/(100-n)$) where n is porosity (%)
Porosity	n	%	Volume of pores as a percentage of total volume of the sample

SHEAR STRENGTH

The shear strength of the soil is used for e.g. slope stability calculations and bearing capacity problems. For short term loading conditions in fine grained materials (clays), the undrained shear strength is used. For longer time spans the material has a drained behaviour and effective stress parameters are used.

The effective stress based parameters a (attraction), $\tan\phi$ (friction) and alternatively $c = a \tan\phi$ (cohesion) are determined by triaxial loading tests on undisturbed (clay) or re-constituted specimens (sand). The shear strength depends on the effective normal stress (total stress less pore pressure) on the critical plane. The test results are presented as stress paths, showing development of stresses and corresponding strains in the sample towards failure. From this and other information, the characteristic values for the shear strength parameters for the actual problem are determined.

The undrained shear strength is defined as the maximum shear stress the soil can experience before failing. This shear strength represents a situation with rapid stress changes, without drainage of pore water or dissipation of pore pressures. In the laboratory, the undrained shear strength is determined by unconfined compression tests (c_{ut}), falling cone tests (undisturbed c_{uk} , remoulded c_{ur}), undrained triaxial tests (compression/active c_{uA} , extension/passive c_{uP}) and direct shear tests (c_{uD}). The undrained shear strength can also be determined in the field by for example cone penetration tests with pore pressure measurement (CPTU) (c_{ucptu}) or field vane tests (undisturbed c_{uv} , remoulded c_{ur}).



SENSITIVITY

The sensitivity $S_t = c_u/c_r$ expresses the ratio between the undisturbed and remoulded undrained shear strengths. This property can be determined from a falling cone test in the laboratory (NS 8015) or by a field vane test in the field. Quick clay for instance has a very low remoulded shear strength c_r ($c_r < 0.5 \text{ kPa}$ NS8015, $c_r < 0.33 \text{ kPa}$ ISO 17892-6), and therefore normally exhibits very high sensitivity.

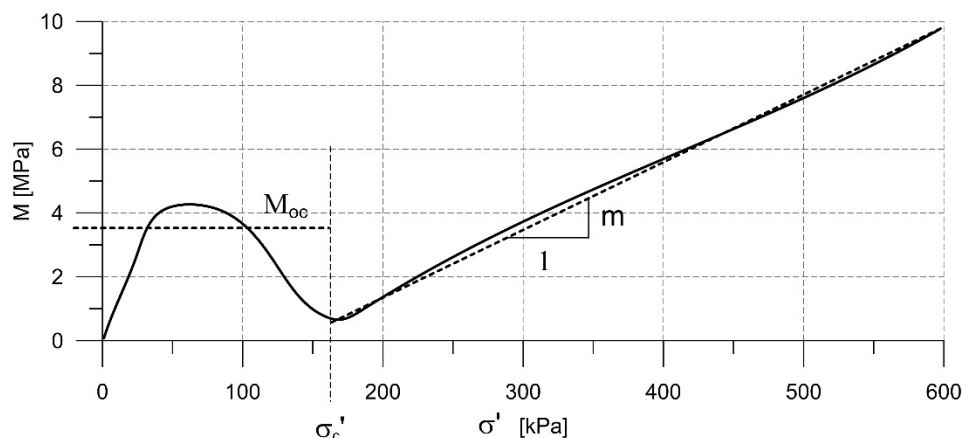
Geotechnical enclosure

Laboratory testing

DEFORMATION AND CONSOLIDATION PROPERTIES

The deformation and consolidation properties of a soil are used for calculating settlements and are determined by loading tests in an oedometer. The soil sample is enclosed in a rigid ring that prevents lateral deformation, and is loaded vertically with an incrementally or continuously increasing load. Corresponding values of load and deformation (strain ϵ) are recorded, and the deformation modulus (stiffness) of the soil can be deduced by $M = \Delta\sigma' \Delta\epsilon$ (Janbu theory). The modulus is presented as a function of the vertical stress σ'_v . A key parameter interpreted from oedometer tests in clay is the preconsolidation stress (σ'_c). This parameter indicates the previous loading history of the soil (i.e. previous overburden).

The deformation modulus differs in the stress range below and over the preconsolidation stress. In clay, the stiffness in the overconsolidated stress range (under σ'_c) can be represented by a constant stiffness modulus (M_{oc}). For stress levels above σ'_c , the stiffness increases with increasing stress. The slope of this curve is described by the modulus number.



FROST SUSCEPTIBILITY

The frost susceptibility of a soil is determined from the grain size distribution curve or by measuring the capillary rise of the material. The frost susceptibility is classified in the groups T1 (No susceptibility), T2 (Low susceptibility), T3 (Medium susceptibility) and T4 (High susceptibility).

COMPACTION PROPERTIES

By compaction of a soil, a denser and more compact layering of the mineral grains is obtained. The compaction properties of a soil are determined on samples with varying water content that are compacted with a certain compaction energy (usually Standard or Modified Proctor). The results are presented in a diagram showing the dry density ρ_r as a function of the water content w_i . The maximum dry density obtained in the test (ρ_{dmax}) is used in specifications of compaction works. The corresponding water content is denoted the optimum water content (w_{opt}).

PERMEABILITY (k cm/sec or m/year)

The permeability is defined as the amount of water q which under given conditions will flow through a soil volume per unit of time. In general, the permeability is determined from the following relationship: $q = kiA$, where A is the gross area of the cross-section normal to the direction of flow and i = hydraulic gradient in the direction of flow (= difference in potential per unit length). The permeability can be determined by controlled flow tests in the laboratory using constant or falling head, by pumping or by a flow test in the field.

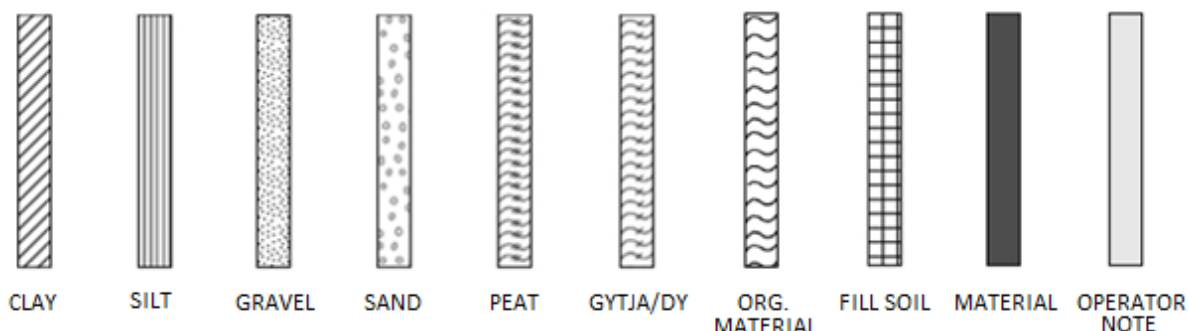
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Laboratory testing

Multiconsult

BORHOLE PROFILE - HATCHING

In the borehole profile each sample is presented with a hatching corresponding to the principle fraction of the material. There is also a separate hatching for notes from the drilling operator. The different hatchings are shown below.



Note: This is a subjective evaluation based on the visual appearance of the material unless a grain size analysis is performed.

CLAY: Clay content greater than 15 %

SILT: Silt content greater than 45 % and clay content less than 15 %

SAND: Sand content greater than 60 % and clay content less than 15 %

GRAVEL: Gravel content greater than 60 % and clay content less than 15 %

MATERIAL: Used when none of the above are appropriate. Usually based on a grain size analysis

PEAT: Marsh plants, more or less transformed

GYTJA/DY: Transformed structure of organic material, may contain mineral constituents

ORG. MATERIAL: Highly transformed organic material with open structure

FILL SOIL: Non-natural deposits

Drilling operator note: Notes from the drill rig operator (e.g. empty cylinder, predrilling etc.)

GRAIN SIZE ANALYSIS (K) / TRIAXIAL TESTS (T) / OEDOMETER TESTS (Ø)

For samples where a grain size analysis, triaxial test and/or oedometer test has been performed, the borehole profile is labeled with G, T or O respectively at the relevant depth. The depth is not exact, so the label is only a reference to separate drawings where the specific test is reported.

SYMBOLS – Water content and Atterberg limits

Measurements of water content and Atterberg limits are given on the borehole profile by the following symbols on their respective graphs. If the water content exceeds the limit of the graph axis, the numerical value is given.

Water content w		Plastic limit w_p	
		Liquid limit w_f	

SYMBOLS – Undrained shear strength

Measurements for fall cone and unconfined compression tests are given on the borehole profile by the following symbols on their respective graphs. If the measured value exceeds the limit of the graph axis, the numerical value is given.

Fall cone, undisturbed c_{ufc}		Fall cone, remoulded c_{urfc}	
Unconfined compression test The line indicates the axial strain (%) at failure		Fall cone remoulded $c_{urfc} \leq 2,0 \text{ kPa}$	0,9

Geotechnical enclosures

Guidelines and standards – ground investigations

**GUIDELINES AND STANDARDS – FIELD INVESTIGATIONS**

Field investigations described in geotechnical enclosures, along with terminology and classification used in reporting, are based on the following guidelines and standards:

Document	Topic
NGF Melding 1	SI-units
NGF Melding 2, NS-EN ISO 14688-1 og -2	Symbols and terminology
NGF Melding 3	Rotary weight sounding
NGF Melding 4	Vane test
NGF Melding 5, NS-EN ISO 22476-1	Cone penetration test (CPTU)
NGF Melding 6	Pore pressure and ground water measurements
NGF Melding 7	Rotary pressure sounding
NGF Melding 8	Commentary codes for field investigations
NGF Melding 9	Total sounding
NS-EN ISO 22476-2	Ramsounding
NGF Melding 10	Descriptive texts for ground investigations
NGF Melding 11, NS-EN ISO 22475-1	Soil sampling
Statens vegvesen Håndbok R211	Field investigations
NS 8020-1	Qualification criteria for enterprises performing ground investigations - Part 1: Geotechnical field investigations

Geotechnical enclosures

Guidelines and standards – ground investigations

**GUIDELINES AND STANDARDS – LABORATORY TESTS**

The laboratory tests described in geotechnical enclosures, along with terminology and classification used in reporting, are based on the following guidelines and standards:

Document	Topic
NS8000	Atterberg limits – terminology
NS8001	Percussion liquid limit
NS8002	Fall cone liquid limit
NS8003	Plastic limit
NS8004	Shrinkage limit
NS8005, NS-EN ISO 17892-4	Grain size distribution
NS8010, NS-EN ISO 14688-1 og -2	Soil – constituents and structure. Classification and identification of soils
NS8011, NS-EN ISO 17892-2	Density
NS8012, NS-EN ISO 17892-3	Grain density
NS8013, NS-EN ISO 17892-1	Water content
NS8014	Void ratio, porosity and degree of saturation
ISO 17892-6:2017	Shear strength by fall cone tests
NS8016	Shear strength by unconfined compression test
ISO 17892-5:2017	Oedometer test, incremental loading
NS8018	Oedometer test, continuous loading
NS-EN ISO/TS 17892-8 og -9	Triaxial tests (UU, CU)
The National Public Roads Adm. Statens vegvesen Handbook R210	Laboratory testing